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### NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

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· (NASA-CR-151160) DESIGN CERTIFICATION TESTS
· HIGH PRESSURE OXYGEN FILTER (HPOF) PROGRAM,
· SUMMARY REPORT (APPENDICES A, B, AND C)
· (Winter Corp., Los Angeles, Calif.) 353 p
· HC A16/MF A01 CSCL 13K G3/37

N77-16341

Unclas 12525

SUMMARY REPORT

DESIGN CERTIFICATION TESTS
HIGH PRESSURE OXYGEN FILTER
(HPOF) PROGRAM

(Appendices A, B, and C)





LYNDON B. JOHNSON SPACE CENTER
WHITE SANDS TEST FACILITY
LAS CRUCES, NEW MEXICO

# APPENDIX A

ACCEPTANCE TEST PROCEDURE

TP-259



E323 WEST IMPERIAL HIGHWAY LOS ANGELES, CALIFORNIA 90045 Telephone (213) 641-4300 Telex. 67-3105 ACCEPTANCE TEST PROCEDURE
TP 259

REVISION A

ACCEPTANCE TEST PROCEDURE TP-259.

HIGH PRESSURE OXYGEN FILTER

WINTEC PART HUMBER 9-812

FOR

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

CONTRACT NAS 9-14466

ORIGINAL PAGE IS OF POOR QUALITY

APPROVED: EB. Soco-	DATE: 2-24-7-6
F. B. Jones, Laboratory Director	
APPROVED: Come	DATE: 2-24-76
R. Roma, Quality Assurance Manage	er
APPROVED: CANONICA	DATE: 2-24-76
B. A. Wilson, Chief Engineer	

#### REVISION RECORD

ECL	DESCRIPTION OF CHANGE	DATE	APPROVED
N/C	Initial Release	2-24-76	FB Journ
A·	Page 3: Added Figure 5 callout.  Page 8: Para 4.1.2: was E.B. Weld  Para 4.1.3: Was 2.5 grams  Para 4.2.1: Added Figure 5  Para 4.2.3: Was 844 + 14Kg per sq. cm.  (12000 + 686 PSIA)  Page 9: Para 4.2.5: Deleted Paragraph  Para 4.3.8: Was 1.08 Kg per sq. cm.  (20" H20)  Para 4.3.9: was reduce GN2 Pressure.  Para 4.3.11: was 1.08 Kg per sq. cm.  (20" H20)0.0127 Kg per sq. cm.  (20" H20)0.0127 Kg per sq. cm.  (20" H20)0.0127 Kg per sq. cm.	9-9-76	Popular
-	Page 10: Para 4.3.13: Added correction data Para 4.4.1.1: Revised flow rates per Para 4.4.2.1: Nasa letter Aug 3, 1976. Para 11: Para 4.4.2.2: Added max AP Page 16: Table 3: Revised Item 3 Data Sheets: Revised to conform to latest configuration and new flow requirements.		
	ORIGINAL PAGE IS OF POOR QUALITY		

## TABLE 1

#### TABLE OF CONTENTS

	Description	Page
1.0	Scope .	4
2.0	Applicable Documents	4
3.0	Test Conditions	5
4.0	Test Procedures	8
4.1	Inspection of Product	8
4.2	Proof Pressure	8
4.3	Bubble Point	9
4.4	Clean Flow-Differential Pressure	10
4.5	Cleanliness Verification	11
4.6	Drying	11
4.7	Final Inspection	12
5.0	Packaging	12
6.0	Data Package	13
	Figures	
· ı	Proof Loading Test Set-Up	14
2	Bubble Point Test Set-Up	15
3	Flow-Differential Pressure Set-Up	16
4	Label and Seal	17
5 .	Proof Loading Fixture 4-2498 Cross Section <u>Tables</u>	
1	Table of Contents	3
2	Test Sequence .	7
3	Instrumentation and Equipment List	18

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#### 1.0 SCOPE

This specification defines the procedures to be used in the Acceptance Testing of the Winter High Pressure Oxygen Filter, part number 9-812. The objectives of these tests is to provide evidence that the production filters will meet the requirements of the Winter Detailed Problem. Statement SP 3400-103.

#### 2.0 APPLICABLE DOCUMENTS

The following documents and drawings form a part of this specification to the extent specified herein.

#### 2.1. Specifications

#### Military

MIL-P-27401 B Propellant Pressurizing Agent, Nitrogen

MIL-C-45662 A Calibration Standards

MIL-STD-794 B Parts and Equipment, Procedures for Packaging and Packing of

MIL-STD-834 C Packaging Data Forms, Instruc-

tions for Preparation and Use of.

MIL-P-26514, Type I Polyurethane Foam, Rigid or Flex-Class 2, 1.5 lbs. per ible for Packaging. cubic foot Density

NASA

JSC-SN-C-0005 Contamination Control Requirement

for the Space Shuttle Program

TT-I-735 A Isopropyi Alcohol (Isopropanol) Amendment 2

MSFC-SPEC-237 A Precision Cleaning Agent (PCA)

NH6000-1 (1A) Requirements for Packaging, Handling and Transport for Aeronauti-

cal and Space Systems, Equipment and Associated Components.

#### Federal

Fed Spec PPP-B-636

Box Fiberboard

a. Type CF, Class

Domestic

b. Type CF, Class Weather Resistant

L-P-278, Type II Grade B, Finish I Plastic Sheet and Strip, Thin

Gage, Polyethylene.

#### Society of Automotive Engineers

ARP-598 1 March 1960 Determination of Particulate Contamination of Hydraulic Fluids by

Particle Count Method.

ARP-599 A 2 Oct. 1972 Dynamic Test Method for Determining the Degree of Clearliness of the Down Stream Side of Filter

Elements.

ARP-901

Bubble Point Test Method.

Rockwell International

MB096-005

Material Cleanliness, Precision

Packaging.

MB085-006

Film Transparent Precision Clean

Packaging (Tinted).

Wintec

SP3400-103

High Pressure Oxygen Filter, Detailed Problem Statement of

2.2 Drawings

9-812

High Pressure Oxygen Filter (HPOF)

4-2498

Flow & Proof Fixture

4-2499

Bubble Point Fixture

#### 3.0 TEST CONDITIONS

#### 3.1 Standard Conditions

Unless otherwise specified, all tests will be conducted under the following ambient conditions:

Temperature:

70° + 20°F

Relative Humidity:

80% Maximum

Barometric Pressure:

Local Atmospheric

-5-

#### 3.2 . Test Equipment

The required instrumentation will be as shown in the schematic diagrams of Figure 1 through Figure 3.

Refer to Table 3 for instrument type, accuracy, range and calibration frequency. All instrument calibrations meet the standards of calibration of MIL-C-45662 with traceability to N. B. S.

System cleanliness to conform to the cleanliness requirements of this specification and specification WSQ-005.

#### 3.3 Test Fluids

Nitrogen per MIL-P-27401 or equivalent. Isopropyl Alcohol per TT-I-735, Grade B. Precision Cleaning Agent (PCA) per MSFC-SPEC-237 or equivalent.

All test fluids entering the HPOF will be prefiltered through a 2 micron absolute (or finer) filter.

#### 3.4 Data

A continuous test log will be maintained for each test specimen. The log shall contain a record of all operations and tests performed and the resultant data for each test. See Appendix 1 for test log forms.

#### 3.5 Test Discrepancies

3.5.1 The failure of any portion of the test equipment will not constitute failure of the unit being tested. The test sequence may be continued at the discretion of the cognizant test engineer if the failure does not represent a danger to the facility, test personnel, the unit undergoing test, or invalidate the required test objectives.

#### 3.5.2 Failure Notification

In the event that the unit under test exhibits any failure or deviation from the test requirements set forth in this procedure, notify Mr.Irwin Smith, NASA-JSC, White Sands Test Facility, Las Cruces, N. M., that a test failure has occurred as follows:

- a) Notify Mr.I. Smith, Telephone (505) 524-5522 within 24 hours after failure occurance.
- b) Prepare and submit a written failure report within seven(7) calendar days.

# TABLE 2 ACCEPTANCE TEST SEQUENCE

Sequence Number	Description	TP 259 Paragraph
1	Inspection of Product	4.1
2	Proof Pressure	4.2
3	Bubble Point	. 4.3
4.	Flow-△P	4.4
5	Cleanliness Verification	4.5
· 6	Drying	4.6
7	Final Inspection	4.7
8	Packaging	5.0

#### 3.6 Test Notification

The Mr. I. Smith, NASA-JSC, White Sands Test Facility, and the Government Inspector, as required by the applicable purchase order, shall be notified at least 48 hours prior to the performance of any scheduled test so that authorized representatives may witness the test as required.

#### 4.0 TEST PROCEDURE

Unless otherwise specified, the acceptance tests are to be performed on all deliverable HPOF assemblies prior to delivery. The tests are to be performed in the sequence shown in Table 2.

#### 4.1. Inspection of Product

4.1.1 Each HPOF assembly (P/N 9-812) shall be inspected for conformance with the drawing requirements. The areas of inspection shall cover:

Finish
Workmanship
Dimensions
Identification
Certified Materials and Processes

- A 4.1.2 Inspect the TIG weld that joins the two 20-1265

  rings with a 40% binocular microscope. \_There shall be
  no cracks or breaks in the welds.
- A 4.1.3 Measure the weight of each HPOF assembly to the nearest 10 milligram and record the weight. The weight of the HPOF shall not exceed 7.0 grams.

#### 4.2 Proof Pressure

A

- A [4.2.1 Install the HPOF into Fixture 4-2498 as shown in Figure 5.
  - 4.2.2 Install the HPOF and 4-2498 fixture into a proof pressure test system as shown in Figure 1.
  - 4.2.3 With the outlet of the 4-2498 Fixture vented to atmosphere, pressurize the inlet of the fixture to 668 ± 6 Kg per sq. cm. (9500 ± 100 psia) with GN2. Maintain this pressure for 5 ± 1 minutes. Reduce the pressure to atmosphere by venting the inlet side of the HPOF.
  - 4.2.4 The HPOF shall not collapse as a result of this test.

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- 4.2.5 DELETED
- 4.3 Bubble Point
- 4.3.1 The 4-2499 fixture and transfer tube shall be flushed with IPA that has been filtered through a 0.8 micron or finer membrane.
- 4.3.2 Install the HPOF into Fixture 4-2499.
- 4.3.3 Measure and record the surface tension and temperature of the Isopropanol (IPA) that will be used.
- 4.3.4 Prefilter Isopropanol (IPA) through a 0.45 micron membrane.

  Measure and record the surface tension and temperature of the

  prefiltered IPA. This IPA is to be reserved for bubble
  point testing of the HPOF assemblies.
- 4.3.5 Attach the HPOF and Fixture 4-2499 to a transfer tube. The transfer tube is a part of the Bubble Point Test system, Figure 2.
- 4.3.6 Using a Hypodermic syringe, fill the transfer tube with IPA (reference paragraph 4.3.4).
- 4.3.7 Attach the transfer tube to the Bubble Point Test System, Figure 2. The 4-2499 Fixture shall be in a vertical position.
- A 4.3.8 Pressurize the HPOF to 1.45 to 1.52 Kg/cm<sup>2</sup> (8 to 14 in. Hg,)
  100 to 190 in. H<sub>2</sub>O. The IPA in the transfer tube
  will be forced through the HPOF to wet all internal surfaces
  of the HPOF. The IPA will rise in and overflow the open
  port of the 4-2499 fixture. All bubbles of entrapped air
  shall cease to emit from the test fixture before proceeding
  with the next step.
- A 4.3.9 Reduce GN<sub>2</sub> pressure to 1.068 Kg/cm<sup>2</sup> (1.0 in. Hg, 14 in. H<sub>2</sub>0) open valve (A) and allow the excess IPA in the transfer tube to drain out of tube. Close the valve (A).
  - 4.3.10 Assure that the open part of Fixture 4-2499 is filled with IPA.
  - 4.3.11 Increase the GN<sub>2</sub> pressure to · 1.154 Kg/cm<sup>2</sup>(3.5 in. Hg, 47.6 in. H<sub>2</sub>O) for 2 min. Then increase the pressure at a rate of 1.051 Kg/cm<sup>2</sup>/minute (0.5 in Hg, 7.0 in. H<sub>2</sub>O/minute.) until the first train of bubbles emit from the HPOF. This is the initial (observed) bubble point and shall be recorded. The initial bubble point shall be corrected.

4.3.12 Method for determining surface tension correction factor.

 $ST = C \times R \times D$ 

#### Where:

ST = Surface Tension - Dynes/cm
C = 16.5 (Capillary Tube Constant)
R = Difference in Rise of Fluid in cm.
D = Density of Fluid at Measured Temp.

4.3.13 Method for correcting the observed bubble point to standard conditions.

Where:

 $P_{S} = (P-dh) \frac{21.15}{ST}$ 

Ps = Standard Bubble Point
P = Observed Bubble Point
(in. Hg x 13.596 = in. H2O)
(PSID x 27.687 = in. H2O)

d = Density

h = Immersion Depth, Inches ST = Measured Surface Tension 21.15 = Standard Surface Tension

- 4.3.14 The standard bubble point  $(P_S)$  shall be greater than (TBD) Kg per sq. cm. (TBD inches of water).
- 4.3.15 Remove the 4-2499 fixture from the bubble point test system and flow prefiltered (0.45 micron) GN<sub>2</sub> through the HPOF to remove all of the residual IPA.
- 4.3.16 Remove the HPOF from the 4-2499 fixture.
- 4.4 Clean Flow- Differential Pressure
- 4.4.1 Install the 4-2498 flow fixture into a flow system as shown in Figure 3.
- 4.4.1.1 Conduct a tare test to measure the system differential pressure (△P) at flow rates 0.045, 0.061, and 0.076 ACFM (1.28, 1.71 and 2.14 SCFM) of GN2 with an inlet pressure of 29.18 Kg per sq. cm. (400 ± 5 psig). Record the tare△P at each flow rate.
- 4.4.2 Install the HPOF into the 4-2498 fixture.
- 4.4.2.1 Install the HPOF and 4-2498 fixture into the flow system (reference Figure 3) and conduct a flow-△P test at flow rates of 0.045, 0.061 and 0.076 ACFM (1.28, 1.71 and 2.14 SCFM) of GN<sub>2</sub> with an inlet pressure of 29.18 Kg per sq. cm. (400 + 5 psig). Record the△P and temperature at each flow rate. This will be the gross-△P at the three noted flow rates.

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- 4.4.2.2 Subtract the tare- $\triangle P$  from the gross- $\triangle P$  for each respective flow rate. The difference will be the net- $\triangle P$  for each flow rate. The net- $\triangle P$  shall not exceed 300 PSID.
- 4.4.2.3 Remove the HPOF assembly from the flow system and the 4-2498 flow fixture and set the HPOF aside.

#### 4.5 Cleanliness Verification

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- 4.5.1 Clean the 4-2498 flow fixture by thoroughly flushing with PCA solvent that has been prefiltered through a 0.8 micron or finer filter.
- 4.5.2 Carefully install the HPOF assembly in the 4-2498 flow fixture. Flush the HPOF in both directions by flowing prefiltered (0.8 micron or finer) PCA through the HPOF.
- 4.5.3 After flushing the HPOF in both directions, take a sample of the PCA effluent while flowing one direction, then in the other direction. Fifty (50) mil of PCA effluent shall be sampled in each flow direction. The effluent samples may be drawn through a Wintec viewer sampler that has been loaded with a precleaned and pre counted 0.8 micron, 47 min. membrane (Type AA or equivalent). The membrane shall be examined and a particulate count made per the requirements of ARP 598.
- 4.5.4 The particulate count shall not exceed Table I, Level 25 of JSC-SN-C-0005 as noted below:

Particle Size Range	Particles/100 ml
<pre>5 microns 5 - 15 microns</pre>	no silting 19
16 - 25 microns	4
>25 microns	0 '

- 4.5.5 If the particulate count of paragraph 4.5.4 is exceeded, repeat paragraphs 4.5.2 and 4.5.3 until the HPOF meets the requirements of paragraph 4.5.4.
- 4.5.6 Remove the HPOF from the 4-2498 fixture.

#### 4.6 Drying

4.6.1 Place the HPOF in a precleaned aluminum dish and place in a vacuum oven. Dry the HPOF at 170 ± 10 degrees F for 15 minutes without a vacuum and 30 to 45 minutes at a pressure of 25 to 28" Hg.

#### 4.7 Final Inspection

4.7.1 Visually inspect the HPOF assembly before packaging to assure the unit did not sustain any damage as a result of the acceptance testing and handling. Assure that there are no particles on the exterior surfaces of the unit.

#### 5.0 PACKAGING

#### 5.1 Inner Packaging

NOTE: Inner packaging shall be accomplished in the Clean Room.

- 5.1.1 Insert the unit into a 2 mil tinted nylon "C" Bag (para 2.9) approximately 6 x 3 inches. The inside of the bag shall meet or exceed the requirements of PB095-005, Level 1.
- 5.1.2 Partially seal bag leaving corner open, evacuate air, and final heat seal bag.
- .5.1.3 Attach an Inspection Seal over the final heat sealed ends of bag, Figure 4B.
- 5.1.4 Place the sealed unit into a 6 mil anti-static polyethylene (para 2.10) contamination barrier bag approximately 6 x 3 inches. Insert a Cleanliness/Identification Tag, Figure 4A into bag and partially heat seal bag, evacuate bag, and final heat seal bag. The inside of the bag shall meet or exceed the requirements of PB0295-005, Level 3.

#### 5.2 Unit Packaging

- 5.2.1 Wrap the packaged unit in a 1/2 inch thick sheet of polyurethane foam. Tape overlap using 1/2 inch wide masking tape.
- 5.2.2 Place wrapped unit into box (para 2.7a) and seal using reinforced tape.
- 5.2.3 Stamp side of each box with the following information:

Item Name: High pressure oxygen filter (HPOF)
Manufacturer's Part Number: 9-812

Quanity in Package

Clean Marking: This unit has been cleaned to Table I, Level 25 of JSC-SN-C-0005.

Traceability Identification

Serial Number

Mfg: Wintec Division of Brunswick Corporation

Buyer Purchase Order Number

Date of Packaging

- 5.3 Shipping Container
- 5.3.1 Unit packages shall be placed into a Weather Resistance Fiber-board Container.
- 5.3.2 Test data and associated data shall be enclosed in an envelope and placed inside of the Shipping Container. Close and seal container using gummed reinforced tape.
- 5.3.3 The container shall be marked with information specified in para 5.2.3.
- 6.0 DATA PACKAGE
- 6.1 The data package shall include but not be limited to the following items as applicable:
  - a) Statement of Certification
  - b) Visual Inspection Characteristics (data sheets)
  - c) List of Dimensional Inspection Requirements (data sheets)
  - d) Copy of Suppliers Shipping Document.

FIGURE 1
PROOF LOADING TEST SET-UP

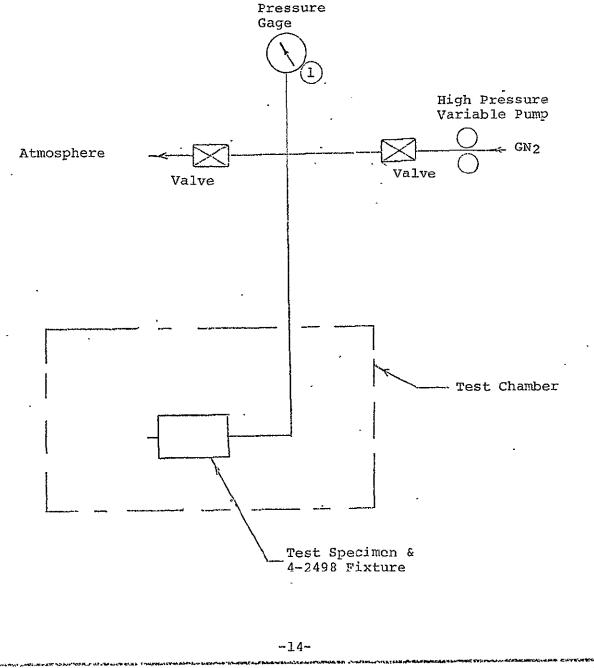
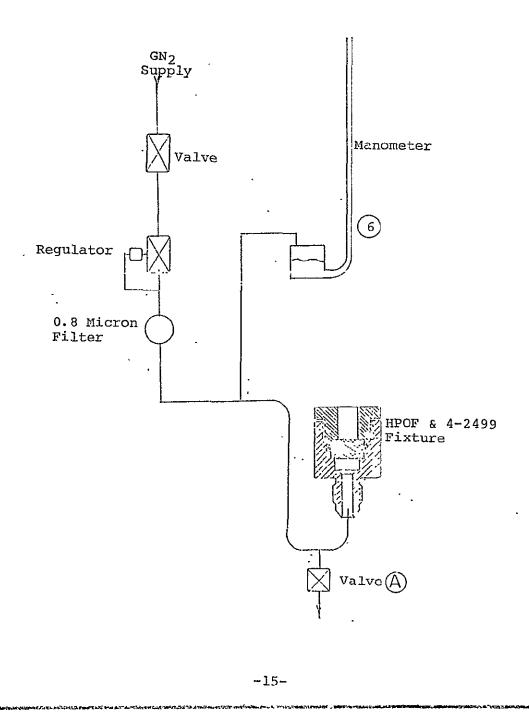


FIGURE 2
BUBBLE POINT TEST SET-UP

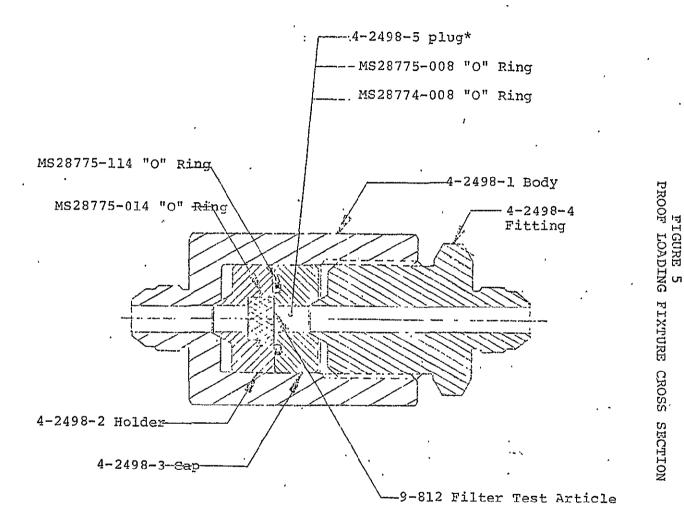


#### FIGURE 4

#### 4A IDENTIFICATION LABEL

WINTER DIV BRUNSWICK CORP.
5223 Imperial Highway Los Angeles, Calif. 70045 Code. 21550
DO NOT OPEN
EXCEPT IN A CONTROLLED ENVIRONMENTAL FACILITY
P/N:S/N
PART NAME HPOF QTY. 1 ea.
Cust. P/N:
CONTRACT NAS 9-14466
CUSTOMER_ NASA
CLEANED PER
LEVEL 25 SERVICE Oxygen
INSP. DATE

4B INTEGRITY SEAL



\*Place smaller diameter of plug toward HPOF (9-812).

TP 259

#### TABLE 3

#### EQUIPMENT & INSTRUMENT LIST

			·
Item No.			
1		Instrument Manufacturer Size Serial No. Range Accuracy Calibration	Pressure Gage US Gauge 6" Dia. 0018 0-20,000 1% 90 Days
	{	Instrument Manufacturer Size Serial No. Range Accuracy Calibration	Pressure Gauge Ashcroft 5" Dia. 0008 0-60 psig 1% 90 Days
3		Instrument Manufacturer Model No. Serial No. Range Accuracy Calibration	△P Transducer System Validyne CDIZ 5101 0-100, 0-300, 0-1000 PSID 1% Prior to Use
4	٠	Instrument Manufacturer Model No. Serial No. Range Accuracy Calibration	Temperature Indicator Barber Coleman Type 7 46H 2317 -300°F to +300°F 2°F 90 Days
<u>.</u> (5)		Instrument Manufacturer Model No. Serial No. Range Accuracy Calibration	Flow Meter Fischer Proter 1/2-27-G-10180 FMK-004B .2 to 3.4 SCFM GN2 1% Yearly

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TP 259

#### TABLE 3

DNA\*

### EQUIPMENT & INSTRUMENTATION LIST (CON'T)

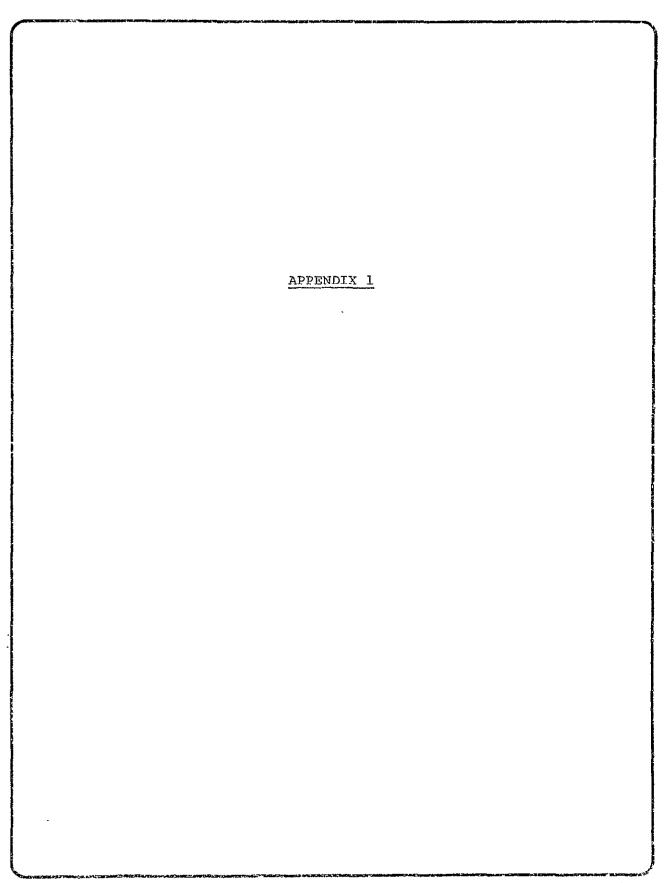
#### Item No.

Instrument Manometer
Manufacturer Meriam
Model No. 30FB25
Serial No. N 24121
Range 0 to 50 in. H<sub>2</sub>O
Accuracy .003 in. H<sub>2</sub>O

Calibration

\*DNA = Does Not Apply

The noted instruments on instrumentation with the same accuracy shall be used for Acceptance Testing.



WINTEC division Brunswick Corporation

147

5223 West Imperial Highway Los Angeles, California 90045 (213) 641-4300 Telex: 67-3105

s,	0,				

#### CERTIFICATE OF CONFORMANCE

Date:		Part Number				
Customer I	. co. 10. q	P.O. Item Number				
Number pai	rts delivered with this shipmen	t				
Shipper No	٥٠	Serial No (s)				
1.	purchase order and specificate were fabricated from materials	its were processed per the above noted ions. Parts manufactured by Wintec s of which physical and/or chemical a file subject to examination.				
2.	Materials furnished by the cus have been in fact used in thei	stomer for the manufacture of parts r manufacture.				
3.	All special processes applied to the above parts have been accomplished by approved sources.					
4.	Units have been cleaned and pa	. ckaged to the following specifications:				
	,	•				
	,					
		BY; QUALTTY ASSURANCE				

# TP 259 WILLEC Wision Brunswick Corporation

SHIPPER NO.

5223 WEST IMPERIAL HIGHWAY . LOS ANGELES, CALIFORNIA 90045 . PHONE: (213) 641-4300 S 0 Н L DATE SHIPPED SHIPPED VIA INVOICE NUMBER SÂLES ORDER NUMBER CUSTOMER P.O. NUMBER CONTRACT NUMBER F.O.B. TERMS: QUANTITY דואט ORDERED SHIPPER BACK THIS TO DATE ORDER SHIPMENT PART NUMBER DESCRIPTION EXTENSION PRICE CUSTOMER INSPECTION GOVERNMENT INSPECTION COMPART INSPECTION

INTETP 259 ALLOWABLE MINTEC CUSTOMER VALUES SERIAL NO. 1831 Inspection CUSTOMER NASA of Product Para 4.1.1 CHINA .320" Length Para 4.1.1 .498 + .000 Reference Only Dia. Para 4.1.1 Inspect E. B. No Cracks Weld or Voids Para 4.1.2 Weight qms 7.0 gms. Max. Para 4.1.3 n Proof Pres- : 0 2 sure Para 4.2 70 7 CUST, P/N Bubble Point 7 7 7 7 Observed Para 4.3 ၂ဂ Rise of Fluid. in Capillary Para 4.3 Fluid Temp. REV. OF Para 4.3 Density of ACCEPTANCE TEST DATA SKEET ATEP 259 9-812 Fluid Para 4.3 Surface Tension of IPA Para 4.3 Standard Bubble Point GOV'T. Para 4.3 REV.

ATP TP -2

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#### APPENDIX B

RESULTS OF ACCEPTANCE TESTS PERFORMED BY WINTEC DIVISION, BRUNSWICK CORPORATION

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It 2 Resorat 12000 = 4.91/m.





APPENDIX C

ORIGINAL

FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA

PAGE: 1

415 psia (nominal) Test Specimen Inlet Pressure Tare Test

DATE: 4/20/76\_\_\_\_

# TABLE 1 FLOW RATE VERSUS ÖIFFERENTIAL PRESSURE

TEST NUMBER 1

PART TO

TEST DESCRIPTION

ŤEST SPECIMEN INLET CONDITIONS

*****	FLOWMETER ONE	****	*****	FLOWMETER TWO	****				- 1
FLOW RATE	PRESSURE (PSI4)	ŤEMP (DEĜ• F)	FLOW RATE (ACPM)	PRESSURE, (PSIA)	TEMP (DEG. F)	PRESSÚRE (PSIÃ)	TEMP	FLOW RATE	
h	45.7	69+0	•16	52.3	70+7	4ñâ.3	69.8	- 626ê. · ·	
0	50.1	6Ŕ <b>.</b> Ť	, žo	57.4	70.8	418.7	69.7	.6278	· -
r	5€.7	6R+4	• ž4	57.4	7ñ.8	475.5	69%6	• 0333	
ŗ	59.6	66•7	• <u>ē</u> 9	58 <u>•</u> 7	69+6	412.9	68.2	. 7418	1
0	52.0	65.2	• <b>4</b> 0	ś7 <b>.</b> 4	68.7	413.5	66,9	.0551	**
0	52.6	64.1	. 49	58.Ī	67.8	418,7	65, 9	.0683	:
0	<b>%2.0</b>	63.6	•59	57 <b>.</b> 4	67.1	477.4	65.4	<del></del>	
n	50.0	63.3	•69	š7 • 4	66.B	476.B	65.Ĭ	16951	
0	52.0	63.3	.80	56.Ž	66.2	472.9	54.7	• <u>ī</u> ġ82	***
ŋ	51.3	63•n	•90	54.9	65.7	413.5	64.3	. Ï <u>T</u> 98⁻	.,
0	51.3	62.7	.90	ŝ4•9	65.3	4 <u>1</u> 5.5	64.0	···· • • • • • • • • • • • • • • • • •	1
0	56.1	65.8	.81	ś4 <b>.</b> 9	65.4	475.5	64.1		
ŋ	52.0	63 <b>.</b> Ĩ	.Ťì	57.4	65.7	417.4	64.4	6973° -	
0	52.0	63.6	•61	<b>57.</b> 4	66.7	475.5	** 64.9**	~ *.ñ848 -	-
0	ج.48	64.3	•50	54•ž	66,8	412.2	65,6	. 1664	
Q	50.1		.41	56.B	67,2	4Ī5 <u>,</u> 5	~~ 66.Õ	0566°	
a	B₹.7	65.3	•31	57.4	67.7	476.8	66.5		ď
Q.	48.8	66+2	• ž\$	54 <b>∙</b> 9	68.5	412.9	67-3	- 0333	·
O	52.0		•21		68.8				
n	52•n	67.4	•13	58.1	69.5	414.2	68.5°		<del></del>
	FLOW RATE (ACFM)  O O O O O O O O O O O O O O O O O O	FLOW RATE (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACFM)  (ACF	######################################	######################################	######################################	######################################	######################################	### ### ##############################	### PRESSURE   PRESSURE   TEMP   FLOW RATE   PRESSURE   TEMP   PRESSURE   TEMP   FLOW RATE   PRESSURE   TEMP   FLOW RATE   PRESSURE   TEMP   PRESSURE   TEMP   FLOW RATE   PRESSURE   TEMP   PRESSURE   TEMP   FLOW RATE   PRESSURE   TEMP   PRESSURE   TEMP   TEMP   TEMP   TEMP   PRESSURE   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TEMP   TE

TABLE 1

TEST DESCRIPTION

PAGE: 2

415 psia (nominal) Test Specimen

Inlet Pressure Tare Test

DATE: 4/20/76

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PART TO

TEST NUMBER 1

TEST SPECIMEN INLET CONFITIONS \*\*\*\* GROSS DIFE: PRESS PRIMARY (PSID) GROSS DIFF. PRESS TYG GROSS NET TARE DIFF\* PRESS ĀVG FLOW RATE (ĀČFM) AVG TEMP DIFF PRESS-SECONDARY PRESSURE (PSID) (PSID) (PSID) (PSID) (DEG. F) (PSIA) ö Ó 40B.J 69.8 .0206 Ò ñ . 0278 69.7 418.7 ô ñ .ŏ333 415.5 69.6 .001 .ñ418 68,2 412.9 0 0.001 .00ī . 7551 413.5 66.9 .001 õ ·0683 0.001 418.7 65.9 0.001 .001 417.4 .0817 65.4 ō .00Ī .0954 0.001 416.8 65.1 Õ 0.002 .002 .1082 412.9 64.7 ō 0.002 .002 .1198 413.5 64.3 ō 0,002 .00ž .1193 415.5 64.0 Ō 0.002 .1072 .002 415.5 64.1 Ô . 1973 .001 0.001 417.4 64.4 .00ī . nB48 0.001 415.5 64.9 ō 0 . 6664 412,2 65.6 ō 0 .0566 0 415.5 66.0 ő ō 0\_ . .0430 416.5 66,5 ō .ñ333 412.9 67.3 0 0 418.1 67.7 .0286 0 0189 0 414.2 68,5 COMPUTED EQUATION: 0 (ACFM) \*#3 (ACFM) \*\*2 + (ACFM) + 0.150933 TARE DIFF. PRESS = -0.000034 - 0.000444 SIGMA = 0.00034

TABLE 1

PAGE: 3

DATE: 4/20/76

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 1

PART TO

TEST DESCRIPTION

415 psia (nominal) Test Specimen Inlet Pressure Tare Test

***	****	****	ŤEST SPI *****	EČIMEN INLEŤ			តិសំសំសំសំសំសំសំសំសំសំ សំសំសំសំសំសំសំសំសំ	****	*******	NET DIFFERENTI	AL PRESS	_
PRESSUR *********		TE	MPERÁŤURE **********	***	***	<b>*******</b>	FLOW RĀŤE,	*******	*****			 .j
KG/SQ CM	PSIA	DEG. K	DEG. C	DEG, F	LITERS/ MIN	ACFM	scFM	KĜ\H <sup>K</sup> GN≨	GN2 LBS/HR	OIFFERENTIAL	PsID	-
8,7,8 <u>\$</u>	408.3	294.2	2 <u>1</u> • 0	69.8	16.2	.0206	.573	1:128	2.488	0.0000	0.000	
29.438	418.7	294.1	21.0	69.Ť·	22.4	.0278	.792	i <u>.</u> 560	39440	0.0000	0.000	_
Ā9 <b>.</b> 210	415.5	294.0	26.9	69.6	26.6	.0333	.940	1.852	4.083	0.0000	0.000	
29.028	412.9	293.3	20.1	68.2	33.3	•0418	1.177	5•317	5•ī08	0.0001	0.001	.1
29 <sub>•</sub> 073	413.5	292.6	19.4	66.9	44.1	.0551	1.558	3:069	6•765	0.0001	0.001	
29,438	418.7	292.0	18,8	65,9	55.5	.0683	1.961	3.861	8.512	0.0001	0.001	
29,347	417.4	7.195	18 <b>.</b> 5	65.4	66.3	.0817	2,340	4.607	10.157	0.0001	0.001	-
29.392	416.B	291.5	is.4	65.Ī	77.3	.0954	2,731	5.378	11.857	0.0001	0.001	
29.028	412.9	291.3	18.2	64.7	86.9	.1082	3.069	6 <u>+</u> 043	13.323	0.0001	0.002	
29.073	413,5	291.1	ĨB,0	64,3	96.5	.1198	3,408	6.710	14.793	0.0001	0.002	Ţ
29.21n	415.5	29 ñ • 9	ĨŤ.8	64.ò	96.6	.1193	3.410	6.714	14.50Ž	0.0001	0.002	•
<u> </u>	415.5	291.0	17.8	64.1	86.7	.1072	3.063	6.032	13.Ž98	0.0001	0.002	
29,347	417.4	291,2	18.0	64,4	79.1	.0973	2,792	5.497	12.119	0.0001	0.001	
29.210	115 <u>.</u> 5	291.4	į8,3	64.9	68.5	.0848	2,420	4,765	10.5 <sub>0</sub> 4	0.0001	0.001	
28.982	412·2	291.8	Ĭ8.6	65+6	53.2	.0664	1.877	3.697	8 • 150	0.0000	0.000	_
ź9,210	415.5	292.0	18.9	66.0	45.6	0566	1,611	3,173	6,994	0.0000	0.000	ij.
29.302	416.A	292.3	<u> </u>	66,5	34.8	.0430	1.229	2.419	5+333	0.0000	0.000	
29.028	7,12.9	292•8	Ĩ9.6	67.3	26.7	.0333	.941	1.852	4+083	0.0000	0.000	
29,393	418.1	293.0	19.9	67.7	23.2	.0286	.818	1.611	3,551	0.0000	0.000	
29•11 <sup>9</sup>	414.2	293.4	20.3	68.5	15.1	.0189	,534	1.051	2.318	0.0000	0.000	-
AVG. 29.183	AVG. 415.1	AVG. 292.3	AVG. 19.1	AVG. 66.4		-	-	- <b>.</b>			<del></del>	
DEV134	DEV. 2.0	DEV. 0.8	DEV. 0.8	DEV. 1.4								•••

PAGE:	±
DATE:	4/20/76

## TABLE 2 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 1

PART IN

TEST DESCRIPTION

700 psia (nominal) Test Specimen Inlet Pressure Tare Test

FLOWMETER CONDITIONS ŤEST SPECIMEN INLET CONDITIONS FI OWNETED ONE MI AUMETED TWA

FI OWMFTER ONE			****	FLOWMETER TWO	****		• •	]
FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG. F)	FLOW RÄTE (ACFM)	PRESSURE. (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	AVG: FLOW RATE: (ACFM)
¢.	57.3	74.n	•13	Ś7•Ś	76.Ż	697.4	75.1	•0108
13	58.2	72.7	.21	58,8	75.9	697.4	74.3	.0180
r),	51.3	71.7	. 5̄5	§7.€	7š.8	697.4	73.8	. 020B
ũ	¤1.0	70.5	•41	57.5	75.4	689,4	73.0	•0255
٩	49.1	69.5	• <b>4</b> 0	54.9	74.8	689.4	72.ī '	; 63 <u>15</u>
ñ	49.7	6Á•3	• Š0	5 <b>4</b> ∙9	74.1	685.4	71.2	.0402
o	47.2	66•Ê	•60	<b>53 • 0</b>	73.0	693.4	69,9	0455
0	57.0	6Š.2	.72	<b>5</b> 5∙6	78.9	697.4	68.1 -	0576
f	52.2	64.1	.B1	56.2	69. ñ	789.4	66.5	• 0643.
0	49.7	64.8	•90	53•7	68.4	694.4	66.1	• ô6 <b>97</b> "
0	49.7	63.6	•90	53.7	67.9	693.4	65.Ť	. ŏ59Ť
ų	49.7	64.7	.80	54∙3	67.9	78944	65.8	• 05 I A
Û	49.7	64.1	.69	54.9	68.ī	697.4	66.1	
٥	49.7	64.6	.60	54.9	68.6	697.4	66.6	
0	51.3	65•ĩ	•49	§6.ē	69.1	7ñ1.4	67.1	.0397
0	49.7	65∙8	•40	55•6	69.7	765.4	67.B	
a	5A.3	66.5	•30	<b>56</b> ∙9	7ñ.3	7ñ1.4	68.4" "	ô245; ·
ŧj	51.0	67 <b>.</b> ž	•ž5	š7•\$	7ñ•9	7ีกิจิ.4	69.1	• 0204-
0	<b>51.0</b>	6Á.Ö	٥۾.	5 <b>7</b> ∙5	71.6	697.4	69.8	. olay
ŋ	50.3	69.1	.ĩ2	\$ <b>7.</b> \$	7ã.4	7ñī.4	70.6	.0108:
			4				·	

ŗ

TABLE 2

PAGE: 2

DATE: 4/20/76

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 1

PART TO

TEST DESCRIPTION

700 psia (nominal) Test Specimen Inlet Pressure Tare Test

RESSURE (PSIA)	AVG TEMP (DEG. F)	AVG FLOW RATE (ĀCFM)	<sub>G</sub> ĀNSS DIFF, PRESS PR₹MARY (PSID)	GROSS DIFF. PRESS SECONDARY (PSIn)	TVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSIO)
697.4	75.1	.0108		ō		0	0
697.4	74.3	.0180		ŋ		0	0
697.4	73.8	.0208		0		0	Q
689.4	73•0	.0255		ń		0	_ 0
689,4	72.1	.0315		ô		0	· • •
685.4	71.2	.0402		ń		9	0
693.4	69.9	.0458		õ		Ò	0
697.4	68 <b>,</b> î	.ñ576		•001		õ	-0.001
749+4	66,5	. 9643		•001		. 0	0.001:
693.4	66.1	, ñ6 <b>97</b>		•001		Ţ Ö Ţ	0.001
693.4	65,7	. 1697		•001		0	0.001
719.4	65.8	.ñ614		•001		ō .	0.001
697.4	66.1	.ñ545		ô		0	0
697.4	66.6	.0472		n		0	0.
701.4	67•Ī	.0397		0		Ó.	0
705.4	67.8	•0311		ń		ō	0
701.4	68,4	,ñ2 <b>4</b> 5		ñ		0	0
709.4	69•1	.0204		ň		Ŏ	_ 0
697.4	69+8	.nī67		n		O	0 _
701.4	70.8	.0102		Q		0	0
COMPUTED E	QUATION:						
	TARE DIFF, PRESS =	0.000360 -	0.033161 (4	CFM) + 0.633359	(ACFM) ##2 +	0 (ACFM)	<u></u>
						SIGMA =	0.000184

PAGE: 3 4/20/76

### TABLE 2 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 1 PART IN

DEV. .355

DEV. 5.0

DEV. 1.4

DEV. 1.4

DEV. 2.6

TEST DESCRIPTION

700 psia (nominal) Test Specimen Inlet Pressure Tare Test

DATE:

TEST SPECIMEN INLET CONDITIONS NET DIFFERENTIAL PRESS ប អ្នកស្រុកសង្គម្នេញ មានស្រុកសង្គម្នាក់ ស្រុកសង្គម្នាក់ សង្គម្នេកសង្គម្នេកសង្គម្នេកសង្គម្នេកសង្គមន្តិក្នុងការបានសង្គមនុស្ស សង្គមនុស្ស ្គមនុស្ស សង្គមនុស្ស សង្គមនុស្ស សង្គមនុស្ស សង្គមនុស្ស សង្គមនុស សង្គមនុស្ស សង \*\*\* TEMPERATURE. PRESSURE FLOW RATE \*\*\* \*\*\*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* KG\HĞ GNŞ 0N2 LITERS/ KG750 CM KG/SQ CM LB5/HR DIFFERENTIAL PSID PSI A DEG. K DEG. c DEG. F MIN ACFM SCFM 49.033 497.4 297.1 23.9 75. Ĩ .0108 .509 1.002 2.210 0 0 14.4 49.033 497.4 ,846 1.667 3,674 296.7 23.5 74.3 24.0 .0180 0 497.4 1.934 4.263 49.033 73.8 ,982 296.4 23.2 27.8 .0208 5.166 689.4 22.8 1,190 2.343 48.469 295.9 73.ñ 33.7 .0255 689.4 2.897 48,469 7ż.ï 1,471 6.387 295.5 22.3 41.6 0315 48,188 685.4 71.2 1.871 3.685 8.123 294.9 27.6 53.0 5040 294.2 21.1 2,162 0 48.751 693.4 0458 4.258 9.387 0 69.9 61.2 .0576 0.0001 49,033 697.4 68.Ï 5.397 11.899 0.001 293.2 20.0 77.6 2,741 49.877 709.4 3,122 -6•14<u>B</u> 13.554 292.3 19.2 66,5 88.4 ..1643 0.0001 0.001 0.0001 0.001 48.751 693.4 ີ 18.9 .0697 3.312 6.521 14.377 1.595 66.1 93.8 48,751 693.4 6.526 14.388 291.9 18.7 65.7 93.8 0697 3,314 0.0001 0.001 49.877 709.4 291.9 18.8 65.B .0614 2,985 5.878 12.959 0.0001 0.001 84.5 49,033 497.4 .0545 5.127 11.302 292,1 18.9 66.1 73.7 2.604 Û 0 49,033 697.4 9,792 0 0 292.4 ĵ9.2 66.6 63.9 0472 2,256 4.442 49.314 701.4 67.1 3.747 8.261 0 0 292.7 19.5 .0397 1,903 53.9 Ó 49,596 705.4 19.9 67.8 2.955 0 293.0 .0311 1,501 6.515 42.5 0 49,314 701.4 0-293.4 50.5 68.4 .0245 1,174 2.311 5.695 33.2 49,877 709.4 1.938 - 0 293.7 25.6 69. Ì .984 27.9 .0204 4.272 49,033 697.4 294.2 21.0 ī.564 0 0 69.8 .0767 .794 3.448 22.5 49.314 701.4 294.7 21.5 70.8 0102 956 . 0 0 13.8 .486 2.108 AVG. 49.089 AVG. 698.2 AVG. 293.9 AVG. 20.7 AVG. 69.4

## TABLE 3 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 1

PART TE

TEST DESCRIPTION

1000 psia (nominal) Test Specimen Inlet Pressure Tare Test

3	<b>ទង់ទទ</b> ១១១១១១១	<b>អ្នក់ខ្លួនសង្កុំខ្លួនស្</b> ងស	FLOWMETER	R CONDITIONS	*60000000000000000000000000000000000000	*****	ŤEST SPECIMEN INLET ČONĎĮTÍONS				
	****	Fi'OMMETER ONE	计条款法序接收格标符	***	ELOWMETER TWO	***		- 17.8	# 7 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		
	FLOW RATE (ACFM)	PRESSURE (PSIA)	TEILD (DEG. F)	FLOW RẬTE (4CFM)	PRESSURE, (PSIA)	TEMP (DEG. F)	PRESSURE (PSIX)	AVG TEMP (DEG. F)	FLOW RATE: (ACFM)		
	3	51.2	67.9	•12	57 • 4	69.6	984.8	68.8	à		
	۵	57.2	66.1	•21	57.4	69.9	7.186	68.0	. 181.		
l,	t	57.2	64.5	•26	57.4	75.2	988.8	67.3	0151		
	Û	50.5	63.2	•31	57.4	7ñ.\$	995.8	66.7	70179		
	p	51.2	61.3	•39	57 <b>.</b> 4	76.3	1ñ20.8	65.8	.0220		
	0	54.5	0.03	•49	Ŝ6•2	70.2	988.7	65.1	.0281		
	٨	49.9	59•ñ	.59	54.9	76.2	986,B	64.6	- 6329		
	n	54.5	5A•ไ	• 70	55.5	70.2	972.7	64.1 -	• 0 • 0 0		
í	9	48.6	57.6	.81	\$ <b>2 •</b> 9	70 = ô	984.8	63.8	*0433		
	ņ	51,2	56.3	.93	54.9	69.9	1ñño.8	63 <b>.</b> 1	.0510 y		
	٦	<b>4</b> 4.5	55∙8	.93	54.3	69.9	992,8	62.9	• 0506		
	c	47.4	56∗1	.80	š1.ô	69.9	996.8	63.1	.0410		
	15	.a.9	56.5	•71	54.9	69.9	1800.8	63.2	-03B8		
	Ω	49.9	57∙ व	•59	54·9	70.0	975.7	63,7	.0334		
i	C	51.2	58.0	• 49	57.4	70.0	992.8	64.0	.0286		
	f*	52.5	50•0	• 40	57.4	7ā•ñ	988.8	64.5	, 0230°		
	Ŋ	r. 1 • 2	62.5	.41	57.4	76.1	984.8	65.2	.0148		
	o o	48.6	61.7	• 25	54.9	71.2	968.7	66.0	.0142		
	t,	5 . S	62.7	•20	57.4	78.3	1716.8	66.5	.0111		
	ħ	49,9	64.7	.;2	56 <b>∙</b> 2	7ő•4	988.8	67.6	.0071		

TABLE 3 FION RATE VERSUS DIFFERENTIAL PRESSURE PAGE: 2

DATE: 4/20/76

TEST NUMBER 1 PART TE TEST DESCRIPTION 1000 psia (nominal) Test Specimen Inlet Pressure Tare Test

TEST	< PEÇ j	rEN	INLET	CONDIT	TONS
****		****	****	***	*****

PRESSURE (pSl <sub>u</sub> )	AVG Temp (Deg. F)	AVG Flow Rate (ACFM)	GÖNSS Diff, Press Primary (Psid)	gross Diff. Press Secondary (PSIO)	AVO GROSS DIFF, PRESS (PSIO)	TARE Dīff, PRESS (PSID)	NET DÍFF. PRESS (PSID)	1
984,5	68.8	.0072		-0.000		n	ó * 00 ō	
987.7	68.4	•6121		-0.00ô		0	0.000	
948.8	67 <b>•</b> ↑	.6151		-0.000		0	0.000	
992•8	66.7	.ŋï79		-0.000		0	0,000	
102).0	65.8	.0220		.00ï		0	.001	į
980.1	55.1	.0281		.001		0		
988.8	64.6	¢2Eñ.		•001		0	001	
972.7	64.1	.ñ400		.001		n	.00 <u>1</u>	
944.0	63.8	.0433		.001		0	.001	
1000.5	63.1	.0510		.001		0	.001	
992.8	62.9	.0506		•00Ĩ		0	.001	1
996.8	63.1	.0410		.001		0	.001	
1000.8	53.2	.ñ388		.001		0	.001	
972.7	63.7	.0374		-0.000		ò	0,000	
992.8	64+1	.6286		-0.000		ō	0.000	
948.8	64.5	•ô230		-0.000		0	0.000	
984.5	65.2	.0178		-0.000		0	0.000	d
968.1	66.0	.ñ142		-0.000		ö	0.000	
1116.8	66.5	.0111		-0.000		n	0.000	
988.8	67.6	.ã071		-0.000		, 0	0.000	<b></b>

COMPUTED EQUATION:
 Tyre DIFF. PRESS = -0.000164 \* 0.012693 - (ACFM) + 0.248070 - (ACFM) \*\*2 +

0 (ACFM) \*\*3

SIGMA = 0.00033

PAGE: 3 DATE: 4/20/76

1000 psia (nominal) Test Specimen

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION

### ( COU MAIR ACKNOW DILLERANTY LINESSON

PIRT IF

64.6

64.j

Dev. 1.5

TEST NUMBER 1

18.1

17.8

Dev. 0.8

69.517

68,39a

Dev. 0.665

n88 g

072.7

Dev. 9.4

291.3

291.1

Dev. 0.8

TABLE 5

			,,,	or manager 1	1 100	•	, C / C	C00/(1/ /1/)/(		ressure Tar	e Test	
,	*****	****	***********	TEST S	PECIMEN INLE	T CONDITION	5 ###########	តំ <i>ក</i> ស្នបសេសស្នា <u>ស</u> ំ	******	ពេលកំពុកកក្	NET DIFFERENTI	
	PRESS	986 984 986	, TEMPERSTURE			****	******					
	KG/SG CM	Alka	DEG. K	DEG, C	DEG. F	LITERS/ Min	4.CFM	scFH	GNŽ KĢ∕H∺	GNŻ LBS/HR	KG/SQ CH Differentia <u>l</u>	p <b>SI</b> <u>0</u>
	69.235	984 a	293.6	21.4	68.B	13.8	1072	.487	,958	2.[13	0.0000	0.000
ı	68.954	a89.7	293.2	20.0	68.0	22.9	.0121	.810	1,594	3.514	0.0000	0.000
	69,517	986.8	292.8	19.6	67.3	28.9	.0151	1.020	2.008	4.426	0.0000	0.000
	69.799	293°U	292.5	19.3	66.7	34.4	179	1.216	2.394	5.279	0.0000	0.000
	71.771	1,20,4	291.9	18.8	<b>6</b> 5.8	43.5	.0220	1.537	3.025	6.670	0.0001	.001
	68,954	081.7	291.6	18,4	65,1	53.6	.0281	1.894	3,729	8.555	0,0001	001

63.3

75.8

69.235 c84 3 17.7 294.8 63.8 83.1 . 9433 2.935 5.778 12,739 0.0001 .001 70,362 Lrov.A 17.3 290.4 63.1 99.5 -.0510 3,515 6.921 15.258 0.0001 .001 69.799 4.Sep 29 .3 17.1 62.9 3,462 6.816 15.27 0.0001 .001 98.0 .0506 70,080 996 A 39ñ.4 17.3 5.549 63.1 79.8 2.818 12.534 0.0001 .001 .0410 70,362 291.5 17.4 1009.8 63.2 .0388 2,676 5.269 11,616 0.0001 75.8 .001 68,390 072.7 295.8 17.6 63.7 63.4 .0334 2.238 4.40? 0.0000 0.000 9.716

.0329

.0400

2,234

2,675

4.399

5.26?

9.698

11.613

0.0001

0.0001

.001

.001

69,799 092.13 294.9 17.8 0.000 64.0 1.956 3.851 0.0000 55.4 . no86 8.489 69,517 088 8 291.2 18.1 64.5 , 9230 1.561 3.973 6,775 44.2 0.0000 0.000 69.235 284.8 291.6 18.4 65.2 .1178 2.375 34.2 1.206 5,236 0.0000 0.000 68.198 966.7 292.0 18.9 66.0 .014g 1.859 0.0000 26.7 .944 4.599 0.000

71.489 1.16 A 292.3 19.2 66.5 21.8 0111 .771 1.518 3,348 0.0000 0.000 69.517 088.A 292.9 19.8 67.6 .0071 .477 .939 2.070 13.5 0.0000 0.000 Avg. 69.601 Avg. 990.0 Avg. 291.6 Avg. 18.5 Avg. 65.2

## TABLE 4 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER F

PART TÈ

TEST DESCRIPTION

2900 psia (nominal) Test Specimen Inlet Pressure Tare Test

PAGE: 1 DATE: 4/23/76

TEST SPECIMEN INLET CONDITIONS FLOWMETER CONDITIONS FLOWMFTER ONE FLOWMETER TWO

***	***	***	***	*****				
FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG. F)	FLOW RATE (ACEM)	PRESSURE, (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	AVG FLDW RATE (ACFM)
r	54.2	78+7	+14	54•n	83•n	2868.0	80.9	.0056
e	45.7	77.3	•21	45 <b>e</b> 2	87.8	2791.2	80.0	.0034
e	49,5	74.7	.26	45.n	81.9	2859.9	78.3	-0041
ţ,	44.6	71.0	.30	43.9	88.8	2859.9	75.9	• 0047
υ	44.6	67.5	• 40	43.7	79.2	2855.9	73.2	.0061
O	44.2	61.8	.50	43,3	76.4	2851.8	69.1	.0076
a	43.4	57•9	•60	42.2	73.8	2847.8	<b>65</b> ₿	- 00 <del>89-</del> · ·
0	4ñ.0	52.0	.70	38.6	68.7	2698.3	60.3	.0100
6	4A • 0	63.2	•73	47.5	73.7	2868.1	68,5	<b>.</b> 0022
e	45.5	62 <sub>+</sub> 8	•20	45.2	77.4	2868.0	68.1	
o	<b>45.3</b>	61.9	•26	44.7	72.9	2863.9	67.4	•0040
ń	46.6	6i •9	•31	46.A	72.3	2863.9	66.6	.0049
n	49.B	59.1	•3?	43•Ī	77.4	2859.9	65.2	70055
ถ	45.7	56.9	• 45	44.8	79.0	2859.9	63.4	.0071
r.	44.4	57.5	•55	42 • 0	67.6	2855.9	60.6	.0081
0	44.9	5ñ•3	•60	43.5	64.8	2855.9	57.5	10001
ħ.	44.4	47.9	.65	42.9	62.1	2851.8	55 <b>.</b> 0	.0099
n	43+4	46+7	•70	42+0	60 <b>-4</b>	2847.8	53.6	.6103
0	42.1	45.7	.80	40.5	58.9	2843.7	52.3	ō114 ·
า	41.9	44.5	•91	39.5	57.1	2863.9	50.8	.0125

TABLE 4
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

2900 psia (nominal) Test Specimen Inlet Pressure Tare Test TEST DESCRIPTION TEST NUMBER F PART TE TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*\* GROSS DIFF. PRESS PRIMARY GROSS DIFF. PRESS NET DIFF. PRESS AVG . VG ÃVG GROSS TARE PRESSURE SECONDARY DIFF. PRESS DIFF. PRESS TEMP FLOW RATE (PSIn) (PSID) (PSID) (PSID) (PSIA) (ACFM) (PSID) (DEG . F) -0.001 -0.â01 -0.000 -0,001 .0026 2868.0 80.9 -0.001 -0.001 2791.2 .0034 -0.001 -0,000 80.0 .001 .001 0 , 2859.9 78.3 .0041 .000 .001 ,001 2859.9 75.9 .0047 .500 .001 .001 Ó .001 .0061 006 .001 .001 0 2855.9 73.2 .001 2851.8 69.1 .0076 .000 .001 .001 0 .000 2847.6 .0089 .000 -0.000 .000 65.8 0 .001 .000 .001 .001 0 2698.3 60.3 .0100 2868.0 68.5 .0022 . 500 -0.000 .000 0 ..... .000 .000 0 2868.0 68.1 .0032 .ñoo -0.000 -0.000 .000 .000 0 2863.9 67.4 .0040 .000 .000 2863.9 66.6 .0049 .000 -0.000 .000 .000 2859.9 65,2 .0056 .600 -0.000 .000 .000 2859.9 .òo71 .600 -0.000 .000 0 63.4 2855.9 -0.001 .0081 -0.001 -0.000 -0.001 60.6 Q --0.001 -0.ôgl -0.00i -0.001 2855.9 57.5 .0091 2851.8 55.0 .0099 -0.501 -0.00i -0.001 0 -0.001 -0.001 -0.001 2847.8 53.6 .0103 -0.001 -0.001 0 2843,/ 52.3 .0114 -0.001 -0.00ī -0.001 -0,001 2863.9 50.8 .0125 -0.00l -0.00ī -0.001 -0.001 COMPUTED EQUATION: 0 (ACFM) \*\*3 TARE DIFF. PRESS = -0.001246 0 \* 0.488453 0 (ACFM) + -40.072254 0 (ACFM) ++2 + SIGMA = 0.000700

PAGE: 3 TABLE 4 DATE: 4/23/76 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER F PART IF

TEST DESCRIPTION 2900 psia (nominal) Test Specimen Inlet Pressure Tare Test

***	***	****	TEST S	PECIMEN INL	EŤ CONDITIONS	***	NET DIFFERENTIAL PRESS				
PRESS!			TEMPER, TURE	***	***	FLOW RATE					
KĢ/SQ CM	PSI <sub>4</sub>	DEG. K	DEG. C	DEG. F	LITERS/ Min	a CFM	SCFM	kë\Hk gn≤	GN2 LBS/HR	KG/SQ CM Differentiäl	PSID
201,639	2965.1	300.3	27.1	80.9	13.9	.0026	.491	•467	2.133	~0.0000 **	<b>~0,001</b>
196,242	2791.2	299.9	26,7	80.0	17.9	.0034	.633	1.245	2.747	~0.0000	-0,001
201.071	2959.9	298,9	25.7	78.3	22.0	,9041	•777	1.530	3.372	.0000	.001
201.071	2859.9	297.6	24.4	75.9	25.4	.0047	.897	1.765	3.893	.0000	.001
200.787	2455,9	296.3	55.9	73,2	33.5	,4061	1,182	2.32?	5.130	.0000	ioo.
200,503	2851,8	293.8	2n•¢	69.1	42.0	, 2076	1,485	2.923	6•445	.0000	.001·
200.219	2847.8	292.0	18.8	65.8	49.2	.0089	1.737	3.421	7.541	• 0 0 0 0	.000
189.706	2698.3	288.9	15.7	6n.3	52.7	.0100	1.861	3.663	8.077	.0000	.001
201.639	2468°v	293,4	24.3	68.5	12.2	.1022	.431	.849	1.871	•0000	.000
201.639	2468.	293.2	20.0	68 • j	17.7	, 2032	,626	1 <u>•</u> 232	2.717	.0000	,000
201.355	S463.9	292.8	19.7	67.4	22.3	.0040	.786	1.548	3.413	•0000	•00ô
201.355	2263.9	292,4	19.2	66.6	27.2	• 1049	.962	1.894	4•j75	•0000	.000
201.071	2959.9	291.6	18.5	65.2	31.1	.0056	1.097	7 <u>.</u> 161	4.763	.0000	.000
201.071	2,59.9	290.6	17.5	63,4	39.4	.0071	1.391	2.739	6∙ <b>∂3</b> 8	.0000	.000
200.787	2855.9	289.0	15.9	6 <sub>0</sub> .6	45.2	.0081	1.596	3,144	6.930	-0.0000	-0.001
200.787	2a55 <sub>+</sub> 9	287.4	14.2	57.5	51.4	.0091	1.815	3.574	7.880	-0.0001	-0.001
200.563	2.51.8	285.9	12.8	55.a	55.7	•1099	1.968	3.875	8.542	-0.0001	-0.001
200,219	2047.B	285.1	17.0	53.6	58.3	.0103	2.057	4,051	8.930	-0.0001	-0.001
199,935	2843.7	284.4	11.3	52.3	64.9	.0114	2,291	4.512	9,947	-0.0001	-0,001
2 <sub>01</sub> ,355	ZR63.9	283 <b>.</b> 6	ាក្∙ទ ក្នុងស្នង	5 <sub>0</sub> .8	71.8	.0125	2,535	4.991	11.504	-0.0001	-0.001
200.148	2,446.8	291.8	18.7	65,6							
1.456	20.7	4.0	4•ព	7.2	DEVIATIONS						

PAGE: 1 DATE: 8-25-76

TABLE 5

### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5

FLOWMETER CONDITIONS

PART 22C

CLEAN CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TEST SPECIMEN
(S/N 022) INLET PRESSURE = 415 PSIA NOMINAL.

TEST SPECIMEN INLET CONDITIONS

	*****	******	********	******	******	*****	******	*******		
	******	FLOWMETER ONE	*****	******	FLOWMETER TWO	****				
	FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG <sub>e</sub> F)	FLOW RATE (ACFM)	PRESSURE, (PSIA)	T <sub>FMP</sub> (DEG. F)	PRESSURE (PSIA)	TEMP (DEG. F)	FLOW RATE (ACFM)	
	.70	50.1	81.3	•71	48.7	8 <sub>2</sub> ,8	*20+0	82.0	.0829	
ľ	<b>.</b> 60	50 <b>.</b> 9	81.5	•60	49.9	82.7	419.4	81.9	•0721	ΟÚ
ļ	•50	50.7	ai <u>.</u> ı	•50	49.9	n2.5	419.4	81,8	<u>.0603</u>	
.	+41	50.5	8 <u>ñ±</u> 9	<b>-40</b>	49.9	82.5	418.7	81.7	• <u>04</u> 86	
ij	•31	50.3	8ถ่ฐ9	• 30	50 • Ï	82.5	418.7	81.7	• p369	0
ļ	• 26	50.3	81 <u>±</u> Ï	•25	49.9	H2.6	418.7	91.9	•0306	
	•21	50.1	81 <u>*</u> 1	•20	49.9	45*6	418.7	81.6	+0247	
į	•14	÷0+3	81:3	•13	50 <b>-</b> 1	82.8	418.7	82,0	+9164	
	. 15	49,5	BīţS	+14	49.5	45.8	41847	82,2	,0169	
1	• 55	50.5	81,5	• 21	50.2	9.5.8	418.7	82.2	-0262	
Ì	• 26	50.3	81:3	• 25	50•Ī	82+8	418,7	82.0	•0311	
;	•32	_ 50+3	8ï:3	•31	49.9	8,5,4	418.i .	82.0	.0374	90
i	• • • • •	49.7	8 <u>1°</u> 1	<b>.4</b> 0	49.3	82.7	418+i	81.9	.0482	ŷ <b>u</b>
İ	.51	20 <b>.1</b>	80.9	•51	49.3	42 <b>.</b> 5	417.4	81,7	.0604	
	•59	49.9	80 ± 9	•60	48.9	H2.4	<b>4</b> 16.8	81,6	.0704	
	.69	50.3	81 • 0	<b>-71</b>	48.9	મ <b>ટ્</b> ∌ઉ	416.1	81.6	• 0829	
- 1										

₩.

#

TABLE 5

CLEAN CONDITION - FLOW RATE VERSUS

PAGE: 2 DATE: 8-25-76

### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

		TEST HUMBER 5	PART 22C	TEST DESCRIP	TION DIFFERENTIA	TION - FLOW RATE Y L PRESSURE. TEST NLET PRESSURE = 4:	SPECIMEN	•
TEST SP	PECIMEN INLET CO	NDITIONS		•				
PRESSUME (PSIA)	AVG TEMP (DEG. F)	A <sup>V</sup> G FLOW R <sub>A</sub> TE (ACFM)	GROSS DIFF. PRESS PRIMARY (PSID)	GROSS DIFF. PRESS SECONDARY (PS10)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	NEŤ DIFF <sub>e</sub> PR <sub>E</sub> SS (PSID)	
420.0	85-0	• 0889	295.292	295.292	295.292	• 001	295.291	
419••	81:9	•0721	214.385	214.385	214.385	•001	214.384	E
419.4	81.8	• 0603	159.709	159.749	159.709	•000	ī59.7 <sub>0</sub> 8	_
418.7	81+7	• 0486	115.778	115.778	115.778	• 000	115.777	
418.7	81+7	• 9369	80.239	80.697	89.468	•000	80.467	Ç
418 <sub>e</sub> 7	81.8	•0306	63.281	63.631	63.456	•000	63.455	Ţ
418,7	81.8	.0247	48,245	48,776	48,51 <u>î</u>	.000	48 <sub>4</sub> 510	•
418,7	82.0	.0164	30,476	30.591	30.533	-0.000	30,533	
418.7	85.5	•01 <sup>69</sup>	31,578	31.741	31.659	•000	31,658	
418.7	82•2	• 0262	52.254	52,885	52.569	•000	52.569	
418.7	82+0	-0311	64.65B	65,211	64.934	•000	64,933	
418.1	82+0	.0374	81.476	81,961	81.719	•000	81.718	
418,1	81.9	.0482	115.778	115,778	115.77 <u>ë</u>	•000	ĨĬŚ• <i>ŦŦ</i> Ť	Ū
417.4	81.7	.0604	161.605	161.699	161.605	•000	161.604	
416.8	81.6	.0704	210.276	210.276	210.276	•001	210.275	
416,1	81.6	•0829	297.505	297.515	297.505	•001	297.504	

JARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFH) + 1.50933E-01 (ACFH) +2 +

0 (ACFM) ##3

PAGE: 3 DATE: 8-25-76

TABLE 5 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PART 22C TEST NUMBER 5

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TEST SPECIMEN (S/N 022) INLET PRESSURE = 415 PSIA NOMINAL.

	********	*****	*****	TEST 5	PECIMEN INL	EL CONDITION	5 *******	NET DIFFERENTIAL PRESS					
	PRESSU	TEMPERATURE			*****	FLOW RATE							
	KG/SQ CM	PSIA	DEG. K	DEG. C	DEG. F	LITTOS	^ CFM	SCFM	KĞ/HĞ GN2	GN.> LBS/HR	KG/50 CM DIFFERENTIAL	PSID	
	29.530	420+0	301.0	27.8	85.0	65 <sub>4</sub> 6	• u829	2.317	4,563	10.059	20.7611	295.291	
Ü	29,484	419.4	300.9	27.7	81.9	56.7	.,721	2.010	3.958	8.727	15.0727	214,384	*4
	29.484	419.4	300.8	27.7	81.8	47.3	.ე6ო3	1,684	3,316	7.311	11.2286	159.708	
ĺ	29,438	418.7	300.8	27.6	81.7	37.8	<u>.</u> 486	1,353	2,66 <u>4</u>	5,873	8.1400	115,777	
Ň	29,438	418.7	300.8	27.0	81.7	28,7	• 1369	1.028	2. 123	4,461	5,6574	80.467	**
	2 <sup>9</sup> ,438	418.7	300.8	27.7	ց <sup>յ</sup> գ	23.6	•0300	854	1,681	3.7,5	4.4613	63,455	
	29.438	418.7	300.8	27.7	81.8	19.1	.0247	.689	1.356	5,489	3,4106	48,510	
į	29 <b>.</b> 438	418.7	300.9	27.8	82.0	12.4	.0164	457	•400	1.985	2.1467	30,533	
ļ	29,438	418,7	301.0	27.9	82.2	12.9	*****	<b>.</b> 47 <sub>1</sub>	•927	2+044	2.2258	31,658	
	29.438	418-7	301=0	27.9	82.2	20.2	• p2"2	·73 <sub>0</sub>	1•438	3-170	3.6959	52.569	
	29,438	418.7	301.0	27.8	82.0	24+0	•0311	.866	1.705	3.760	4,5653	64, <sup>9</sup> 33	
ĭ	29,393	418.1	300.9	27.8	82.0	28,9	.0374	1.039	2 <u>*</u> 1.46	4,511	5,7453	81.718	0
	29.393	418.1	300.9	27.7	81.9	37.5	• N442	1.340	2:639	5.818	8.1400	115.777	
	29.347	417,4	300.8	27.6	81.7	47.1	.10604	1.677	3,301	7.278	11.3619	161,604	
	29.302	416.8	300.7	27.6	81.6	55.1	.0704	1.954	3.847	8.481	14.7838	210-275	
	29.256	416.1	300.7	27.5	81.6	65.3	• 0829	2.296	4.522	9.969	20.9166	297,504	
	2 <sup>9</sup> •41 <sup>9</sup>	418.4	300.9	27.7	8 <sub>[•9</sub>								
	•050	•1	•1	-1	-1	DEVIATIONS	s						

## FLOW RATE VENSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 8-25-76 "

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PIPT 225

TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TEST SPECIMEN (S/N 022) INLET PRESSURE = 700 PSIA NOMINAL:

 TEST SPECIMEN INLET CONDITIONS

	FLOWN ETCH ONE	***		FLOSMETER TWO					<del></del>
FLOW RATE (ACFM)	PRF 55U(-F (PS1 <sub>7</sub> )	TFMP (0FG• F)	FLOS RATE	PHFSSURE.	TEMP (OEG. F)	PRESSURE	AVG Temp (Deg, f)	AVG FLOW RATE (ACFM)	
<b>.</b> 87	49,7	23.	•94,	47.6	h5.5	719,6	84.2	• 0597	
<b>∗</b> 79	49.5	53	•9)	47.9	95•	719.6	83.6	.0540	••
•69	5 .?	2)+9	•71	48.9	84.7	719.6	83,3	•0481	7
.61	Þ ·•]	A1 +7	-61	48.9	×4.5	719.6	83,1	•0417	
•50	49.7	5-1-7	* <sub>6</sub> 1	46.9	94.5	719.6	83.1	•0343	•
.41	p. <u>.1</u>	en <sub>e</sub> s	•40	49.5	84.7	719.6	83,4	.0282	G.
.32	49.9	₹ו3	.31	49.3	-4.9	719,6	83 <sub>•</sub> 6	•0Ž20	
.27	49.5	₹* •7	<b>,</b> >6	49.3	P5.1	719.6	83.9	•0181	<del></del>
•21	49.7	87.1	* S +	49.5	≯5 <b>.</b> 4	719.6	84.3	•01 <del>4</del> 4	
14	49.7	33.7	.;3	49.5	F5.6	719.6	84.7	•0095	
•14	۶. ړ۶	P4.4	.13	51.1	F6.1	719.6	85.2	•0095	<del>-,</del>
.24	p∙.l	94.2	• n3	49,9	· 6•	719.6	85,1	•0163	
•27	٥ / • 1	84 • *	- 25	49.9	86.	719.6	85•n	+0181	
.31	50.2	83•4	•35	49.9	86.	719.6	84.9	.0214	<u>F</u> ,
<b>.</b> 42	ל, ול	93.3	• 4 ì	49.7	≻5 <b>.</b> 8	719.6	84.5	-0287	
•51	D: •1	ÿ5.*∂	• 5	49.3	A5•6	719.6	84.2	•0350	
•59	5~.1	BF • 4	• 59	49•1	45.3	715.7	83.8	.0409	>7
•69	49.9	42.	.71	48.5	85	715.7	83.5	•0481	
•77	غ <b>.</b> د	31.4	•41	48.5	-4.4	715.7	82.9	• 0544	•
.84	51.2	19.14	.91	48.3	-4.1	715,7	82.6	.0602	

	TEST JUMBER 5	PART 228	TEST DESCRIPT	TION DIFFERENTI	ITION - FLOW RATE AL PRESSURE. TES INLET PRESSURE -	T SPECIMEN
TEST SPECIMEN INLET	CONDITIONS			and and the second second		
<u> </u>	N.A.	GROSS	GRASS	AVG GROSS	TARE	NET:
PRESSURE TEMP	FLOW RATE - (ACFM)	PRIMARY (PSID)	SECONDARY - (PSID)	DIFF. PRESS - (PSID)	DIFF. PRESS	DIFF PRES
719-6 84-2	<del></del>	<del>152,565</del>	<del>152,565</del>	152-565		<u>152,565:</u>
<del>719,6</del>		193 <del>.</del> 31t	<del>133,31</del> 0	133-310	-0+000	<u> </u>
<del>719,</del> b	184m	··114 <del>,371</del>	114.371	- 114-371		<u> </u>
- <del>719.6</del> - 83.1	·· ~ :0417	· ··· 94 <del>-4</del> 44	95.116	94.760	-0.001	94.780
719.6	<del></del>	73.737	74.283	74-010	-0.001	<del>74</del> -010
719-6 83.4	.0282	- · ·57:852	<del> 58.</del> 5-i	58 - 177	-0.001	58 <b>.177</b>
719:0 83:6 /	0220	43,648	43 <sub>-81</sub> 9	43.73 <u>+</u>	-0.001	43,734
719,6-83,9		34.667	34,726	34+697		34.497
<del>719_6</del>	·	26-498	<del>26,633</del>		-0.00Ĭ	26+556
719.6	<del></del>	16.59	16.562	<u>16√576</u> -		<u>16.576</u>
<b>719.6</b> 85.2-		16,764	16.9.5	16.83 <u></u>	-0.00i	<u>16+83</u> 4-
<del>719*0</del>	.0163	30,496	30.706	30-60 <u>1</u>	-0.00i	30+60 <u>1</u>
	,-181		34,669	34.581	-0+00 <del>1</del>	3Å√É0Ì——
	^214	42,084	42,321	42.203	-0.001	<u>424593;</u>
719,5 44,5		59,231	<del>59,763</del>	<del>59,49?</del>		59 <sub>%</sub> 497
719*6 84*2	0350	·75 <sub>1</sub> 853	76,493	76 <b>-</b> 173		<u></u> 76√173;
		91.618	92,591	92,105	-0+001	92 <b>∵ ì</b> 06:
715.7 83.5-	<del></del>	114-055		1-14+055		
715-7 82.9.	3544	1 <del>35 <sub>1</sub>52</del> 0	135,520	135.520	-0.000	
		157.615	157.615	157,615	<b></b> 0.8000	<u> 157.615</u>
	PRESS-=3-60000E-0	4-+3 <sub>2</sub> 3 <u>1</u> 610E=ŋ2¢	ACEM)	01—(ACEM)***	0-(ACÉM	) <del>* i</del> 3
	4 of 4 letterminate and distance of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of the control of					

		- TE	ST NUMBER 5	PART 2	28	TEST D	ESCRIPTION	DIFFERENT	PIAL PRESSUR	OW RATE VERSUS RE. TEST SPECIME SSURE = 700 PSIA	
***	*********	***	TEST-SP	ECIM <del>EN-I</del> NLE	T-CONDITION	5	*****	****	***	NEŤ DÍFFEŘENŤ	AL: PRES
PRESSI-		44444444	TEMPERATURE	54 <del>55554</del>		****	FLOW RATE		****		
KG/SQ CM	PSIA	DEG. K	DEG. C	DEG. F	L <del>iter</del> s/	ACFM	SCFM	ĸĕ∖Hਔ ŒNS	L'BS/HR	KG/SQ-ČÚ ĎIFFÉRENTIÁĽI	PSID
50.594	719.6	305.2	29.0	84.2	80.4	.0597	2.845	5 <u>•</u> 60]	12.349	ĩo.7264	īš2,565
50,594	719.6	301.8	28.7	83.6	73.1	.0540	2.579	5.079	ĭ1•197	9,3726	133,310
50 <u>.</u> 594	719.6	301.7	28.5	83.3	64.8	•0481	2.298	4.524	9.974	8.04iī	<u>į̃ī4,37</u> į
50,594	719.6	3r1,6	28.4	83.1	55.9	• p417	1.992	3.955	8.647	6,6623	94.760
50 <u>.</u> 594	719.6	301.6	28.4	83.1	45.7	• tr343	1,638	3,224	7,108	5.2034	74.010
50.594	719.6	301.7	28.5	83.4	37.3	.0285	1.345	2.649	5 <b>.</b> 84ó	4.0902	58,177
50,594	719,5	301,8	28.7	83,6	29.1	.0220	1.050	2,067	4,558	3,0748	48,73
50,594	719.6	302.0	28.8	83.9	23,8	.0181	.863	1 • 699	3.745	2:4394	34,691
50.594	719,6	302.2	29.0	84.3	19.0	+0144	.688	1 • 354	2.986	1.8678	26.566
50,594	719.0	302,4	29.3	84.7	12.3	•0095	,452	<b>-</b> 690	1.963	1.1654	<u>16.576</u>
Š0.594	719.6	302,7	29,6	85.2	12,3	•0095	,454	<u>.</u> 89 <u>4</u>	1.971	1.1836	Ĩ6- <u>8</u> 34
50.594	719.6	302.7	29,5	85.1	2î <u>.</u> 5	•0163	•776	1,528	3,368	2.1515	30. <u>6</u> 01
50.594	719.0	302.6	29.4	85.0	23•7	.0181	.860	1.693	3.733	2.4313	34,581
50.594	719.6	302.5	29.4	84,9	28.2	•0214	1.018	2.005	4-421	2.9671	42.203
50,594	719.6	302.4	29.2	84.5	38.0	.0287	1.367	2.692	5.935	4,1831	59, 497
50.594	719.6	302.2	29.0	84.2	46.7	•0359	1,669	3,287	7.247	5.3555	76.173
50,318	715.7	302.0	28.8	83.8	54,5	•0409	1.942	3,824	8+430	6.4756	92.10
50,318	715.7	301.8	28.6	83.5	64.3	• 0481	2.282	4,493	9.906	B.0189	114.056
50.318	715.7	301.5	28.3	82.9	73.6	•0544	2,587	5.094	ĭĭ•230	9.5280	135,520
50.318	715.7	301.3	28•1 -#####	82.6	82.6	•060≥	2.865	5,641	12-436	ĭ1•0815	įš7.615
50 <sub>¥</sub> 539	. 7:8.8 -	30p,0	28.3	84-G	·····						

53

## TABLE 7 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST : DUMBER 5 PART 22A TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS-DIFFERENTIAL PRESSURE. TEST SPECIMEN (S/N-022) INLET PRESSURE - 1000 PSTA

PAGE: 1 DATE: 8-25-76

FLOWMETER CONDITIONS

FLOWMETER CONDITIONS

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	****	FLOWMETER ONE		<b>经共政营益税收收收</b> 销额	FLOWMETER TWO	***				
	FLOW RATE (AÇFM)	PRESSURE (PSI <sub>A</sub> )	TEMP (DEG: F)	- FLOW BATE (ACFM)	PRESSURE, (PSIA)	TEMP (DEG. F)	Pressure (PSIA)	TEMP (DEG. F)	<u>flow Rate</u> (ačřm)	   
	.88	50.2	77.2	•92	48.3	*2•2	1711.9	79.7	• ó43 <b>7</b>	
	.78	50.4	76.5	•81	48.7	81.6	1-Īi.9	79.0	. ē39ē	
	•69	50.4	76.4	•71	49∙1	1.3	1-11.9	78.8	, ó344·	
	•60	49.7	76•4	•61	48.7	81.2	1 15.9	78.8	•0293	†
Ľ	•50	49.9	76.6	•50	49.1	41.4	1111.9	79.ó	. dŽÅ6:	<u>-</u>
	•41	49.9	77 <u>•</u> 3	•41	49.3	81.6	1 15.9	79.5	• 0200	Ì
	•31	49.7	77.8	•30	49.3	~í.9	1-15.9	79.9	•0149	
	.26	50.1	78.3	•52	49.9	r2.3	1115.9	80.3	.0126	
	•55	49.9	78.9	•21	49.7	82.5	1:15.9	80.7	.ÕĨÕÁ·	
	•16	50.1	79•6	•15	49.9	H2.9	1 1 15.9	8 <u>1.</u> ž	•0074	
	•16	50.4	81.0	•15	50.2	83.6	1^15.9	82.3	•0ã75	i
<u></u>	.23	49.5	81.9	•55	49,3	93.6	1"15.9	8ž.3	. ôŢ ċ8	
	•27	49.7	8 .8	•26	49.3	83.6	1-15.9	82.2	• 0130	
	•32	49.7	8 •6	•31	49•3	83.6	1 15.9	82 <b>.</b> Ī	.0151	
 g	.41	49.9	8 •1	•41	49.3	33.5	1*15.9	81.8	.0200	
	•50	49.9	79•3	•50	49.1	83.2	1'15.9	8 <u>1</u> .2	•02451	
	.60	50.4	78•5	•61	49.5	82.8	1711.9	80.6	•0298	
	•69	50.4	77.9	•71	49+1	PZ.4	1111.9	80.Ž	,0343	i
	•78	50.4	77:1	•BU	48•9	81.8	1~11+9	79+4·	• 0387	
	.87	50.2	76,4	•91	48.3	11.1	1011.9	78 <b>,</b> 7	• 0494	
Ľ				,						
_					_				<del></del>	

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: DATE:

8-25-76

1

CLEAN CONDITION - FLOW RATE VERSUS --TEST DESCRIPTION DIFFERENTIAL PRESSURE. TEST SPECIMEN TEST WUMBER 5 PART 22A -- (S/N 022) INLET PRESSURE =-1000-PSIA--3 NOMINAL. TEST SPECIMEN INLET CONDITIONS \*\*\*\*\* eR: SS cRoss AVG GROSS TARE--- NET'--DIFF. PRESS DIFF. PRESS дVG ΛVG DIFF. PRESS DIFF PRESS DIFF. PRESS TEMP SECONDARY PRESSURE FLOW RATE PRIMARY (PŠIĎ) (PSID) \_(PS10)\_\_\_\_ (PStp) (ACFM) (PSID) (PSIA) (DEG. F) īīī.320 .... 111,320 -0.000 111,320 111,320 1011.9 79.7 . 437 964484. .... 96,484 -0.000 96.484 96,484 1011.9 79.0 .0390 82-345 82.345 -0.000 82.095 82,595 1011.9 78.8 .4344 67.805. 67.805 -0.000 68,476 1015.9 78.8 . .293 67,535 54.318... 54.317 -0.000 79.5 .4246 54,132. 54.5 3 163 1011.9 4 -.4Ž+839 42.838 -0.000 .0200 42,917 1015,9 79.5 42.760 \_30.313:.. 30,381 30,313. -0.000 30.245 1015.9 79.9 .0149 24.914 24,876 24.895 -0.000 -1015.9 80.3 ...126 20.029 -0.000 -20+029 -- --20,011 .0104 20.047 1015.9 80.7 13,585 -0.000 13,558 13.611 \_ga74 1015.9 81.2 ... 13.786 13.786 -0.000 13,844 13,732 1015.9 82.3 .0075 . .. 20.835.. 20.835 -0.000 20,869 1015.9 6.2.3 .01:25 20.800 1.1 25,932 **~0.000** 25,932.. 1015.9 82.2 .013n 25.899 25,965 30.918 -0.000 1915.9 1.58 .4151 30.824 31,612 42,665 42,586 42,744 -0.000 .... 1015.9 81.8 .0200ıμ ...54.538. 54.B.B 54.538 -0.000--1015.9 81.2 .::245 54, 258. 68.716 --0.000. 69.022 1011.9 40.6 ...4298 68.410 82-064 81.847 82,280 82.064 -0.000 -.4343 1011.9 150.2 95,853. \_95.853. -0.000 -95,853 95,353 1011.9 79.4 . 387 110,688 110.688. --0-000----..434 . 110.688 1011.9 78.7 Į, TARE DIFF, PRESS = -1.64000E=04 + -1.26930E=02 (ACFM) + 2.48070E=01 (ACFM)\*\*2.+ D. (ACFM) 443.

.134

1.9

•6

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 8-25-76

TEST UMBER 5

PART 22A

1.1

DEVIATIONS

• 6

TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TEST SPECIMEN (S/N 022) INLET PRESSURE = 1000 PSIA

TEST SPECIMEN INLET CONDITIONS

NOMINAL.

NET DIFFERENTIAL PRESS.

PRESS		****	TEMPERATURE	*****	****	***	FLOW RATE		****		
KG/SQ CM	PSIA	DEG. K	ĐEG. G	DEG. F	LITEPS/ MIN	1CFH	SCFM	KĞ∖HĞ GNS	GN2 Las/HR	KG/SQCH Differential	PŠĮD
71.144	1:11:9	299,7	26.5	79.7	83.9	. 1437	2.951	5.810	12.809	7.8266	111.320
71.144	1011.9	299.3	24.1	79.0	74.9	.0390	2,641	5.201	Ĩ1.466	6,7835	96,484
71.144	1011.9	299.7	26	78.8	65.9	• ^ 344	2,332	4.591	10•12i	5.7894	82,345
71.423	1915.9	299.2	26.	78,8	<b>66•1</b>	• 1293	1.994	3.926	8,655	4.7672	67,805
71.144	1 '11 . 9	299.3	24.1	79.0	46.8	245	1.668	3.28 <u>4</u>	7.241	3.8189	54.318
71.423	15.9	299.5	26.4	79,5	37.9	•0200	1.361	2.680	5,909	3.0119	42.839
71,423	1015,9	299,8	26.6	79.9	28.1	.a149	1.013	1,995	4,399	2.1312	30,313
71.423	1015.9	300.0	24.8	84.3	23.6	• '126	.856	1.686	3.716	1.7503	24,896
71,423	1015,9	300.2	27.0	80.7	19.5	.0104	.706	1,391	3.066	1.4082	\$0.050
71,423	1015.9	300.5	27.4	81.2	13.7	• 1074	.501	.987	2.176	.9551	í3,585
71,423	1015.9	301.1	27.9	82,3	13.7	. 2075	•5⋴4	.993	2.189	•9693	13.786
71,423	1015.9	301.1	27.9	82,3	20.1	.0108	.727	1.431	3.154	1.4648	20,835
71,423	1015.9	301.0	27.9	82.2	24.4	013	.881	1.735	3.825	1.8232	25,932
71,423	1015.9	301.9	27.8	82.1	24.4	.0151	1.023	2.014	4.441	2.1738	30.918
71,423	1.115.9	300.8	27.7	81.8	37.6	•020n	1.350	2.658	5.860	2.9997	42.665
71.423	1015.9	300.5	27.4	81.2	46.6	.~245	1.661	3.271	7.210	3.8344	54,538
71 <b>.</b> 144	1011.9	300.2	27.0	80.6	56.6	.0298	2,009	3.956	8.721	4.8312	68.716
71.144	1911.9	299.9	26.6	80.2	65.4	.1343	2.317	4.562	10.058	5.7697	82.064
71.144	1011.9	299.5	26.3	79.4	74.3	•1387	2.619	5.156	11.368	6.739]	95.853
71:144 *****	1611.9	299•1	26±9	78.7	83+4	• 3434	2.936	5•781	12.746	7.7822	110.689
71+311	1014.3	300+0	26.9	80.4							

	W. 200 100		2.375 T   F   F   T   T   T   T   T   T   T		TABLE 8	E Biggarde (1977)	PAG DAT	E: 1 E: 9-8-76	<del></del>
-  -  -			20 4 4 4 10° 20° 20° 20° 20° 20° 20° 20° 20° 20° 2	FLOW RATE	VERSUS DIFF	ERENTIAL PRESSURE	CLEAN CONDITION - R PRESSURE DATA ACQUI (10,000 PSTA NOMINA	RED AFTER-10-III	e <del>cii irressu</del> re
	E WAS 100 TO I E COMPAN		TEST NUMB	270 270	3¢	TEST DESCRIPTION	IN FORWARD DIRECTIO INLET PRESSURE = 41	N. TEST SPECIA 5 PSIA NOMINAL,	MEN (S/N 023) DATA
_	****	****		R CONDITIONS	****	****	OBTAINED AFTER P	CIMEN INCET (	ONDITIONS.
	\$ <del>\$ 4 4 5 5 5 5 5 5</del>	FLOWMETER ONE	****	*****	FLOWMETER TW	0			
 [ˈ!	FLOW RATE (ACFM)	PRESSURE (PSI <sub>4</sub> )	TEMP (DEG. F)	FLOW RATE (ACFM)	PRESSURE (PSĨA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG, F)	FLOW RATE (ACEM)
	•79	50.1	81.7	•81	48.3	82•7	413,7	82.2	•0951
	•69	49.9	81.7	.71	48.5	84.58	413.1	85•5	•0834
	.61	49.9	81.6	<u>.61</u>	48.7	82.9'	413.0	82.2	•07ŽŤ
		49.9	81.7	51	49.1	83.0	412,4	82,3	.0631
٠.	.42	49.7	81.7	.41	49.3	H3•2	4i2.4	82.5	• 0495 <sup>1</sup>
;	.32	5v.2	82.0	.31	49.9	83.4	412.4	82,7	.0382:
	. 27	>0.4	82.1	, 26	50.0	83.6	412,4	82.8	.0319
	.22	50.1	82.3	•21	49.9	83.7	412.4	83.0	.0260·
	.16	50.4	82.7	.14	50.2	84.0	412,4	83,4	.0183
	•16	49.9	82.9	•14	49.9	R4+2	412.4	83.6	•0181
	.23	56.2	82.7	•22	49.9	84.1	<u> 412.4</u>	83.4	•0270
	. 27	49.9	82.6	. 26	49.5	84.1	412,4	83.3	•0316}
-	<u>\$</u>	20.2	82.3	.31	49.9	84.0	412,4	83.2	•0382·
	42	50.2	82.0	. 41	49.7	83.9	411.7	82.9	.0501
_	•51	50.1	81.7	•51	49.3	83.6	411• <u>i</u>	82.6	•06 <u>1</u> 3.
. بند	•60	50.1	81.5	•60	49.1	83.4	410.4	82.4	. 5728:
	.69	49.9	81.4		48.5	83.1	410.4	82.2	.D840·
ļ.—	.77	50,4	82.0	,79	48.9	82.9	409.1	82.4	<u>.0944</u> :
·									

			EST NUMBER 5	FLOW RATE VERSUS DI	IFFERENTIAL PRESSURE	PRESSURE D. (10,000 PS	ITION <u>FLOW RATE VER</u> ATA ACQUIRED AFTER 10 IA NOMINAL) GN <u>IMP</u> ACT	HIGH PRESSURE CYCLES. FLOW	[
_		CIMEN INCET CON	DITIONS	PART 230	1131 02341711	INLET PRES	DIRECTION TEST SPE SURE = 415 PSIA NOMIN AFTER PROOF TEST		<del>.</del>
	******************	****	****		· · · · · · · · · · · · · · · · · · ·				
	PRESSURE	AVG TEMP	AVG FLOW RATE	GROSS DIFF. PRESS PRIMARY	GROSS DIFF∙ PRESS SECONDARY	AVG GROSS DIFF. PRESS	TARE, DIFF. PRESS	NET DÍFFL PRESS	
	(PSIA)	(DEG. F)	(AÇFM)	(PSID)	(PSID)	(bžič)	(PSID)	(PSID)	
	413.7	85.2	.0951	303,085	303,085	303.082	.001	303,084	
_	413.0	85.5	,0834	221,545	221,546	221.546	.001	221,545	
~	413-0	82.2	.0727	174,456	174,456	174.456	.001	174,455	
	412,4	· 82.3	. v611	133,370	133,370	133.370	.001	133,369	
	412.4	92.5	10495	98,922	98.922	98 <b>•</b> 555	.000	<b>38€ à</b> 50	
٠	412.4	82.7	•0382	69.577	70,162	69.865.	•000	69,868	
-	412.4	82.8	•0319	55.805	56,572	56 <b>.</b> 189,	•000	564187	
	412.4	83.0	.0260	44.112	44 <b>.</b> 355	44.234	•000	44.232	_
-	412.4	ri3.4	• 183	29.511	29.614	29.563.	•000	29.561.	
•	412.4	63.6	• 7181	29.105	29.327	29•516	• 000	58.512.	
•	412.4	83.4	.0270	46,545	46.458	46.502	•000	46,501	
	412,4	U3.3	•n318	55.680	56.256	55.968	•000	55,967	
	412.4	83.5	• 0382	70.202	70.794	70 • 49 <u>8</u>	•000	'70 • <del>•</del> • 96	
_	41127	#2 <b>.9</b>	.0501	100.818	100.818	100.618	•000	100, 916	
	411-1	82.6	.0613	134,318	134,318	134.318	.001	1349917	
	410·4	92.4	.0728	175.720	175,720	175.720	•00j	1756719	<del></del> -
	41054	85.5	.0840	226,919	226,919	556*à1à.	•001	226,918:	—
	409.1	82.4	• 0944	298.977	298.977	298.977	+001	290.976	<del></del>
			·				<del> </del>		
,		TARE DIFF. PRE	SS = -3.40000E-0	7 -4.44000E-04 (A	CFM) + 1,50933E=01	(VČEM) ***5 +	0 (AČEM)	** <u>3</u> .	
_									
							·		

						*			PAGE: DATE:	3 9-8-76	<del></del>
				FLOW RAT	TABLE 8 E VERSUS DIF	FERENTIAL	PRESSURE			N RATE VERSUS DIFFER	
		TE	ST NUMBER 5	PART	230	TEST D	ESCRIPTION	(10,000 IN FORWA	PSIA NOMINAL) ARD DIRECTION. ESSURE = 415 I	O AFTER 10 HIGH FRES GN <sub>2</sub> IMPACT CYCLES, TEST SPECIMEN (S/N PSIA NOMINAL, DATA	FLOW
*********	********	******	TEST SE		ET CONDITION		*****		ED AFTER PRO	NET DIFFERENT	
PRESSU	RE		TEMPERATURE			-	FLOW RATE:				
					LITERS/			GN2	GNZ	KB/SD/CM	
KG/SQ CM	PSla	DEG. K	DEG. C	DEG. F	MIN	ACFM	SCFM	KĞZHR	LBS/HR	DIFFERENTÎAL	PSID
29.083	413.1	301.1	27.9	82.2	74.1	•0951	2.616	5•151	11.355	21.3089	303.08
29,037	413.0	301.1	27,9	82,2	64,9	.0834	2,292	4,512	9,948	15,5762	221.54
29,037	413,0	301,1	27,9	82,2	56.6	.0727	1.997	3,933	8,670	12,2654	174,45
28,991	412,4	301,1	28,0	82.3	47,4	.0611	1.675	3,299	7,273	9.3768	133,34
28,991	412,4	301.2	28.0	82.5	38.4	.0495	1,357	2,673	5,893	6,9548	98,92
28,991	412.4	301.3	28,2	82.7	29.6	.0382	1,046	2.059	4,539	4,9122	69,00
28,991	412.4	301.4	28,2	82,8	24.8	.0319	.874	1.722	3.796	3,9504	36,14
28.991	412.4	301.5	28,3	83.0	20•2	.0260	.712	1,402	3.090	3,1098	44623
28.991	412.4	361.7	28.5	83.4	14•2	•0183	•501	.986	2+173	2+0784	29,5
28.991	412.4	301.8	28.7	83.6	14.0	.0181	.496	.976	2:151	2.05#0	29.21
28.991	412.4	301.7	28,6	83,4	20.9	.0270	•738	1.453	3.204	3,2693	46,5
28,991	412.4	301.7	28,5	63,3	24.6	•0318	.869	1.712	3.773	3,9348	55.94
28,991	412.4	301.6	28.4	83.2	29.6	.0382	1.045	2.057	4.535	4+95644	70.49
28,946	411+/	301.4	28.3	82.9	38 • 8	•0501	1.369	2.696	5.945	7.088ĩ	100.91
28,900	411.1	301,3	28,1	82.6	47.4	.0613	1,676	3,299	7,273	9,4434	134,31
28,855	410.4	301.2	28,0	82.4	56.2	.0728	1.985	3.909	8,618	12,3543	175.71
28,855	410.4	301.1	27,9	82.2	64.9	.084n	2,292	4.512	9,948	15,9539	226,91
28.764	409.1	301.2	28.0	82.4	72,7	.0944	2,568	5,057	11.149	\$1.0201	298,97
28.966	412.	301.4	28.2	82.8							
. 057	,5		<del></del>	• 4	DEVIATION	5					

PAGE: 1 DATE: 9-8-76

TABLE 9

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 INVACT CYCLES. FLOW IN FORWARD DIRECTION. TEST SPECIMEN (S/N 023) INLET PRESSURE - 1000 PSIA NOMINAL. DATA

TEST NUMBER 5 PART 23A TEST DESCRIPTION

OBTAINED AFTER PROOF TEST,
TEST SPECIMEN INLET CONDITIONS. FLOWMETER CONDITIONS

****	FLOWNETER ONE	*****	****	FLOWMETER TWO	***	<b>.</b>			
LOW RATE '	( <u>P</u> SYA) byfganyf	TEMP (DEG: F)_	FLOW RATE (ACFM)	PRESSURE	TEMP (DEG. F)	> 4 P + 4	KRESSURE.	AVG TEMP (DEG. E)	AVG FLOW RATE ., (AÇÇN)
•86	ρo'T	75•5	+91	47.9	80.4		1011.2	77,9	0429
.78	žų'S	75 <u>•</u> 1	.81	48.5	79+9		1011.9.	77.5	0389:
•69	49,9	. 75•1	•71	48,5	79.6	·	1011.9		• 03 § 0
•61	àñ•T	75•3	•61	48•9	79+6		1911-2	771.5	• 0298
.51	şγ.1	75-8	•51	49.3	₿Q•Q	= .u	1)15,9		0280
•41	<del>.49</del> .7	76•4	.41	49,1	80.3		1015.9	78.4	*0500
.32	ôå⁴1	77 • 4	•31	49.9	80.8	···· .	1,115.2	79.1	<u> </u>
.27	چ, ٥٥	78•n	•26	49.9	81+2		1015.9	79.6	,0132.
,22	ಶ್ವ ೪	78 <sub>•</sub> 6	•51	50.0 _	81.5		1015.9		•0107
•14	49,7	79•4	•13	49,5	81,9	-	1015.9		*0068
.14	50.1	80 • 8	.13	49.9	82.7.		1011.9	_Bl <sub>e</sub> 7	•0068
.23	45.₺	8468	.23	49.7	82.7		1915.9	81.7	-0113.
•27	49.9	8. •7	• 26	49.5	82+9	*	1015.9	8 <u>i.8</u>	<u>.</u> 0131
•32	à∿•7	80 • 5	•31	49.9	52.9		1711.9	81.7	
•41	. 56.1	80.40 ,	. 41	49.7	8Š*8		1011.9	81.4	-0203
•51	5v.6	79•2	-51	49,9	82.5		1015.9	80.8	
.611	ອນ.1	78:3	•60	49:1	98.0		101149	80-1	10223;
•74	50,1	77+5 .	+71	48.7	81.5		. 1911-9	79.5	-0344-
• 78	Þý.4	76+8	•81	48,9	81.0		1)11,2	78+9	
+81	5 <sub>0</sub> .4	76-2	•92	48 <u>.3</u>	B0.3		1011.9		.0435

PACE: 2

0 (ACFM) \*\*3

विट रिया स्थानकार्वे वेकस्पस्स	ECIMÊN ÎNLET CO	TEST NUMBER Ş	TABLE 9 FLOW RATE VERSUS D . PART 23A	IFFĘŔENTIAL PRESSY	PRESSURE DATA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,000 PSIA (10,	TION - FLOW RATE VERSITA ACQUIRED AFTER 10 IN A NOMINAL) GN2 IMPACT DIRECTION. TEST SPECTURE - 1000 PSIA NOMINALFIER PROOF TEST.	HIGH PRESSURE CYCLES. FLOW IMEN (S/N 023)
PRESSUHE (PSIA)	AVG LEMP (UÉG. F)	AVG FLOW RATE (ACFM)	GROSS DIFF. PRESS PRIMARY (PSIU)	GRASS DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF: PRESS (PSID)	NET DIFF. PRESS (PSID)
1011.9	77.9	.0429	93.076	93.865	93.470	<b>~0.000</b>	93,471
1011.9	17.5	.0389	82.300	83,119	82.710	-0,000	82,710
1011.9	17.4	.0340	69.61B	70,478	70.04B	-0.000	70+04B
1611.4	/7 <b>.</b> Š	.0298	59.354	60.048	59.70]	-0.000	59.701
1015-4	17.9	.0250	47.952	48.671	48.311	+0.000	48,311
1015.9	18.4	.0200	37̃.6n3	37,668	37,636	<b>-0.000</b>	37,636
1012.4	ſġ.Ī	. ភ្នំរីនឹង	27.522	27.547	27,535	-0,000	27.535
1015.9	<b>!9.6</b>	.0132	22.944	22,958	22.95 <u>I</u>	-0.000	224955
1015.7	80.0	•01u7	18,019	17.975	17 <b>.</b> 997	<b>~0.000</b>	17,997
1015.9	80.7	.0068	10.951	10.944	10.947	-0.000	10.947
1011 <sup>7</sup> Å	81.7	.0068	11.009	11,115	" 11.06Z	-0.000	11.065
1015.9	81.7	.0113	19.004	19.120	19.062	+0.000	19.06 <u>2</u> .
1015.9	81.8	.0131	22.713	22.843	22.778	0.000	22,778
1011-9	81 <u>.</u> 7	•0156	27.869	28.064	~ z̄?.967	-0.000	27.967
1011.9	81.4	.0203	38.009	38,186	38.098	-0.000	38,098
1015.9	ង០ <u>•</u> និ	. 0250	47.952	48,671	48.311	<b>-0.000</b>	48,311
1011.9	80 <b>. 1</b>	•0583	57.976	58,784	58,380	<b>→0.00</b> 0	58,380
1011-5	19.5	.0344	70.742	71.426	71.084	-0.000	71.084
1911.7	/8 <u>.</u> 9	.0391	83.041	84.067	83.554	-0.000	83,554
1011.7	78.2	•n435	96.393	96,393	96.393	-0.000	96.393

ARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM) \*\*2 +

PAGE: 3 DATE: 9-8-76

TABLE 9
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW IN FORWARD DIRECTION. TEST SPECIMEN (S/N 023) INLET PRESSURE = 1000 PSIA NOMINAL. DATA OBTAINED AFTER PROOF TEST.

TEST NUMBER 5 PART 23A TEST DESCRIPTION IN FORWARD DIRECTION. TEST SPECIMEN (S/N 0
INLET PRESSURE = 1000 PSIA NOMINAL. DATA
OBTAINED AFTER PROOF TEST.

1:-	*****	*****	*****	ŤĘST S	PECIMEN INLE	T CONDITION	<u> </u>	***		*******	NET DIFFERENTI	
Įr.	PRESS		I \$6444444	EMPERATURE	****	****	****	FLOW RATE	****	***		
	_K@/5Q_ ÇM		DEG. K	DEG. C	.DEG. F	LITERS/ MIN	AÇFM	SCEM	KŖ\HĤ GNS	GNŽ LBŠZHR	KG/SQ CH DIFEERENTIAL	— Ézíű
	71-144	1011.9	298.7	25,5	77,9	_82 <u>.4</u>	0429	<u>5•811</u>	<u>5.73</u> 2	12:637	6,5716 _	99.471
	71.144	1011.5	298.4	25.3	77.5	74.8	0389	2,643	5.205	_11:474	5. <u>8</u> 151	. BP+[]0
Ħ	71:144 .	1711-57	228.4	25.2	77.4	65.3	•0340	2.307	4.544	_10±014	4,9249	704948
н	71_144	1011.4	298.4	25.3	77.5	57.4	.0298	2.026	3.989	8.794	4.1974	57.701
	71.423	1015.9	298.7	25.5	77.9	48.2	•0250	1.702	3.351	7.387.	3.3966	40.311
	71.423	1015.9	298.9	.25.8	78.4	38 • 6	•0200	1.362	2.683	5.914	2.6461	37.536
	71.423	1015.9	299.3	. 26•2	79.1	29.7	.0154	1.048	2.063	4.548	1.9359	_27,935
	71.423	1015.9	299.6	26.4	79.6	25.4	.0132	.896	1.765	3.890	1.6137	22.952
p	71,423	1015,7	299,8	26.7	80.0	20.6	.0107	,727	1.434	3.156	1,2653	_ 17,227 .
٠	71.423	1015,9	300.2	. 27.0	80.7	., 13 <u>.</u> 0	<u>•0068</u>	459	.903	1.991_	7427	13. '47
	7].144	1011.7	300.8	27,6	<u>8</u> 1,7	13 <u>.</u> ļ _	0068	.461	908	\$ 005		11, 462
	71.423	1015,9	30.0.8	27.6.		21.6	.0113	.761	1,499	3,305	1.3402	19,462
	71.423	1015,5	300.8	27.7	81.8	25.0.,	.0131	.663	1.738	3.833	. 1,6015	. 22.778
	71.144	1011.9	300.8	27.6	01.7	29.8	_	1,054	2.075	1.575	1.9563	7,967
p	71,144	1011.9	300.6	_ 27.4		38.8	.0203	1,371	2.699	5,950	2,6785	_ 88 1AB
•	71.423	1015.9	300.3	. 27.1	80.8	. ,48 <u>.0</u> ,_	0250 _	1.695	<u>3•33?</u>	. 7:356	3.39 <u>6</u> 6	113
	71.144	1011.9	299,9	26.7	80.1	56:1		1,980	3.898	8,593	4.1045	, , ,
	71 <u>•</u> 144	1011 - 7	299.6	26.4	79,5	66+0	•0344	2.329	4.587	10:112	4,9977	1
	71:144	1011,2	299•2	26.0	78,9	_		2.646	5.210	11±487	5,9745	83× 354
	71 <u>+</u> 144	1011.9	298.9 *****	25.7	79.2.	_		-	5.81%	. 12:914 .	9±7771	96.393
	71.270	1013.1	299.6	26.4	79.6	a =						
	• 138	2.0	.8	. , ម	1.4	DEVIATION	ş			-		

		w ap 445348 ME 79 999	TEST MUNBER	4 5 PART.	25Ç	. ŢĘST_DĘSCRIPŢION I	(S/N 025) INLET PRE	RE. TEST SP	ECIMEN	
**	***	****	FLOWNETER	CONDITIONS	**************************************		NOMINAL. TEST SPEC	IMEN INLET	ONDITIONS:	
		FLOWMETER ONE		*****	.FLQWMETER. TWO					
El	OW RATE	PRESSURE (PSIA)	TEMP (DEG_F)	FLOW RATE	PRESSURE	TEMP (DEGF)	PRESSURE:	TEMP, (DEBL E)	PLON RATEI	<u> </u>
	•70	5v.B	84 <u>4</u> 3	74	49.3.	85 <sub>4</sub> 5	419-5	84-9		<u>į</u>
	-69	> - 6	84.3	7.L	49.3	85.3	418.8	<u>84.8</u>	<u> </u>	_
	<b>∓</b> ₽0	2 <u>،</u> باد	8441	61	49 <u>+</u> 3	85+1	418.2	84.6	.071 <u>6</u> :	
	<u>.</u> 50	49.9	83,9	50 -	49.1	85	418+2	8 <u>4.</u> 5:	<u>• 0596</u>	
	<u>.</u> 41	<b>Ģ</b> <u>•</u> 4	83.8	<u>_41</u> _	49•9.	.84 <u>.</u> B	18.2	64,3:	¥ó∳gă,	[ [
	<u>.</u> 31	₹• او	<u>83</u> _8	30	49.9.		118.2	84.3.	-0354	
	<u>•</u> 26	49.9	83 , 7	26		84 <u>•</u> 7	418-2	8 <u>4.2</u>	*0306/	
	*šš	àΛ°Ì	83,8		49.9 .	84.8		B <u>4.3</u>	₹052ĕı	-
	<u>.</u> 15	טא*ן	84.0	<u>14</u>	49.9	. 6540	<u> 418+2</u>	84.5	0 <u>170</u>	¦
	<u>.</u> 15	42±9	B4 <u>1</u>	<u></u>	.49.7.	05 <sub>e</sub> 1		84.6	*0198°	į
	•\$1	47.9	84-1	121	. 49,9	65_1,	_418.2	B4 6:	<u>. 0252;</u>	- 1
	•27	9ų.1	. 83.9	26	49.9		118.2	84*4	<u>.0315'</u>	
	<u>.</u> 31	9 y <u>. 1</u>	B4. 0	.30	49 <u>.</u> 7	. 85,1,		84.6	_036 <u>6</u>	
	<u>.</u> 41	<u>ې ، 4</u>	83 48	40	49:9	85 <u>•</u> 1	417.5	84,4	<u>.0487</u>	 
	<u>.</u> 50	þų "]	83•6	•50	49:3	84 . 8	417.5	84.2	, 0595!	
	•59	5v <u>.6</u>	83.5	.60	49:5.	B4 <u>7</u>	416.9	84±1	<u>, 6 ŤĨŢ</u>	
	<u>.</u> 68	90.4	. 83,6	7ŭ.	49.3	54.7		84,2,	<u>.</u> 08251	
	<u>.</u> 71	5y.2	83,9	.74	4 <u>₽</u> •9	8448	<u> </u>	B4.4	• 0885:	
			•n•			•	<b></b>			
			* *		•				<del></del>	1

PAGE: 2 DATE: 8-31-76 TABLE-10 FLOW RATE VERSUS DIFFERENTIAL PRESSURE 1114--CLEAN CONDITION - FLOW RATE VERSUS
IEST DESCRIPTION DIFFERENTIAL PRESSURE. TEST SPECIMEN TEST\_NUMBER 5 \_\_\_ PART 25C (S/N 025) INLET PRESSURE = 415 PSIA .NOMINAL. TEST SPECIMEN INLET CONDITIONS GROSS. GROSS... AVG GROSS DIEE - PRESS NET. AVG AVG DIFF. PRESS TARE PRESSURE. I EMP \_FLOW\_RATE \_PRIMARY SECONDARY. DIFFE PRESS (PSID) (PSIÓ) (PSTA) (ACFM) (PSID) (PS10) (PSID) (QEG. F) 419.5 84.9 .)859 308,142 308,142 308.142 .001 308,141 276.222 . 1833 276.222 276,221 410.5 84.8 276,222 .001 418<u>•</u>€ . 1716 200.687 200.486 84.6 200.687 200.687 •001 88.5 .000 418.5 84.5 .0596 147.908 147,908 147.908 147,787 111,246 111,247 111,247 418.2 84.3 · n489 111.247 1000 ₹. 418.4 84.3 .0364 75,521 75.850 75,685 .000 754684/ .000 41B.C B4<u>•</u>2 .0309 60,650 61.312 60,981 691980 غ-814 54.3 . :254 4B.515 48,355 48,435: 484484 .000 418.4 84.5 .0170 30.515 30.475 30.438 30.475 .000 .000 418.9 84.6 .0168 30.20é 30,400 30.303 30,302 418.4 48, 139 40,131: . 0252 48,226 48,132 84.6 .000 บบ .0315 418.4 84.4 62.654 63.21.9 62,931 .000 62.93D. 418.4 75.894 76,482 . 0366 76,188 76.187 84.6 .000 417.5 84.4 . 1,487 111,247 111.247 111.247 111,246 .000 כ-עם 417.5 . 1595 148.856 148.856 84.2 148.856 148+855! .000 416.9 203,532 4001 b4.1 .0717 203.532 203,532 203,531 416.6 5,46 . 825 271.481 271.481 271,481 .001 271,480 416.6 14.4 . 1862 307.826 307.826 307.826 .001 307.825! LARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM) +2 + 0 (ACFM) ##8: يبر. լսս..

	-panty an anythropist	TE	ST MUMBER S.	PART 250	Ç	- ŢĒŞŢ		DIFFERENTI (S/N 025)	AL PRESSURE INLET PRESS	W RATE VERSUSTEST_SPECIMEN URE = 415 PSIA	
			ŢEST SI	ECIMEN INLET	CONDITIONS			.NOMINAL		NET DIFEERENT	
PRESS	JRE		TEMPERATURE	**************************************	*******************		ELOW_RATE				
G/SQ.CM	, PSla	QEG•.K		DEG - F	LITERS/	ACEM.	SCEM	KGNHH GVS	GNS	KBYSO: CH	Pain
29.493	419.0	302.5	29 .4	84.9	67.5.	<u>.</u> ⊔859	2:384	4.695	10,351	21.6645	:30 <u>8; 141;</u>
29.447	418.6	302.5	29.3	84.8	65.4	. • 0833	2.308	4.545	10.019	<u>19.4203</u>	271.221
29.402	. 418 <u>.</u> 4	_302_4		84.6	56 <u>.</u> 1	. 40716_	1 <u>.</u> 9 <u>8</u> 2	3.204		1421087	spořě <u>je.</u>
29.402	418.4	302.3	29.1		46 <u>*</u> 7		<u>1,6</u> 49	3,2,5		<u>วับรีรีอัฮอัง</u>	<u> </u>
29 <u>•40</u> 4	41 <u>8•</u> 4	. 302.2.	29 <u>.</u> į	84.3	38_3	0489	1,354	2.667	5,879	7 <u>-0214</u> -	<u> </u>
.29.402	416*t	302.2	29.1	84.3	28 <u>.6</u>	_0364_		<u>}.987</u>	<u> </u>	2 <sup>-3</sup> 51 j	·ř <u>Š, 484</u> ,
29.402	418.4	302.2	29,11	84.2	24.3	0309	<u></u>	1 <u>•68/</u>	<u>3•719·</u>	4-2873	20% <b>300</b> 4
29.402	418.4	302+2	29+1	84.3	20 <u>•</u> 0	0254_	7.05	j•388	3_059	3,4052	48: 484.
29,402	418.4	302.3	29-2		13 <u>.</u> 3	<b>-</b> 0170	<u>-</u> -470	<u> </u>	Š₹0 <b>¥</b> Ś.	5-1456	30 <u>6</u> 499:
29:447	418.5	302.4	50-5	84.6	13 <u>.</u> 2	<u>_</u> 016B				₹ <u>1</u> 130 <u>\$</u>	30 <b>~3</b> 0\$
.29.402 _	41844	302.4	29.2	84.5	<u>19•7</u>	0252	<u>.697</u>	12373	3,027	3738 <del>4</del> 0	<u> 40-131</u>
. 29 <u>•</u> 402	- 41826			84.4	24_7	<u>2</u> 15	87 <u>3</u>	1=718.	3.788	\$44 <u>844</u>	¥5.430
_56*¥0\$	<u> </u>	4, SOE	29.2	84.6	28 <u>•</u> ?	*0366	<u> </u>	<u>1,995.</u>	4=397	<u> ទុះ្ខាទត្តកុំ:</u>	·şēřšāš.
29.356	417.9	305 <sup>-3</sup>	59 • j	84.4	38 <u>•</u> 1		1:346	5 <b>4</b> 650	5,941	<u>'Ž-8214'</u>	<u> </u>
 _29 <u>.</u> 356	417.5	30\$*z	29.0	84.7	46 <u>=6</u>	<u>±</u> µ595	<u>1,645</u>	3,240	7.142	10-4422,	· 148-255:
 29.310	416.7	302.1	28.9	84.1	56 <u>.</u> }	<u> </u>	1,981	<u> </u>	<u>8,601</u>	1453095	żoż <u>ę</u> żą <u>i</u>
_29 <u>.</u> 265	41 <u>6</u> 44	_ 302 <u>.</u> 1		84.2	6444.	<u>.</u> µ825	2,275	4.479	9.874	13.º 0888.	\$ <u>\$</u> \$\$\$
.29.265 #####	416.4 8#884	302.2	29.1 ******	*****	2 <u>.</u> 3	0862	2.378	¥¥ĕ8\$	10.322	sí°ēĕśj	_307 <del>.</del> \$35;
29.380	41 <u>8</u> • v	302,3	59 · j	44.4				w	4		
<u>•</u> 642	i,o	•1	• 1		DEALVITONS		• -				

PAGE: 1

TABLE 11

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5-25 PART 25B TEST DESCRIPTION DIFFERENTIAL PRESSURE. TEST SPECIMEN (S/N 025) INLET PRESSURE = 700 PSIA NOMINAL.

FLOWMETER CONDITIONS
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	***	****	*****	****	****			
FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG+ F)	FLOW RATE (ACFM)	PRESSURE (PSÍA)	TEMP (DEG. F)	PRESSURE (PSIÅ)	AVG TEMP (DEG. F)	FLOW RATE: (ACFM)
.87	49,9	72.6	•90	47.9	74.0	715,7	73',3'	• <u>0</u> 604
	50.2	72:7	.81	48.5	74.4	707.8	73.5	4 05 55'
•70	49.9	73•0	•71	48.5	74.2	707.8	73.6	-0490.
59	49.9	73.6	<u>•61</u>	48.9	74.7	7i1.8		•0416t
.50	50.4	74+0	•50	49.7	75.2	707.8	74+6·	.0359:
•40	49.9	74•7	<u>•41</u>	49.3	75•7	767.8	<u>'7542.</u>	• 0283'
•30	50.5	75•4	•30	49.9	76+4-	711.8	75691	. ožīj:
•26	50.2	<u>75∙B</u>	• 25	50+0	76.9	711.8	<u>76,3</u>	.0180·
.21	56.4	76•2	•50	50•2	77.7	711.8	<u>76,9</u>	0146
	50.4	76•5	•14	50.2	78.5	7j5,7	₹7.5·	•00991
•14	49.9	77.4	•14	49.9	78+1	715,7	77.8	• 0096·
.22	50.1	77+4	•22	49.9	77,9	7 <u>1</u> 5,7	77.7	. 0152:
•26	5v.1	77.4	• 26	49.9	78.0	715.7°	77.7	0184
.31	49.9	77 • 2	•31	49.Š	77.7	715,7	77.4.	.0815
•41	49.9	76•8	•41	49.3	77.4	715,7	77.1	, ģž83:
.49	50.1	76•2	•50	49.3	77.6	715,7	<u>76,9</u>	. 0345'
58	5.04	75•7	•60	49.3	77.5	715.7	76.6	,0411
•67	5v.4	75•2	÷70	49.3	77.7	707.8	76.5	+048Ží
.75	50.6	74+6	•81	49.1	77+4	711.8	76+0	• 0545
• 65	50.2	74.5	•91	48+3	77•9	711.8	76.2	• 0608/

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PAGE: 2 DATE: 8=31-76 FLOW RATE VERSUS DIFFERENTIAL PRESSURE CLEAN CONDITION - FLOW RATE VERSUS
TEST DESCRIPTION DIFFERENTIAL PRESSURE TEST SPECIMEN
(S/N 025) INLET PRESSURE = 700 PSIA NOMINAL. TFST JUMBER 5-25 PART 25B TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* GROSS DIFF. PRESS GRASS DIFF. PRESS SECONDARY AVG GROSS DIFF. PRESS TARE DIFF. PRESS DIFF. PRESS (PSID) ĀVĠ FLOW RATE TEMP (OLG. F) PRIMARY (PSID) (PSID) (PSID) (PSID) 17---73.3 144,853 . n61·4 144.853 144,853 144.853 -0.000 73.5 · 7555 126.839 126.839 126.839 126.839 -0.000 707.5 .0490 107.560 107.560 107.560 -0.000 107.560 711,8 74.1 88.204 . 416 88.597 88,401 -0.001 88.401 74.6 71.531 707.5 0353 71,261 71.261 70.991 -0.001 75.2 707.5 . ^ 283 · 54.216 54,7B) 54,498 -0.001 54,498 711.5 75.9 39,956 . 213 39,824 40.087 39.956 -0.001 711.8 76.3 .0180 32.640 32,708 32,775 -0.001 32,708 76.9 146 25,571 25,596 25,583 -0.001 25,583 7799 715.1 77.5 16.648 16,716 16.682 -0.001 16,682 77.8 715.7 0098 16,416 16,544 16,480 -0,001 16,480 715.7 77.7 .1152 26.73 26,858 26,794 26.794 -0.001 11-------77.7 184 33.393 33,638 33,516 33.516 -0.001 715.7 77.4 .4215 40.404 40,606 40.505 40.505 -0.001 77,1 715. 55,729 55,411 . 283 55,093 -0.001 55.411 715.7 , 345° 70.517 71,215 79.916 -0.001 70,916 76.6 715.7 · 64I1 88.2.4 88.913 80.559 88,559 -0.001 .0482 107,560 107.560 107.560 -0.000 107.560 - L- 11.8... 76.0 r 545 127.787 127,787 127.787 127.787 -0,000 711.8" 76.2 06.18 148,014 148,914 148.014 -0.000 148,014 TARE DIFF. PRESS = -3.60000E-04 + -3.31610E-02 (ACFM) + 6.33359E-01 (ACFM) +2.+ 0 (ACFM) \*\*3

<b></b>				FLOW RATE	TABLE 11 VERSUS DIFF	ERENTIAL	PRESSURE				
·	- · ·		ĘST NUMBER 5-25				ESCRIPTION	DIFFERENT	TAL PRESSUE	OW RATE VERSUS WE. TEST SPECIMI SSORE = 700 PSIA	
			TEST SPE	CIMEN INLE	T CONDITIONS	*****		******		NET DIFFERENT	IALI PRESS
PRESSU	RE	34454345	TEMPER, TURE	444444	000000000	*****	FLOW RATE	*******			
KG/SQ CM	PSIA	DEG. K	nEG. C	DEG. F	CITERS/ MIN	ACFM	SCFM	GN2 KG/HR	GN2 LBS/HR	KU/SU CNI DIFFERENTIĂLI	₽ŠID≀
50.318	715.7	296.1	23.0	73.3	82.8	• 0604	2.925	5.759	12.696	10.1842	1444.053
49.765	707.8	296.2	23•1	73.5	75.2	• 1555	2.657	5.232	11+534	8,9776	ĭ26,839
49.765	7,7.8	296.3	23 • 1	73.6	66.4	• 049 0	2.343	4-614-	<u>10+172</u>	7.5022	187.54p
50.041	711.8	296.6	23.4	74.1	56.6	•0416	1.997	3.933	0.67 <u>i</u>	6.2[3 <u>2</u>	684493
49.765	707.8	296.8	23.7	74.6	47.7	• 0353	1.685	3,318	7+314	,5', 0 <u>102</u> '	<u>"Ārēki</u>
49.765	707.8	297.2	24.0	75.2	36.2	•0283	1.348	2.653	5-850	3,4316	544 <b>498</b>
50.041	711.8	297.6	24.4	75.9	28.9	.0213	1.022	2•012	4-435	2 <b>.</b> \$992'	:396756
50.041	711.8	297.8	24.6	76.3	24.5	•018n	.863	1.700	3.748	2;2996	32,708
50.041	711.8	298.1	25.0	76.9	19.8	•0146	•700	1.378	3•ñ38	1.7987	25,583
50.318	715.7	298.4	25.3	77.5	13.4	•0099	.474	•934	2+060	1.1729	<u> 164682</u>
50.318	715./	298.6	25.4	77.8	13.3	•0098	<u>.470</u>	•925	2+039	1.1587	16,480
50.318	715.7	298.5	25.4	77.7	20+7	•0152	.730	1.438	3.171	1.8838	264794
50,318	715.1	298.6	25•4	77.7	24.9	•0184	.881	1.734	3.823	2.3564	33,516
50.318	715.7	298.4	25•2	77.4	29•3	•0215	1.034	2 • 036	4+488	2.8478	40.505
50.318	715./	298.2	25	77.1	38•5	£850•	1.360	2.678	5.903	3.8958	55 <u>; +11</u>
50,318	715.1	_298,1	<u>24.9</u>	76.9	47 • 0	0345	1.659	3.268	7-204	4,9859	70.916
50.318	_ <u>715./</u> _	297.9	24.8	76.6	56•N	+0411	1,978	3.894	8+586	6.2263	68.569
49.765	767.8	297.9	24.7	76.5	64.9	• 0482	2.291	4.510	9.943	7,5622	107,560
50.041	<u>711.8</u>	297•6	24.5	76.0	73.9	.0545	2.610	5.140	<u> </u>	8.9843	127.787
50.041		- <del>297.</del> 7	24.5 448##	76.2	82•4	•0608	2.910	·\5\729'	12.631	10+4064	148.014
50.097	712.5	297.6	, 24.5	76.0		······································	•				: P
.199		7	···	1,2	DEVIATIONS	<u> </u>		<del></del>	•		***

	······································		FLOW RAT	TABLE 12 E VERSUS DIFF	ERENTIAL PRESSURE	-		
		TEST NUMBE	R 5-25 PART	25A	TEST DESCRIPTION	CLEAN CONDITION DIFFERENTIAL PRESS (S/N 025) INLET PR	SURE. TEST SI	PECIMEN
*********			CONDITIONS	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	988408000000		CIMEN INCET C	
	FLOWMETER ONC			FLOWMETER TW	0			· · · · · · · · · · · · · · · · · · ·
	*********	******			***		AVG	AVO
FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG.F)	FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG, F)	PRESSURE (PSIA)	TEMP (DEG. F)	FLOW RATE (ACFM)
.84	58.5	68•3	•90	48.3	73.7	1007.9	71.0	•õ42Ŝ.
.76	56	68•0	•81	48.9	73•3	1007.9	70.6	•0389′
.67	49.9	68+	•71	48.3	73•2	1007.9	70.6	.AEE0.
.58	49.7	68•3	•61	48.5	73•2	1007.9	70.7	•0290
•49	49.7	68•8	•50	48.9	73.5	1007.9	71.1	.0244
•40	49.7	69•4	•40	49•Ĩ	73.8	1007.9	71,6	, ö197°
.30	50.1	7Ġ•1	•31	49.9	74.2	1007.9	72.1	.0151.
•26	49.7	7)•8	.26	49.Š	74.6	1007.9	72.7	.dižB
•21	49.9	71 • 4		49•7	74.9	1007.9	73•1	.0103
<u>•14</u>	49.5	72.3	•14	49•1	75•4	1007.9	73.8	.0068
•14	56.1	73•6	• j 4	49.9	76 • 2	1007.9	74.9	•0069
•24	Þ(.•S	73•7	.24	49.9	76.4	1007.9	<b>75.</b> 0	.õlié
.27	50.4	73.7	,26	50.2	76.4	1007.9	75.1	.0133
•31	49.9	73.5	31	49.5	76.6	1007.9	75.0	.0152
•40	50.4	73•0	•40	49.9	76.4	1007.9	74.7	,0198
<u>.48</u>	50.1	72.4	•49	49.3	76.2	1007.9	74.3	.6241
.58	50.2	71 • 4		49.i	75.6	1007.9	73.5'	,0290
•66	56.02	70.5	•70	49.1	75.1	1007.9	72.8	. 6336
.75	5u.4	70:0	•8 <u>0</u>	48.7	74.6	1407.9	72.3	.038]
.05	50.4	69:3		48.3	74.0	1007.9	71.7	.ō428.

						PAGE:	8=31=76
****	**************************************	F	LOW RATE VERSUS C	2 IFFERENTIAL PRESS	URE		
		EST NUMBER 5-25	PART 25A	TEST DESCRI	PTION DIFFERENTIAL	rion - Flow, Rate V L. Pressure, Test NLET PRESSURE = 10	SPECIMEN
	PECIMEN INLET CON			,			
	AVG	ĀVĠ	GROSS DIFF. PRESS	GROSS DIFF. PRESS	AVG GROSS	TAREL	NET
RESSURE (PSIA)	TEMP (DEG. F)	FLOW BATE (ACFM)	PRIMARY (PSID)	SECONDARY (PSID)	DIFF. PRESS (PSID)	DIFF. PRESS' (PSID)	DIFF. PRESS (PSID)
1007.9	71.0	-0425	99,870	99.870	99.870	-0.000	99.870
1007.9	70.6	•0389	88,328	89,124	88.726	-0.000	88.726
1007.9	70.6	.0334	73,735	74.586	74.160	-0.000	74-161
1007.9	70.7	•0290	61,984	62,577	65• <u>5</u> 80	-0.000	682580
1007.2	71.1	•11244	49.57B	50.251	49,915.	-0-000	494915
1007.9	71.6	•n197	39,168	39.281	34.55¥	-0-000	394225
1007.9	72.1	.0151	28,796	28.811	28 - 804	-0.000	284804
1007.9	72.7	.0128	23,756	23.761	23.758	-0.000	23,758
1007.9	73.1	.01/3	18,425	18.376	18.400	-0.000	18,401
1007.9	73.8	•0068	11,762	11.743	11.753	-0-000	11.753
1007.9	74.9	.0069	11,936	11.972	11.954	-0.000	11.934
1007,9	75.0	.0118	21,554	21.697	21.626	<b>-0.000</b>	21.626
1007.9	75.1	.0133	24,972.	25.080	25.026	-0.000	.55, 056
1007.4	75•0	.0152	29,202	29.328	29.265	-0.000	59.565
1007.9	74.7	.1198	39,342	39,512	39.427	·=0.000	39.427
1007.9	74.3	.1241	49,328	49.935	49.631	-0.000 -	49,632
1007.9	73.5	•0290	61,733	62,261	61.997	-0.000	61.997
1007.9	72.8	•n336	74,233	74.902	74.56B	-0.000	74,588
1007.9	72.3	-0381	87,470	88,176	87.823	-0.000	87.823
1007 <u>.</u> ¥	71.7	.0428	101,766	101.766	101.765	-0,000	101.766
	JARE DIFF. PRE	SS = -1.64000E=04	+ -1.26930E-02 (	ACFM) + 2.48070E	-01 (ACPR)2,	0 (ACPM)	<b>**3</b>

PAGE: 3 DATE: 8-31-76 TABLE 12 FLOW RATE VERSUS DIFFERENTIAL PRESSURE CLEAN CONDITION - FLOW RATE VERSUS TEST DESCRIPTION DIFFERENTIAL PRESSURE. TEST NUMBER 5-25 PART 25A TEST SPECIMEN (S/N 025) INLET PRESSURE = 1000 PSIA NOMINAL. net bifferentiali press: TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\* \*\*\*\* PRESSURE TEMPERATURE FLOW RATE \*\*\*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\*\* GN2 KB/SQ CM LITERS/ GN2 18 KG/SQ CM PSIÒ PSIA DEG. K DEG. C DEG. F MIN **ACFM** SCFM KÖZHR LBS/HR DIFFERENTIAL -rinα. 5.721 996870 70.865 1007.9 12-614 294.8 21.7 71.0 82.3 .0425 2.906 7.0216 88,726 70.865 1007.9 70.6 75.3 5.239 îī•550 6.2381 294.6 21.5 .0389 2,661 4.507 70.865 1007.9 294.6 21.4 70.6 64.8 .0334 2,289 9.937 5.2140 74.161 1111: 70.865 1007.9 294.7 21.5 56.3 ·0290 1.988 3.914 8-628 443788 62,284 70.7 70.865 1007.9 294.9 21.7 71.1 47.2 .0244 1.667 3.283 7-238 3.5094 496915 70.865 1007.9 295.2 22.0 71.6 38.1 •0197 1.346 2.650 5.842 2.7578 39,225 1007.9 22.3 •015<sub>1</sub> 2.034 4.484 240251 28,004/ 70.865 295.5 72.1 29.3 1.033 23.75**8**: 1007.9 1.715 70.865 295.8 22.6 72.7 24.7 .0128 .871 3.781 Ĭ-6704 1007.9 22.9 1.378 1.2937 70.865 296.0 73.1 19.8 ·0103 .700 3.037 10.401 1007.9 .915 ĩi.793: 70.865 296.4 23.2 73,8 13.2 •0068 .465 2.018 .0263 Ĩ1.9\$4 70,865 1007.9 297.0 23.8 74.9 13.3 .0069 .470 .926 2-041 .8404 1.572 21.426 70.865 1007.9 297.1 23.9 75.0 22.6 .0118 .798 3.466 1.5204 1007.9 23.9 1.779 70.865 297.1 75.1 25.6 .0133 .903 3.921 1.7595 25% 026 70.865 1007.9 297.1 23.9 75.0 29.2 .0152 1.030 2.026 4.472 Ź. 0375 29,265 70.865 1007.9 296.9 23.7 74.7 38.1 .0198 1.347 2.652 5.848 2.7720 39,427 70.865 1007.9 296.6 23.5 74.3 46.4 .0241 1,639 3.227 7-114 3,4894 49,032; 70.865 1007.9 1.974 61.997 296.2 23.1 73.5 55.9 ·029n 3.887 8.569 4-3568 70.865 1007.9 295.8 22.7 .0336 4.512. 74,568 72.8 64.9 2,292 9.948 512426 70.865 1007.9 295.5 22.4 72.3 .0381 5.123 6.1746 87.483: 73.7 2.602 11.294 70.865 161.766 1007.9 5.765 295.2 22.0 71.7 82.9 .0428 2.928 12-710 7.1549 \*\*\* \*\*\* 70.865 1007.9 295.8 22.7 72.8

.000

.8

.8

1.4

DEVIATIONS

<u> </u>							PAGE: 1 PATE: 9-14-76	
		NEW ROOM C	FLOW RAT	TABLE-13 E VERSUS DIFFE	RENTIAL PRESSURE	GLEAN-CONDITIONFLC DATA ACQUIRED ON TEST ADDITION OF SYNTHETIC	SPECIMEN (S/N CONTAMINANT.	027) PRIOR TO THE
·	round bearings in my	LEŽI-MNBE	R_10 PART-	278	iest_pescripțion	PRESSURE = 415 PSIA (	NOMINAL).	T;
	-	EI OWMETER	CONDITIONS	· · · · · · · · · · · · · · · · · · ·		TEST SPE	IMEN INLET C	
*****	**************************************	********		***********	**********	*************	***********	00000000000
***	FLOWMETER ONE	***	****	ELOWNETER TWO	***		AVG	AVG
FLOW RATE	<u>(₽Ş(V)</u> bĕr≅znuf	TEMP (DEG = E)	FLOW RATE	PRESSURE (PSIA)	(DEG F)	PRESSURE (PSIA)	TEMPI IDEG: E)	FLOW RATE,
- • 76	49,9	69:2		48.4	7054	413+7	69±8	
<u> •67</u>	<u> </u>	69:2-	<del>,7</del> 1	48 8	70+4	413+n	69 <u>*</u> 8	08 <u>27</u>
<u> </u>	<u> </u>	68 <u>.</u> 9	60	49 <u>*3</u>	70.4	413.0	69 <u>_6</u>	
<del></del>	<u>\$0.</u> 5		50	49.5	70.4	412.4	69.6	<u>•0€0ặ</u>
220	<u> </u>	68 <u>•</u> 7		49.5	70 <u>.</u> 4	411.7		<u>*0₹8⊕</u> }[
	<u>≱û*3</u>	68 <u>+</u> 8	.30	49.9	70.5	411.7	69.7	0370
<u>•26</u>	>u_5	68 <u>.</u> 9		50,1	70.5	411.7	69.7	
<del></del>	<u> </u>	6 <del>9<u>•</u>.1</del>	• <u>•</u> 5j-	49 <u>.</u> 9	79.7	411.7	69 <u>•</u> 8	•0\$E3
14	49.7	69,2	-14	49.5	7 <sub>12</sub> - 8	411.7	70.0	.0169
.14	50.3	69.4	-14	49.9	71.1	411.7	7.0 • 2	0170
<u>\$</u> 22	5è•3 .⊤	69≜2		49.9	7.j. • 9		7.0 <u>+</u> 0	
<u> </u>	50.5	69.•1	-26	50.1	70.9	411.1	70.0	-0350 <del>-</del>
<u>*</u> 31	<u> </u>	68.9		50 <u>.</u> 1		411-1	69.8	0380
<u>.4</u> 1	49.9	. 6846,		49.2	7#•5	410.4	69.6	
<u> </u>	<u> </u>	68 \$ 2	<u>•5</u> ]	49.0	7.u • 4	409 B	69.3	10614:
<u></u>	<u>\$</u> 0.3.	65 <u>e</u> 2	61	49.2	7.1.2	409.1	69.2	<u>.</u> 0724:
<del></del>	<u> </u>	- 68±0		8	59.9	408.5	69.0	<u>• 0830</u>
<u>. 75</u>	<u> </u>	6u-5	8 <i>u</i>	48,2	69.8	407.8	69 ž	
hara		<del></del>	<del> </del>					
	,							ر <del></del> ا،1،1،

- 7 ji

PAGE: 2 DATE: 9-14-76

CLEAN-CONDITION - FLOW-RATE VERSUS-DIFFERENTIAL FRESSURE:

FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED ON TEST SPECIMEN (S/N 027) PRIOR TO THE ADDITION OF SYNTHETIC CONTAMINANT. TEST SPECIMEN INLET PRESSURE = 415 PSTA (NOMINAL). - TEST HUMBER 10 PART 27B-TEST DESCRIPTION 711 TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* DIFF PRESS DIFF. PRESS SEGONDARY FLOW BATE AVG GROSS DIFF PRESS ŢARE DIEFE PRESS NEŤ DÍFEL PRESS: JEMB JEMB PRESSURE (PSIA) (DEG F) (ACFM) (pSID) (PSID) (PSID) (PSID) (PSID) 413.7 . 1936 69.8 302.835 302,835 302,835 302.833. .001 413.0 . 4827 225,939 225.939 225.939 225-938 69,8 .001 3334 .0718 176,258 176.258 413.0 69.6 176,258 .001 176 257 69.6 412.4 .06v3 133.538 133,538 133.53<u>B</u> .000 133,537 411.3 69.6 . 7488 98,413 98.413 98.413 .000 98-412 3937 411.7 69.7 .0370 64.109 68,668 66.389 66.387 .000 .000 411.5 69.7 •93<u>1</u>1 50.817 55,694 53.255 53.254 •000 411. 69.8 .0253 43.026 43.102 43.064 48-062 411.7 10.0 .0169 26,898 26,968 26.933 .000 26,932 27.371 411. 70.2 .0170 27,247 27.309 .000 27.307 46.802 411.1 70.0 .0266 45.884 46.343 46-342 .000 411.1 70.0 .0320 58,470 57,592 56.031 58.030 .000 7111 .0380 71,832 72.216 411.1 69.8 72.600 <u>•</u>000 72,215! 69.6 .0493 100.628 100.628 100.658 410.4 .000 100.627 409.4 69.3 .0614 138,918 138,918 138.918 .001 138.917 .001 409.1 69.2 .0724 179,422 179,422 179,422 179,421. 408.5 69.0 .0830 231.002 231.002 •001 231.005 231,001. 407.8 69.2 .0934 305,999 305,999 305.999 .001 305,998 IARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM) \*\*2 + 0 (ACFM) ##8.

-TABLE -1-3-

		. 4. 4.0.2.2.1990	FLOW RATE	TABLE 13 VERSUS DIFF	ERENTIAL F	RESSURE	DATA ACQUIR  ADDITION OF	ED ON TEST SPI	ATE VERSUS-DIFFEREN ECIMEN (S/N 027) FI NTAMINANT, TEST-SFI INAL).	RIOR TO THE
· · · _ · · · · · · · · · · · · · ·		±E2±10WBEù10	PART 2	7B	ŢĒST-Ņ	<u>eculți</u> on				
		TFST S	PECIMEN INLE	T CONDITIONS					NET DIFFERENT	IALI PRESS:
*****	***********	**********	***********	\$ 0 5 0 0 0 0 0 0 0 0 0 0	**********	******	*****	******	********	****
SSURE 8566844444	*****	- IEMPERATURE-	**	***	****	FLOW-RATE	****	***		
PS1a		DEGC	DEG. F	LITERS/ MIN	ACEM	ScFM	KG/HĶ GNS	GN2 LBS/HR	KGYSQ:.CM: DIFFERENTIAL!	PSID:
<u>413.</u>		21.0	69.8	74_6	0936	2,635	5_185	11.437	<u> </u>	0
413.9		21.0	69_8	65_8	0827	2,323	4.574	10.085	15-8650	\$ <u>\$</u> 2 <del>\</del> \\$38 30\$\\\\\$33
413-4		20.9	69.6	<u>57.</u> 2	0718	<u> </u>	<u>3.977</u>	8_757	15-3951	176 257
		20+8	69_6	<u>48_</u> 0	<u>.</u> 0603	1,694	3_336	7 <u>.</u> 354	9,3886	<u></u>
<u>41</u> ]	294.0		69.6	38_7	-0488	1,368	2.694	<u>5</u> _939	<u>6.515</u> į	001415;
<u>41,-</u>	<del>-</del>	20.9	69.7	29.4	0370	1.037	\$ 045	4,502	4:6675	<u> </u>
411 <u>4</u>	•	20.9	69.7	24 <u>.</u> 7	<u>-</u> 0311	.873	1.719	3,789	3,7441	53,254
4114/	294-2	21.6	<u>69.8</u>		.0253	.709	i∙3ôë	3,077	3-05/6	<u> </u>
411.3	294.3	21.1	70.0	13,4	•1169	.472	•930	2.050	1.8935	50.535
<u>411.</u>	294.4	21.2	70.2	13.5	.0170	•47.7	.939	2 <u>•069</u>	1,9199	<u> 27:307:</u>
<u>411,41</u>	294,3	21.1	70-0	21:1	<u>. 1266</u>	.745	1.466	3.233	3-2581	<u> 464342.</u>
411.4	294,3	21.]	70.0	25•4	<u>.0320</u>	.89 <u>6</u>	<u>1•763</u>	3.888	<u> </u>	<u>58-030</u> ,
411.	294.2	21-0	69.8	30-1	_0380	1.063	5.003	<u>4-615</u>	5.0772	72,215
410-4	294.0	20.9	69.6	39.0	•0493	1.378	<u>2.713</u>	<u>5•981</u>	7,0748	<u> 100#651.</u>
409.0	293.9	20.7	69.3	48.5	<u></u>	1.714	3.375	7 <u>,440</u>	9.7668	<u> </u>
409.1	293.8	20.6	69.2	57.1	<u>•</u> 0724	2.017	3.971	8 <u>.755</u>	12 <u>.61</u> 46	<u>17954\$1.</u>
408.	293.7	20.5	<u>69.n</u>	65.5	<u>.083</u> 0	5.315	4,552	10_036	16*5 <b>†</b> j0	\$3₹°ŏŏ₹
407.5 ####:			69.2	<u>73.5</u>	10934	2,595	5,109	11 <sup>5</sup> 56 <del>4</del>	<u> </u>	- <u>ặặṣ' 996</u> :
	,		69.7							
411.4			*5	DEVIATIONS	<u> </u>					
1.4	÷ •1	• j	**	SEATHITON	<u> </u>					· · ·

		201 201 101 101 101 101 101 101 101 101						GE: 1 <del>TE:9-14-76</del>		_
				FLOW RAŤ	TABLE 14 E VERSUS DIFFE	RENTIAL PŘESSURE	CLEAN-CONDITION - FLOW DATA ACQUIRED ON TEST -ADDITION OF SYNTHETIC	SPECIMEN S/N 02	7 PRIOR TO THE	
			<del>†</del> ESŤ-NUMBE	R 10 PARŤ	ź7A	TEST DESCRIPTION	PRESSIRE = 1000 PSTA (	NOMINAL).		
		**********	FLOWMETER	CONDITIONS		ARRANARA ARRANARA	TESŤ SPE	CÎMEN ÎNLET Ĉ	ONŌŢŤĬOŅŜ:	
	4 9 9 4	FLOWMLTER ONE			<u></u>				•	<u>.</u>
	*******	• •						AVG.	ÁVÖ <u>L</u>	
	ELOW RATE	PRESSURE (PSIA)	ŤĘMP <del>(DEG<u>*</u> F)</del>	FLOW RATE	PRESSURE (PSIA)	TEMP (DEG. F)	PRESSURE:	TEMPI (DEG+_E)	řľov Řáře (AČÉH)	_
	<u>+8</u> 7	- 4ō · o	7456	•91	47+6	77+7	1009+2	76+1	+ò4ĕ9'	
	<u>•78</u>	<del>5</del> 0+4	<del></del>	+81	48+6	77.0	<del>1009+2</del>	<del></del>	<u>+ ō390</u>	
	<u>*ē</u> 9	50 <b>-2</b> -	<del>73:1</del>	<del>-</del> 71	48+8	76-6	1305.3	<del></del>		_
_	<u></u> 60	<del>50</del> -1	<del>7</del> 2+9	<del></del>	<del>49+1)</del>	76+4	1.05√3	· '74,7'	<u> </u>	
	<u>•51</u>	50+Z-	72 <u>.</u> 8	<del></del>	49+2	76+3	1905.3	·	, 02×0	 31
		<u>50,4</u>	73.0	40	49.5	76.3	<u>lno5,3</u>	<u>'₹¥ç₹'</u>	- îñî	_ ~
	32	50.2	73 <sub>+</sub> 3	31	49,5	76.5	1.105.3	7×,9'	, <u>0</u> į̃š́6′ · · ·	
	27	50,2		<u>, ż</u> 6	49.59	76.5	1005,3	<del>75</del> 40	,ó <u>į́32</u> ;—	
	22	<u> </u>	<del>- 73.9</del>		49 <b>.</b> 3	76.8	1005,3			_
		<u> </u>	74 <u>+</u> 6	.13	50.F	<b>77 ∗</b> 0	1005.3		.0060	<u> </u>
	15	50.2	75.2	,ī3	49.9	77.43	1005.3	7642:	.0070	
	.22	50.1	<b>7</b> 5-0	.21	49.7	77.2	1001.3	76.ĭ		g r
	27	49.7	74-6	+26	49.2	77-1	1001+3	'75'-9'	•ōīá <u>;</u> :—	<del>.</del> .
_	32	49.7	74:		49+2	7.7. ()	1701.3	75 <u>+</u> 5	• ōīš <u></u>	<u>}-</u>
		50-1	73+3	41	49.2	76.7	1001.3	75+0:	0204	<u>"</u>
	51	50.1	72:4		49.2	7.6.3	1001.3	<u>74+3</u>		_
	60	50.4			49.3	75.6	1501.3	73.5°	, čž9'9:	_
		50-1	<del>7`<u>*</u>4</del>	71	48-6	75.1	1:01.3:	<u> </u>	+ô3ĂĂ:	
	78	50.2	69+5	B1	48.4	74.4	997.3	71.9	-039ž;	
		50.4			48+2	73+6	997.3			
	F#!	•	04-1	<b>*</b> • • • • • • • • • • • • • • • • • • •		,		• - 3 •		àa
_	·									
							r			
_			-		<del></del>				•	, '

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			# Ninemen	FLOW RATE VERSUS 0	IFFERENTIAL PRESSUR	RE DATA ACQUIRED  ADDITION OF EVEN	N FLOW RATE VERSUS ON TEST SPECIMEN S/N NTHETIC CONTAMINANT.	027 PRIOR TO THE	
	<u> </u>		†EST NUMBER-14-	PART-27A	TEST-DESCRIPT		O PSIA (NOMINAL).		—:
	TEST SP	ECIMEN INLEŤ	CONDITIONS						
	· · ·				GRASS				
	_PRESSURE	AVG TEMP	AVG <del></del>	DIFF. PRESS	DIFF. PRESS SECONDARY	AVG GROSS	ŤAŘÉ — DIĚŘ PŘESS	NEŤ DŽŘÉ: PŘESS:	
	(PŠIĄ)	(DĒĞ, F)	(ACFM)	(P\$10)	(PSID)	(PŠIĎÍ	(PŚŢD)	PSID)	
	1009.2	76 <u>.</u> 1	.0429	91.701	92.186	91.940	<b>-0</b> - 0 0 0	91.941	
	1009•5	75.3	.0390	81.146	81,435	81.291	-0.000	81,291	3
	1005.3	74.9	.n344	68,952	69,425	69.18 <u>8</u>	-0.000	69',189'	
_	1005.3	74,7	.1298	57,559 <sup>,</sup>	58,363	57.961	<b>-0</b> - 0 0 0	Š7',961'	
_	1005,3	74,6	•0249	46,989	46,986	46,987	-0.000	46 <sub>9</sub> 988i	
	1005 <u>.</u> 3 ·	74,7	.0200	36,039	36,094	36.066	-0.00ô	36,066	
	1005.3	74.9	.n156	26,768	26.724	26.746	·=0.000	26.747	_
_	1005.3	75,0	•0132	ŹŹ', 249 <sup>,</sup>	22,136	22.193.	0-000	žž.193:	
	1005.3	75.3	.nio5	17.150	17.040	17.095:	·=0 = 0 0 0	Ĩ7.095	
	1005.3	75.8	•0069	B.981	8.984	8 • 9 8 Ž.	-0.00ó	8-982:	
	1005.3	76.2	•0070	10.835'	10.924	10.880	-0.000	Ĭo.880	
	1001,3	76.1	•01 '8	17.672	17.727	17.699	-0.000	17.700	
	1001.3	75.9	.~131	21,959	22.079	22.019	-0.000	22.019	1
	1001.3	75,5	•n155	26,884	26,954	26.919	·=0 + 0 0 0	ž6.9Ĭ <i>9</i> ′	_
	1001,3	75,0	•0204	36,850	37.015	36,932	-0,000	36,933	<b></b>
	1001.3	74,3	. 0253	48.090	48.250	48.170	<b>*0.00</b> 0	48.170	
	1001,3	73,5	•n299	58,311	58,995	58,653	-0.00ŏ	58.653:	
	1001,3	72,7	.0344	69,827	70,373	70.100	-0.000	70.100	
_	997,3	71.9	.0392	81,765	82,383	82.074	⇔0.000	82.074	
	997,3	71.i	.0441	95.657	95,657	95,657	<b>⇔0.000</b>	95,657	
		TARE DIEE	Poecs - 1 64000E	04 +1.26930E-02 (A	CFM) + 2 48070F=0	1 (ACFM) ##2	0 (ACFM)	*43	

PAGE: 3 DATE: 9-14-76 TABLE 14 GLEAN-GONDITION---FLOW RATE-VERSUS-DIFFERENTIAL-PRESSURE. DATA ACQUIRED ON TEST SPECIMEN S/N 027 PRIOR TO THE FLOW RATE VERSUS DIFFERENTIAL PRESSURE ADDITION OF SYNTHETIC CONTAMINANT, TEST SPECIMEN INLET PRESSURE = 1000 PSIA (NOMINAL). -PART-27A -T<del>EST--DESCRÍPTÌ</del>ON-TEST-HUMBER-10-767 NET DIFFERENTIALI PRESSI TEST SPECIMEN INLET CONDITIONS PRESSURE \*\*\*\*\*\* GN<sub>2</sub> GN2 KBMSQ ÇM LITERS/ KGZHR. DIFFERENTIAL PSIn. LBS/HR SOFM MIN. ACFN KG/SO CH DEG. K DEG -- C DEG.--F 91.941 2.914 5.737 12-648 6•464i 70.956 1009.2 297.7 76-1 82.5 -429 81.291.... 70.956 -7<del>5-1</del>-5.7753 1009.2 297.2 75.3 0390 2.652 5-221 <del>ī1•51</del>0 24-7 4.595 \_69<u>+189</u>.... 0344 2-334 <del>10+13</del>1 4.8645 70.677 297+9 გე"მ 66+1 1005.3 . \$7.961... -5<del>7</del>--1-1298 3.974 8.761 4+0751 74-7 2.018 -<del>70-677</del> 1005-3----296-9-23.7 ::31 46+988... 1-688 3.323 7.326 3+3036 296+8 74-6 47-8 945ء 70-677 1005.3 23.6 1.357 2.671 5.889 2:5357 366066 23.7 74.7 0200 70.677 1005.3 296.9 2.075 4.574 1.8805 26<del>, 747</del> 23.H 29.8 0156 <del>70.677</del> 1005; 3 297.0 3,895 ž2**-193**-897 1.5603 1005.3 53.9 75-0 25.4 41.32 70-677 297-1 70,677 75.3 0105 1.398 3.081 1.2019 1005.3 297.2 84.902 925 .6315 70.677 2.040 1005.3 297.5 .0069 471 927 2.043 .7649 <u>īo, Buo</u> 70-677 1005-4 297.7 76.2 0**07**0 **73**0 17.700 I 1,437 3,169 1,2444 <u>70.398</u> 1001.3 297.6 1.5481 75.9 25.0 0131 884. 1.741 3,838 22,019 70.398 1001.3 297.5 1.8926 ž6.919 75.5 0155 1.048 2.064 4.55n 70.398 1001.3 297.3 24.2 29.7 1.374 2.7.5 54965 2.9966 75.0 70.398 1001.3 297.0 23.9 38.9 0204 1.708 0253 3,363 7.415 3.3867 48<u>, 170</u> 23.5 74.3 70<u>398</u> 1001.3 296.7 48.4 3.985 58, 653 8.785 4-1237 70.398 73.5 57.3 0299 2-024 1001.3 296.2 23.0 4.596 4-9<u>285</u> 70+100-70+398 1001+3 295+8 55.0 72.7 66-1 446ر. 2.334 <del>-10+133</del> <del>, ,,39,</del> 5•<del>77</del>64 .8<del>2% 074</del> -70+118 997.3 295+3 71.9 2.652 5.222 -i1+513 22.2 2.987 997.3 294.9 5.882 <u>.72.967</u> 6-7<u>253</u> 955687 70-118 71 · 1 \*\*\*\* \*\*\*\* \*\*\* \*\*\* 74.7 70.551 1003.5 296.9 23.7 DEVIATIONS .194 2.8 • 6 •6 1.0

			**				· · · · · · · · · · · · · · · · · · ·	PAGE: 1 DATE: 9-15-	7.
					MADY to 15			DATE: 9-15	-76
			-	FLOW RATE	VERSUS DIFFE	RENTIAL PRESSURE	CLEAN CONDITION -		SUS DIFFERENTIAL
			T⊧ST ¦UMBER	12 _ PART_R	80	TEST DESCRIPTION	*** PP // /**	STREAM) DIRECT	PION. TEST
	****	****		CONDITIONS	********	*****	TEŠŤ ŠPÉ	CIMEN INLET C	ONDITIONS:
	•	FLOWMETER ONE		******	<b></b>		- 4 200 40 144		
į	ELOW RATE	PRESSURE (PSIA)	TEMP (DEG, E)	FLOW RATE	PRESSURE (PSIA)	TEMP	PRESSURE	AVG TEMP (DEG. É)	FLOW RATE (ACEM)
	•73	49.9	75+6		48.3	75 <b>.</b> 8	417.5	75.4	* 0 <b>0</b> 7 1
	<u>•6</u> 9	<b>50•</b> 4	75•1		48,9	75.9	416.9	<u> 75.5</u>	.0837
	<u>.</u> 58	5ų.4	. 75.2	6v	49.3	. 76.0	416.9	75.6	.0709
	<u>.</u> 49	20.5	75,3 .	<u> </u>	49:3	75.9 .	416.2		_0596:
	<u>-</u> 40	à0.*5	75.3	• 4(1	49,5	75 <u>.</u> 7.	416.2	75 <sub>2</sub> 5'	-0484/
	•30 -	ងុំប្∙្1	75 • 7	•30	49.5	76.1	416.2	<u>'75,9</u>	.0360·
	*5é	49.9			49.3		416.2	76-3	-0¥9÷
	•\$1	50*5	_ 76+1	20	49,9	77.2	416.2	76-6	.0247
	<u>.</u> 14	49.9	76.4	13	49.7	78.0	416.2	77.2	.0164
	214	49.9	76•8	13	49.5	. 79.8	416=2		•0163
	<u>.</u> 21	49.9	76•8	21	49+3	. 79,9	415.6	78-4	• <u>025P;</u>
	.26	49.7	. 76.9	•26	49•3	79•9	415.6	78.4	- 0307
-	•3ò	\$@•1	76.8	•30	49.5	79.7	415.6	78.2	
	<u>#</u> 40	,	76.5		49+9	. 79+3		77.9	<u>+0483;</u>
	- 678 -	`âñ*8` "	7.6 • 1	.49				77.5	<u>. 0592;</u>
-	<u>.58</u>	à6•e	. 76.3		49.3	78,9		77.6	• 0715'
	<u>•67</u>	50.4	76-8		48.9		113.7	77.7	•08 <u>22</u> :
	. <u>•</u> ₹0 .	<b>ρ</b> ñ*9	77.3	• 73	48,9	78.5	413.0	77.9	-0 <b>5</b> 62.
									<u></u> .
			, , , , , , , , , , , , , , , , , , ,		- 30.4	* * 10 ***** * *****		·	

	·		LOW RATE VERSUS DI	-	PRESSURE: 1	FION - FLOW RATE V DATA ACQUIRED WITH IDE UPSTREAM) DIRI	FLOW IN THE FO
3 7 m	·	TEST JUMBER 12	PART 280	TEST DESCRIP		N 028) INLET PRE	
TEŜŤ SP Ļūsķeķeņe	ECIMEN INLET CO	NDITIONS			(NOMINAL).		
PRESSURE (PSIA)	AVG <u>I</u> EMP (DEG <sub>e</sub> F)	AVG FLOW RATE (ACFM)	GROSS DIFF. PRESS PRIMARY (PSID)	GROSS DIFF. PRESS - SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF* PRESS (PSID)	píře PŘES (PŠIO)
417:5	75 <u>.</u> 4	•0871	309.946	309.946	309.946	•001	309.945!
416-9	75 <u>.</u> 5	-0837	277.662	277.662	277.662	•00 <b>1</b>	277-661
416.9	75.6	+0709	203.186	203.186	203-186	•001	203.185
416.2	75.6	• ( 596	153.641	153.641	153.641	•00ō	153,640
416.2	75 <u>∗</u> 5	• t, 484	113.686	113.686	113.686	• 000-	113-665
416.2	″ 75 <u>.</u> 9	•0360	77.162	77.986	77.52 <u>4</u>	•000	77,523:
416.2	76.3	.0304	62,627	63,502	63.065	•000	63 <sup>±</sup> 06∳.
416 <u>*</u> 2	76.6	.0247	49.118	49,118	49.118	.000	49.118
416 <u>.</u> 2	77.2	"n164	30.611	30,611	30.6117	-0.000	301611
416.2 -	7̂8•҈3 ¯	.0163	30.611	30,611	30.611	-0.000	30; 611 <sup>¢</sup>
415.6	78.4	.0252	50.717	50,717	50.717	•000	50:717
415.6	78,4	.0307	63,755	64,461	64•10 <u>8</u>	•000	64-107
415.6	78.2	.0363	78,414	79.484	78.949	.000	76, 546
415.6	77.9	• 0483	115.284	115.284	115.284	•000	115,263:
414.9	77.5	•0592	152.363	152,363	125-363	•000	152,302,
414.3	77.6	•0715	207.341	207.341	504.341	•001	207-340
413.7	77.7	•0822	272.868	272.868	272°898	•001	272,867
	77.9	•0862	309.307	309.307	309.307	•001	309-306
,	ļarē dīff. Pr	ESS = -3.40000E-05	+ -4.44000E-04 (A	<u>СЕ</u> М) + 1.50933E-	oī (WCEM)**\$·+·	0 (ACFM)	**§.
	· · · · · · · · · · · · · · · · · · ·	•					

OF POOR QUALITY

PAGE: 3 DATE: 9-15-76 FLOW RATE VERSUS DIFFERENTIAL PRESSURE CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. DATA ACQUIRED WITH FLOW IN THE FOR-WARD (S/N SIDE UPSTREAM) DIRECTION. TEST TEST DESCRIPTION TEST . UMBER 12 PART 28D SPECIMEN (S/N 028) INLET PRESSURE = 415 PSIA (NOMINAL). TEST SPECIMEN INLET CONDITIONS NET DIFFERENTIALI PRESS: PRESSURE TEMPER.TURE FLOW RATE **ជាំងសត្តិតំនៃសត្**តិស៊ីស៊ីស៊ីស៊ីស៊ីស៊ីស៊ី GN2 KG/SQ CH LITERS/ PSID. DIFFERENTIAL KGYŞQ CM PSIA DEG. K DEG. C DEG. F MIN ACFM \_\_\_\_SCEM\_\_\_\_ KG/HR LaS/HR 417.5 297.3 75.4 . 4871 .2.450. 4.825 10.637 21,7913 3n9: 945: 29.356 24.1 69.4 277,661 297.3 24.2 75.5 2.350 4.625 10.202 19.5215 29.311 416.7 .0837 24.2 75.6 3.917 2n3; 185 29.311 416.9 297.4\_\_\_\_ 56.3 ...0709 1.989 8,636 14.2853 1,670 3.289 10.8020 153,640 29.265 24.2. \_\_ .75.6 • u596 7.251 410,2 297.4 47.3 .0484 1.355 2.669 24.2 75.5 5.883 7,9928 113,665 29.265 416.2 297.3 3B,4 .0360 1.008 1.985 ·ŤŤ: 522: 29.265 24.4 75.9 4.377 416.2 297.6 28.5 5: 4504 297.8 24.6 76.3 .03/4 851 1.677 3,696 44433B 68: 964 29.265 416.2 24-1 29.265 416.4 297.9 24.8 76.6 19.5 • 0247 \_\_\_\_\_691 \_\_\_\_1.360 2,999 .0164 . ...458 . . . 202... 29.265 416.2 298.3 . 13.0 1.988 25.7 78.3 12.8 29.265 416.2 298,9 .0163 ......453 ..... .893 1.968 100. . 29.219 415.0 298.9 25.8 78.4\_\_\_\_19.9 · 0252 3.047 29.219 415.6 298.9 25.8 78.4 24.02 .....307 855 1.683 3.711 4.5p72 644107 25.7 78.2 28.6 .0363 1.988 5.55n6 781948 ...29.219 415.0 298.8. 4.382 1154283: UD--.29.219 415.0 25.5 \_\_77.9 \_\_ \_ .0483 1.346 2.650 5.842 8.1052 298.7 38 - 1 25.3 77.5 ...29.174 414.9 ... 298.5 46.7 .0592 1.649 3.247 7,158 10.7121 <u>152.362:</u> 298.5 25.3 77.6 257,340 29.128 414.5 56.2 .0715 1.986 3.910 8.620 14,5775 55.083 413./ 298.6 \_\_77 ,7\_ 272.667 . 25.4 64.6 , 4822 2.280 4.490 9.899 19-1844 4.697 29.037 ... 298.7... ...25.5 77.9 21.7464 309,346 67.5 2.385 10.355 \*\*\* \*\*\* 415. 29.230 298.1 25.U 77.0 40 دەنا •060 DEVIATIONS • 8 •6 • 0 1.0

DATE: 9-15-76

TABLE 16
FLOW RATE VERSUS DIFFERENTIALI PRESSURE ENTIAL: PRESSURE CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL FRESSURE.

DATA ACQUIRED WITH FLOW IN THE FORWARD (S/N SIDE UESTREAM)

DIRECTION. TEST SPECIMEN (S/N 028) INLET PRESSURE 
TEST DESCRIPTION: 1000 PSIA (NOMINAL).

PART 28C TEST NUMBER 12

*****	****	FLOWMETER	CONDITIONS	****	***	TEST SAEC	THEN INLET	ONDATIONS:	
******	FLOWMETER ONE	****	****	FLOWMETER TWO	***				
FLOW RATE	PRESSURE (PSDA)	TEMP (DEG. F)	FLOW RATE	PRESSURE,	TEMP.	PRESSUREI	TEMPI (DEBL FO	ELOWI RATE:	_
<u>.</u> 86	50.2	67.5	.9}	48.0	72.9	1009,2	·Ť02;	TOREN.	_
•78	59.0	66.6		48.0	72.3	1006-5		-0395	
•69	20.2	66.1	<u>4</u> 71	48-6.	71.8	Ĭuua-\$		0349.	
.60	50.4	65.9	060	49_0	71.5	iŏŏărș	<u>\$</u>		_
.51	50,0	66:1	.51	49.0	71.6	1008/5:	- seusi		
<u> </u>	20.2	66:4		49 <u>.</u> ŝi.	71:8		<u> </u>		
<u>•31</u>	50.2	67 <u>*</u> 0		49.5	71±9	<u> 1008-á.</u>			_
<u>*27</u>	<u> </u>	67.3		49.2	7 <u>1.</u> 9	<u> </u>	<del>- çŏ≠ē≀</del>		
-21	≱6.∓š	67 <u>÷</u> 7	<u>\$2</u> 0	49.7	<u> 71.7</u>	1006*5	69 <u>+</u>	- iejej:	
<u>.14</u>	48.4	6827	13	49.50	7i <sub>2</sub> 5	120942	<del></del>	<u></u>	
-14	<u> </u>	69.49	<u>+13</u>	49.29	<del>72•</del> 5	<u> </u>	·71 <u>::</u> 2:		
.22	50.4	6948		49.9	72 <u>:</u> 7	<del>joộy,</del> ż	<del>- 'ĭ}±2: -</del>	<u></u>	
-26	<u> </u>	69:6	<u>• 25</u>	49.9	72.9	<del></del>	<u></u>		_
<u>. 31</u>	#Q.4	6946	<u>.3n</u>	49.0	73-0	j00 <del>6</del> /S	<u>71.2:</u>		
- 41	<u> </u>	69-9		49±2	73+0	1008/ż	<del>70<u>-9</u></del>	<u> </u>	
50	\$8.2	68 <u>.</u> 3	-50	49.2	72+8	<u> </u>	<u> </u>	0247	
<u>-60</u>	<del>50.7</del>	6 <del>7</del> •3	•60	49:3	72:1	<u> 1008*5'</u>	6917	<u>^</u>	
<u>.69</u>	<u> </u>	6646	.70	48.8	71.5	1006.3	49-1	+0315;	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
<u>.78</u>	20.0	65 <u>.</u> 8	81	48.4	70 <u>.</u> 8	i00\$.3	<u>66∓3:</u>		_
<u>. 87</u>	20.5	65 <u>.</u> 0	<u>*9</u> }		70.3	1002/3	<u>67-6</u> 1		

PAGE: DATE: 9-15-76 TABLE 16 FLOW RATE VERSUS DIFFERENTIAL PRESSURE CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE, DATA ACQUIRED WITH FLOW IN THE FORWARD (S/N SIDE UPSTREAM) DIRECTION. TEST SPECIMEN (S/N 028) INLET PRESSURE = TEST NUMBER 12 PART 28C TEST DESCRIPTION 1000 PSTA (NOMINAL) TEST SPECIMEN INLET CONDITIONS GROSS DIFF. PRESS PRIMARÝ GROSS' DIFF. PRESS SECONDARY AVG GROSS. DIFF. PRESS TAREI PAEES: DIĘĘL PRĘĘS: (PSID) AVG TEMP AVG FLOW RATE PRESSURE (DEG. F) (PŠTÁ) (PSID) (ACEM) (PSID) 1009.2 70.2 .0429 100,608 100.608 100.608 **⇒**0 <u>6</u>0 0 0 0 100.60B 1009.2 69.4 .0385 86,805 88,282 87.544 #0 & 0 0 0 o : 87,544 1009.2 68.9 .0343 75.995 76,905 76.450 76,450 #0 ¥ 0 0 0 · 1009.2 68.7 .0296 64.579 64.291 64,003 w0.000 644291 1009.2 68.8 .0248 52.054 52,569 52,312, 52,312: -04000 1009.2 69.1 .0199 39.890 40.47B 40.184 #0 #000· 40.384 1009.2 69.4 .0151 29,215. 29.574 29,395 29/395! **404000** 1009.2 69.6 .0128 24.597 24,626 24.611. 244412; ·#0≥000: 1009.2 69.7 .0103 19,202 19,225 19.214 19.214 -06000 1009.2 70.1 .0067 11.835 11.830 11.835 11.833. ·#0#000: 1009.2 71.2 .0068 12,067 12.174 12,120 15,120 -0€000 1009.2 71.2 0105 19.675 19,608 19,742 19.675 **-09000** 1009.2 71.3 .0129 24.829 24.971 24.900 #0 £000. 244900 1009.4 71.2 .0154 29,968 30,381 30,175 ₩0,000 30 . 175: 1009.4 70.9 40.546 .0199 40.267 40.825 40,546 #0.000 1009.2 0.5 51.804 •0247 52,253 52.029 ·=0±000. 522 029 69.7 2,6001 .0298 64,868 65,211 65.040 -**∞**0 ≥ 0 0 0 65,040 1005.3 69.1 .0342 76,116 76.905 76.510 -#0 -000 750510 1005.3 68,3 .0388 87,967 89.230 86,599 88~999 #0 Å 0 0 0 1005,3 97.6 .0434 102,820 102,820 105.850 102,621 ·•0.000 ARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACEM) + 2.48070E-01 (ACEM)\*\*2..+ O (ACEMPAS:

DATE: 9-15-76 TABLE 16
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

ENTIAL PRESSURE

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED WITH FLOW IN THE FORWARD (S/N. SIDE DESTREAM)

DIRECTION. TEST SPECIMEN (S/N 028) INLET PRESSURE 
LEST DESCRIPTION 1000 PSIA (NOMINAL). TEST NUMBER 12 PART 28C

******	***	*****	***	*******	ET CONDITIONS	, , <u>, , , , , , , , , , , , , , , , , ,</u>	****	****	<u>នកគត់កូបកំពត់</u>	NET DIFFERENT	tvestojine i Vri Liičio
PRESS	URF #########	****	<u>TEMPERATURE</u> Sassassassass	****	****	*****	FLOW RATE	*****	844 <del>44</del> 44		
KG/50 CM	PSIA	DEG. K	DEG. C	DEG. F	LITERS/ MIN	ACEM	SCEM	Х <u>а</u> хна Gias	GN2.	KBYSQ CM	PS#D
70,956	1009.4	294.4	21.2	70.2	83.4	0429	2.946	5.801	12.789	7.0735	
70,956	1009 <u>.</u> d	293.9	20.8	69.4	74.8		2.643_	5,205	11-475:	<u>6-15</u> 08	er_5&c
70.956	1009,4	293.7	20.5	68.9	66.9	.0363	2,361	4,649	10.250	5'-3750	
70.956	1009.4	293.6	20.4	68.7	57.7	0296	2.037	4.01]	8,842	4,5201	64-291
70,956	1009.4	293.6	20.5	68.8	48 • 4	0248	1.708	3,353	7.414	3,6779	5g; 31;
70,956	1009.2	293,8	20.6	69.1	38.7	.0199	1.365	2,688	5'-927	2.8252	40_184
70.956	1009.2	294.0	20.8	69.4	29.4	.0151	1.039	2.045	4.5n8.	2.0667	290.391
70,956	1009.4	294.0	20.9	69.6	25.0	.0128	-882	1.73]	3.828	1.73ŋ <u>4</u>	246912
70.956	1009.4	294.1	20.9	69.7	20-1	0103	.7.08	1,395	3_075	1.3509	19,71
70.956	1009.4	294.3	2) • 2	70.1	12.9	•0067	456	.899	1.982	8319	<u>11; pā</u> ;
70,956	1009.4	295.0	21.8	71.2	13.1	.0068	.463	912	2 <u>.012.</u>	8521	12,12
70 <u>•</u> 956	1009,2	295.0	21-8	71.2	20.3	0105	.718	1.413	3-116	1.3833	19,67
70.956	1009_4	295.0	21.8	71.3	25.0	0129	864	1.741	<u>9.</u> 837	1+7597	34.90
70.956	1009,4	294.9	21.48	71.2	29 8	0154	1.053	24073	4.569		30 <u>+ 1</u> 75
70.956	1009.4	294_8	21.6	70.9	38-6	0199	1.364.	<u> </u>	5-922	- 2 <u>0</u> 807	
70.956		294.6	21.4	70.5	48-0	0247	1.695	3.337			63-099
70,956	1005**	294.1	20.9	69.7	58.0	0298	2+049	<u></u>	9 <u>.</u> 894		<del></del>
70.677	1005.4	293.8	20.6	69-1	66.4	.0342	2+346	<u> </u>	10-184	5.3792	
70,677	1005.3	293,3		6 <u>8</u> .3	75 <u>.4</u>		2,662	5 <u>242</u>	11-557	Ç*3501	98.559
70.677 6556	1005.5	293.0	19.8	67.6 *####	84.5		S•88 <del>Ý</del>	5.875	15:055		⊤13 <sup>3</sup> -ijŚĺ
70.914	1008.5	294-1	21 • 0	69.8				····-	1, 1 4, 1 1	<del></del>	
.071	1.0	•5	•5	.9	DEVIATIONS	<u> </u>		·-	,		

PAGE: 1 DATE: 8-2-76

# TABLE 17 FLOW ŘÁŤE VERSŮS ĎÍFFERENŤIÁL PRESSŮRE

ŤESŤ NUMBER 6

PĂŘŤ 3C-Î

TEST DESCRIPTION

CLEAN CONDITION-IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA PRIOR TO CN. IMPACT CYCLES. TEST SPECIMEN (S/N 021) INLET PRESSURE 415 PSIA (NOMINAL).

FLOWNETER CONDITIONS

TEST SPECIMEN INLET CONDITIONS

******	FLOWMETER ONE	*****	<b>*********</b>	FLOWMETER TWO	******			-2.1
FLOW RATE (ACFM)	PRESSURE (PŠI <sub>A</sub> )	ŤĖMP (DEG- F)	řlow RăŤe (ĀČŘM)	PŘEŠSUŘE• (PSIA)	ŤĘMP (DEG. F).	PRESSURE (PSIA)	TEMP (DEG. E)	FLOW RATE  (ACEM)
•72	50.4	ŤŔ•¢6	•76	49.Ī	79.0	417.4	78.8-	
•67	50.4	78.9	•70	49.ī	79•4	416.1	79.1	
<b>.</b> 58	50,4	79.0	•60	<b>49.</b> 3	79.4	416.1	79 <b>,</b> 2	ŏžōś
.49	50,4	Ťá.8	•50	<b>4</b> 9.9	79 <b>₊</b> 3.	4 <u>ī</u> Š <sub>*</sub> Š	79.Ö	0600 <u>_</u>
•40	50,i	ŤŔ•6	<b>,</b> 40	49 <b>.</b> 5	79 <b>.</b> 1	4ī <b>š</b> .8	78 <b>.</b> 8	
,31	50,i	78.9	, śó	<b>4</b> 9.9	79.1	4ī4,á.	79. ō	<u> </u>
•26	50,2	76•8	<u>, 2</u> 5	50.Ī	79∙Ž	414.8	. 79.0	
.21	50.2	79.4	•žo	50. <u>1</u>	79 <b>.</b> 8	414.8	79.6 .	0250
.13	50,2	80.0	•12	šo•ī	8 <b>ō</b> •Ž.	414.8	ėã.ĭ.	0154:
.13	50.1	6ñ•5	.ī2.	<b>49.9</b>	8ñ•4	414.8	80.5	.0153
.21	50.1	79·9	•20	49.9	8Õ•Ž	414.A	åÕ•Õ	
.26	50.2	79•Ž	• ž6	<b>49.9</b>	8ถึ•ន័	414.8	7.9.9	
•31	49.9	78•9	•šī	49.7	8ñ <b>+8</b>	4Ĩ4.Ž	79.8	.ôġŦž.
•40	49.9	7ã∙ê	•Ã0	49.3.	8 <b>ž•</b> ñ	414.2	80•∔	. •0462 .
.49	50,2	79•0	•Š0	<b>4</b> 9 <b>.</b> 5	8Ž•Š	<b>4</b> Ī3•š	šō.a	0600
<b>.</b> 58	50,1	78•9	•60	49.Ĩ	81.5	+ĨŽ.9	80.2	~• 07ĪĪ · · ·
.6 <sub>8</sub>	50.1	79•Ž	•71	<b>48</b> •7	81.3	4 <u>12.</u> 2	ģō.3.	ēžė
.70	50.4	Ť <b>9•</b> Ť	•74	<b>49.</b> 1	នកំ.ទ	411.6	áñ,3	ōš68

TABLE 17 FLOW ŘÁŤE VERSÚS ĎÍFFERENŤIÁL PRESSURE

PĂŔŤ ŚĆ-Ĩ

PAGE: 2 DATE: 8/2/76

CLEAN CONDITION-IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA PRIOR TO GNA IMPACT CYCLES. TEST SPECIMEN (S/N 021) INLET PRESSURE 415 PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS

TEST NUMBER 6

PRESSURE (PSIA)	AVG TEMP (DEG. F)	ĀVG FLOW RATE (ĀCFM)	igross Dife• Press Primary (Psid)	GROSS DIFF. PRESS SEÇONDARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TÁŘE DIĚĚ PŘESS (PSIĎ)	ŅĖŤ ōĭřě, Pāgss (PŠjō)	
417.4	78.8	• ñ878	305.617	305.617	305.617	•00Ī	305.616	
416.1	79•Ĩ	.₹B19	251.257	251.257	251,297	•õôī	251.256	,
416.1	79.2	.0788	186.467	186.467	186,467	•001	186.466	
415.5	79•ō	.0600	140.324	140.324	140.324	• 000	140.323	
414.8	78.8	₌õ480	Ĭõõ.5õ3	100.503	100,503	• õõõ	Ĩōō.ŠōŽ	u
414.8	79•Õ	.ñ368	68.620	69.214	68.917	• 000	68.916	-
414.8	79.0	.0308	5 <b>4.</b> 218	Š4.676	Š4,447	•000	54,446	
414.8	79,6	.0250	4ï.899	4Ž <b>.</b> 178	8E0.54	•000	42.037	
414,8	80,1	.0154	23,544	23,523	23,533	-0.000	23.532	-
414.8	80.5	.ñī53	žà.3ĨZ	23 <b>.</b> 465	23,388	-0.000	23,397	
414.8	80.0	.0248	4ī.725	41.947	- 41.836	• ŏ ō o o	41.635	1
414.8	79.9	.ñ315	56,474	56.88 <u>6</u>	56,681	• ŏŏōō	56,680	
414.2	79.B	.ñ372	69.994	70.794	 70.394	•000	70.393	
414.7	80.4	• ō482	101.135	101.135	ïōī.135		TōĬ.ÌśĀ	
413.5	80.8	•0600	140.324	140.324	140,324	• 000	140.323	• –
412.9	80•Ż	• 0711	īśś.68ō	188.680	188.680	•00Ĭ	ĨĠĠ+ĠŤ8	
412.2	80.3	•កំទំឧខ	Ž\$6.945	256.94š	256,945	•001	256.944	- <u>-</u>
411.6	80.3	•ñ868	29ĩ.ŏ78	291.078	291.078	•001	291.077	_ 1

TEST DESCRIPTION

TARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM)\*\*2 +

ō (ACFM) ##

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PAGE: 3 DATE: 8/2/76

TABLE 17 FLOW KATE VERSÚS ÖTFFERENTIAL PRESSURE

ŤESŤ NUMBER 6 pákŤ jC=i TEST DESCRIPTION CLEAN CONDITION-IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA PRIOR TO GN IMPACT CYCLES. TEST SPECIMEN (S/N 021) INLET PRESSURE 415 PSIA (NOMINAL).

یا	<b>ប់អ</b> ល់សព្ <b>ពព្</b> សស	*****	********	ŤEST :	SPECÎMEN ÎÑL	ET CONDITIONS	5 • * * * * * * * * * * * * * *	<b>.</b>	****	÷÷÷÷÷÷÷	NEŤ DIFFEREN	TIĂL PRESS
	PRESSL	IRE	*****	TEMPÉRÄŤURE	****	***	*****	ĖĽOW, RAŤE,	*********	****	* ***	
	KG/SQ CM	PSIA	DEG. K	DEG. C	DEG. F	LĪŤĒRS/ MĪN	AČFM	SĈFM.	KG\HR GNS	GŇŽ LBS <sub>Y</sub> HŔ	KG/SQ CM	PSID
	29·347	417.4	299.2	26.0	78,8	7ö.4	.0878	2•453	4+829	10-647	žĺ+4869	305.616.
	29 <b>,</b> 256	416.1	299,3	26.2	79,ĭ	65 <b>.</b> 3	.0819	2.280	4-490	9.899	ĨŹ.665ō	251.256
•	ž9,256	416.1	299 <b>.</b> 4	26,2	79,Ž	Š6.0	<b>.</b> 0708	ĭ.969	3.877	8,547	Ĩ3 <b>.</b> Ĩó99	186,466
	ž9,210	415,5	299,3	ž6 <b>,</b> 1	79.ō	47.4	.060ñ	ī,669	3,286	7.244	9.8657 .	140.323
	ž9,165	414.8	299,2	26,0	78, á	3Ť <b>.</b> 5	.048ñ	î,332	2.623	5.783	7.0660.	156.502:
	ž9 <b>,</b> 165	414.8	ź99 <b>,</b> 3	26.1	79.0	28.7	saéo.	ĩ.ŏ20	2+0ÓB	Ă.ĂŽŤ	4.8453	68:976
	Ž9 <b>.</b> 165	414.8	299.3	26.1	79.ō	24.0	.0308	.854	1.681.	3.7n5.	3.8279	5å <sub>4.4</sub> å6c.
	ž9.165	414.8	299,6	26.4	79,6	Ĭ9• <b>4</b>	•0 <b>2</b> 5ō	<b>.</b> 694	1.386	3.011	2.9555	ĂŽ', DÁŤ'.
	29 <b>.</b> 165	414.8	299.9	26.7	1.58	11·8	•n <b>ī</b> Š4	.427	•841	1.854	ī.6545	
	29.165	414.8	300.1	žè.9	8ñ.5	11.5	.0153	.422	.831	ī•833.	1.6443	. 23.387 .
	ž9•165	414.8	ž99.8	žė•7	8ō∙ō	Ĩ9•3	• ŋ <b>Ž</b> 48	88à.	1 • 354	2.985	2.9413	41.835 <u>.</u>
	Ž9.165	414.8	299.7	26,6	79.9	ŽÃ.5	•á3 <b>1</b> 5	873.	1.719	34791 .	. 3.9850	564680
	29.119	414.2	299.7	26.6	79.8	29.0	.0372	ī.ŏ28	2.025	4.465	4.9491	70.393
	Ž9.119	414.2	áãō.ō	Žà•9	8ō,4	37.6	•0 <b>4</b> 82	ī.332	2.622	5.781	<b>7</b> +1104	īōī.ļ34
ķ	Ž9+073	413.5	300.3	27.1	80.8	46.9	.060ā	ì.654	3.256	7.179	9.0657	îĂō.323:
	29 <b>.</b> 028	412.9	299.9	26.8	80.2	5Е8	•071ī	ī.96ō	3.859	8.518	13.2654	188.678
	28,982	412.2	<b>3</b> õõ.o	26.8	80,3	65.1	•ŋ <b>8</b> 28	2.278	4.486	9.889	ĩ8.06ŜÕ	256,944. J
	28,937	411.6	300,0	26.8 *****	Bõ.3	68.3	.0868	2,385	4+697	Ĩő <b>.3</b> 54.	_ 20.464B	291_077
	29+147	414.6	299.7	26.5	79.7							
	.069	1.0	•3	•3	•6	DEVIATIONS	;	-		···		

PAGES: 1 DATE: 8/2/76

#### TABLE 18 FLOW RĂTE VERSUS DIFFERENTIAL PRESSURE

ŤĖSŤ ŃŮMĐER 6

PĂRŤ 3B

TEST DESCRIPTION

CLEAN CONDITION-IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. FLOW RATE VERSUS	
DIFFERENTIAL PRESSURE DATA PRIOR TO GN, IMPACT CYCLES. TEST SPECIMEN (S/N 021) INLET PRESSURE 700 PSIA (NOMINAL).	

### 

****	FLOWMETER ONE	พิจะตัดตัดตัดตัดตัดตัด	***	FLOWMETER TWO	• * * * * * * * * * * * * * * *	
FLOW RATE (ACFM)	PRESSURE (PŜĪA)	ŤEMP (DEG• ř)	FLOW RĀŤĒ (ĀČFM)	PŖĘSSUŘE+ (PSIA)	TEMP (DEG. F)	
<b>.84</b>	50.4	7â•ī	•9Ĭ ·	<b>48,</b> 5	74.6	
•75	50.6	69•6	.ėī	49.1	74.2	
•67	50.2	69.4	•71	48.9	73 <b>.</b> 9	
•58	50.2	69•4	•60	49.3	73 <b>∙</b> 8	
•49	50.2	69•6	•ŠÓ	<b>49.</b> 7	73 <b>.</b> 9	
•39	49.7	69•9	• <b>4</b> 0	49.3	74-1	
•30	49.9	70+6	•30	<b>49.</b> 5	74.5	
•25	50.1	71.0	. 25	<b>49.</b> 9	74.7	
•21	50.1	71.8	•Ž0	49.9	75.3	
<b>.</b> 14	50.1	₹ĕ•å	• <del>1</del> •	49.9	75 <b>.</b> 7	
•i4	49.7	<b>7</b> 3∙6	•14	<b>49,</b> 9	76.5	
•22	49.7	73•6	•21	49.7	76 <b>-</b> 5	
•26	49.9	₹4•6	• 55	49.7	76.5	
•30	-50.1	<b>7</b> á∙3	•3Ĭ	49.9	76+4	
+4ò	49.7	7ž•9	•41	49+3	- 76+3 -	
.49	49,9	72.4	· •50	<b>49.</b> 3	76•0	
•58	49.9	71.9	•è0	<b>48.9</b>	ŤŠ•Ť	
•67	50.1	71.5	•7î	Ã8.9	75.Ż	
.76	50.4	71.0	•81	<b>48.9</b>	74.7	
•84	50.4	70•7	•91	<b>48</b> ∙§	74.2.	

### TEST SPEČÍHEN INLET CONDITIONS

PŘEŠSŮŘE (PSĽÁ)	. — - ĀVG— - · TEMP — - (DEG• F) .	FLOW BATE (ACEN)
711.8	·· · 72.3	
711.8.	. 71.9.	ō5ã6.
711.6.	71.7	
7ñ7.6	71.6	
7ñŤ∙é	71.7	
7ôř•é		.0276
767-8-	72+5:	
7â7.8	<b>72.9</b>	6179
7ñ7.á.	·73.5	
7ñ7.8	· 74+0	
711.6	75.1	
-711.6		0149 <sup>,</sup>
7īī.á	· · · · 75 • 0	
711.8 ·	<del>74.</del> 9	· 0214
·711+6	<u></u>	- îśśī
7ñ7.á	<del>7</del> 4+2'	Ô3Ă7:
787.Á	73 <b>∙</b> 8	ō41ō. ·
787.a	73. <del></del>	
7ñ7.8.	ŤŽ+9:	
707.8 .		iòiz,

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PAGE: 2 DATE: 8/2/76

TABLE 18 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEŠŤ DESČŘÍPŤÍON

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PART 3B

CLEAN CONDITION-IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. ..ELOW RATE VERSUS. DIFFERENTIAL PRESSURE DATA PRIOR TO GN. IMPACT CYCLES. TEST SPECIMEN (S/N 021). INLET PRESSURE 700 PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS

TEST NUMBER 6

PRESSURE (PSIA)	AVG Temp (deg. ř)	ÃVG Flow Rate (ãctm)	GROSS DIFE+ PRESS PRIMARY (PSID)	GROSS DÍFF• PRESS SEÇONDARY (PSÍD)	AYG GROSS Diff• Press (PSJD)	TÁRE DÍFF, PRESS (PSÍD)	DĬĔĔ ĊŘĔSS. (ŘŠÍĎ)	[
711.8	72.3	• 06/19	ĩ48.015	148.015	148.015	-0.000	148.015	
711.8	71.9	• ñŜ46	126.84ñ	126.840	126.840	-0.000	126.840	-
711.8	71.7	.0479	105.665	105.665	105.665	•ō•ōoō	108.665	
707.8	71.6	.ñ417	86.528	87.618	86.773	-0.001	86.773	
707.8	71.Ť	. ñ348	6 <b>7.</b> 786	68,371	68.079	+ō+ōòī	68-079	
707.8	72.0	•ñŽ76	50.500	51.305	50.902	-0.001	Šŭ.9ÔŽ	
707.8	72.Ŝ	.ñã13	37.097	37.226	37 <b>.</b> 162.	-0.001	37.162	
707.B	72.9	.ñī79	30,011	30,093	30.052	<b>⇒</b> 0.001	30.052	
707.8	73.5	.ñ144	22.982	23.034	23.008	-0.001	23.008	
707.8	74 <b>-</b> 0	• ã â 9 9	14,792	14.73Å	14.763	÷0.001	14.763	
711.8	75∙1	86ññ•	Ĩ4,6Ĩ8	14.734	Ĩ4.676	-0.001	14.676	- 1
711.8	75.Ĭ	•ñ149	24.086	24.239	ž4.162	-0.001	24.162	-
711.8	75.Ō	.ñī79	ž9,953	30.ÎSÎ	30.052	-0.001	30.052	
711.8	74.9	.ñ214	37,562	37',687	37.624	-0.001	37.624	-
711.8	74.6	•õžBi	51.078	52,569	52.224	-0.00ī	5ž.2Ž4	•
707.8	74.Ž	• 0347	67.536	68.37]	67.954	-0.001	67.954	
707.8	73.8	.0410	85,177	86.070	85,623	-0.001	85.623	j
707.8	73,4	.ñ481	106,297	106,297	106.297	-0.00	106,297	•
707.8	72,9	•ñ\$52	126,420	128,425	128,420	-0.000	128,420	
707.8	72•5	•ñ612	148.647	148.647	148.647	-0 • ō ō ō	Ĩ48+647	

TARE DIFF. PRESS # -3.60000E-04 + -3.37610E-02 (ACFM) + 6.33359E-01 (ACFM) ##2 .

0 (ACFH) \*\*3

# TABLE 18 FLOW ŘÁTE VERSÚS DIFFERENTIAL PRESSURE

ORIGINAL								. PAGES			
Ä					TABLE 18				8/2/76		
<del>O</del>				PLOW ŘÁŤ	TABLE 18 E VERSUS DIFF	ERENTIÄL	PRESSURE	DIFFE	RENTIAL PRESSI		SUS
PAGE		ř	EST NUMBER 6	PĀŔŤ	38.	TESŤĎ	ESCRĬPŤÍON—	IMPAC	T_CYCLES. TES	JRE DATA PRIOR TO G ST_SPECIMEN (S/N_02 PSIA (NOMINAL)?	
PAGE IS			řésť s	Pečimen inl	ĖŤ CONDITIONS	*****	****	 ėnėtrėnė		ŅĘŢ', DĬĘFĘŖĖŅŢ	TĂLI PRESS:
P(	RESSURE	* ***	TEMPERATURE	***	****		-FĽOÙ RĂŤE	*******	*****		
			- <u>-</u> -	nina ä	LĬŤĖRS/	- ÁĞÊM	SĆFH	GNŽ KĠ∠HR	GŃŽ ĽBS∕NŘ	KG/SQ CM DIFFERENTIĂL!	PŠÍŌ:
KG/SQ :		_	DEGC	DEG. F	94.8	- 4GPM	2.933.	5.776	īž. īšš	īġ•Àġ6Š	ĩĂố: 0ĩ5'
Š0+0			ĕĕ• <b>4</b>	72.3 71.9	76.1	• 056+6.	. Ž.634	5.186	- <u>1</u> 1.433	8.9377	_ <u>126.840</u>
\$0.0 \$0.0	•		ŽŽ•2 ŽŽ•õ	71.7	66+5 ~	•0479	2.113	4.554			105.465
•		-	22.0 22.0	71.6	57.3	.0417 .	ĭ.999	3.937		6.Îōóś	664773
49.70 49.70			22.0 ŽŽ•Ì	71.8 71.7	47.45	ñášB	I-668	3.284	- 7. žio	4.7864	68,079
49.7			<u>5</u> ≨•3	72.0	44.45 44.4	0276		2.6ñ3	5.776	3.5786	50.99E:
49,7			22.5	72.5	Žė+8	+0213	ī.ōžī	_2.0 <u>1</u> 0	i.ă.i	2,6 <u>1</u> 27	37, ļēĒ;
49.7			22.7	72.9	24-1	.0179	857	1.688			
49.7			22•1 Ž3•1	73.5	ī9.4	•0 <b>1</b> 44		1.369		<u> </u>	<u>23.006:</u>
49.7			23.3	74.ō	-13.2 -	0099	. ĂŦĀ	.913.		ī.0379	<u>ī</u> Ā.,763
Š0.0			23.9	75.Ī	13.0 -	. • à 098		922	žñ33	î.òàīë	ŢĂ.676.
50+Ó			Ž3.9	75.ī	20+0-		žī6	_1.639	3.107		ŽĂ. 16Ž
50+0			Ž3.9	75.ñ	Ž <b>4</b> •1	-•0179	856	1.686			30.032
5 <b>9</b> •0		_	23.8	74,9	29.1	•0214-		2•02 <del>1</del>			j7.62 <del>4</del>
, 50.0	_		- 23.7	· 94v6	36.2			2.651	Š'• ÓÊ'	3,6717	ĕĕ; 2 <b>2</b> 4.
, <del>.501</del> 0. 49.7			23.5	74,ž	47.1		i.656	3.261_	<u>7.</u> 789	<del>^</del> .7776	
49.7			23 <b>.</b> 2	73.8	56.1	.0410	ī.962	_3.862		6.ñĭ99	
49.7			23.0	Ž3,4			Ž.304	-		7.4734	106.297:
Ā9.7			22.7	7Ž.9			2. <sub>6</sub> 45			9.0ž88	126.420
49,7		_	22,5.	72,5	-		ž.933				<u>T</u> 48\647
49.8	-		žž•9	73.3				<del></del>	······································		
.ì		_	•6	ĭ.ī	DEVIATIONS						

PAGE: 1 DATE: 8/2/76

	TABLE 19	2 700 mmm	
FLOW RATE V	LRSUS DI	FFERENTIAL	PRESSURE

CLEAN CONDITION-IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. FLOW RATE VERSUS TEST NUMBER 6 PART 3A TEST DESCRIPTION DIFFERENTIAL PRESSURE DATA PRIOR TO GN. IMPACT CYCLES. TEST SPECIMEN (S/N 021) INLET PRESSURE 1000 PSIA (NOMINAL).
TEST PECIMEN INLET CONDITIONS. FLOWMETER CONDITIONS \*\*\*\*\* TEMPI (DES F) FLOW BATE RESSURE ŢEMĒ (DEG F) CACEMI (ACEML \_\_ (PSIA) (PSIA) \_\_(DEG\*\_E)\_\_. , <u>43</u> 81.6 ك و يود 76,5 41.2 1011.0 70.0 .0412. .90 .0379 .15 70.6 75:6 .80 44.7. 80.8 1011.9 \_\_ 78.2. 1011.9 80.1 77.46 • 9336 \_752l. •71 \_\_\_He7. . 40£-79.9 1007.9 77.5 .0290 ·÷Β ? y. 6 \_\_\_ 75:1 .60 49.3 79.9 \_\_\_\_\_1007.9 77,5 .0244 .48 70.4 75 1 49.9 .50 80.1 1007.9 77.9 .0197 . . . . . . . . - Y.4.\_\_. 75,6 44... 80.1 1007.9 78-0 .0153 15. 24.4 50.1 .7620 .31 \_\_\_78-2\_\_ 80.2 \_\_\_\_ . 1007.9 . •56 ⊋y.8 , 7623 · 26 50.4 .... - 01 m 78.4 50.2 80.3 1007.9 ----.0104. ٠٤١, 24.P 76 • 5 .20 80.6 1007.9 :14 9 v • 4 77:3 و1: . . 50 . 2 . 78.9 · 0048 • <u>1</u>4 27.2 7727 49.7 8.0 • 3 1007.9 79.0 .0068 •13 80.1 1007.9 78,7 .0105! .61 7 v . d . 77,4 .21 50,1 47.1 79.9 1007.9 78 ± 4. 10124 • 25 77:0 - 25 49.5 17.7 76.5 49.5 79.6 1004.0 78.0 .0150 ٥٤٠ .30 77.4 .0197 47.5 79.2 1004-0 +40 75.6 ... ·40 42.1 02.3 147 47.5 7427 .50 \_45.7 78.6 1004.0 76.6. \*p# 47.2 77.9 1004.0 75.6 .0291 73,7 48.7 .6j 77.3 1000-0 75-1 .00 1212 . 7.2:9 £74. .40.3 •0334 1000.0 . 15 74.6 7200 .80 48.5 . 76•5\_\_\_\_\_ \_\_\_7423 . 10384: 75.7 73,5 ±84 77.9 71,2 •9 l 47.8---1000.0 .0487

PAGE: 2 DATE: 8/2/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION-IMPACT/FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. FLOW RATE VERSUS
DIFFERENTIAL PRESSURE DATA PRIOR TO GN,
IMPACT CYCLES. TEST SPECIMEN (S/N 021)
INLET PRESSURE 1000 PSIA (NOMINAL).

רבּפָּד יעטאפָבּאָ 6

PART 3A

TEST DESCRIPTION

PRESSURE PRESSURE	(nče• Ł) ĭFWb ĭAG	FLOW KAIE	GRUSS DIFF. PRESS PRIMARY (PŠIŲ)	GRUSS DIFF. PRESS SECONDARY (PSID)	DIFF. PRESS	DIFF. PRESS	OIFF PRESS	 
TÖİTÖĞ	79 <u>•</u> ₫	.412	99.009	99.009	99.009	<b>~</b> 0•000	99.010	
iñīj"ă	iais	•03( <sup>9</sup>	67.853	88•593	88 . 443	#0.000	88*553	
rofrix	1126	.0346	75.014	75,967	75.482	-0.000	75.490	•
1007:3	11.5	• 05Å0	61.656	62.749	eś• řēš	70.000	62,183	
100/5%	<u> </u>	<u>•</u> 0244	49.391	50.083	42.131	-0.000	49.738	- —- d
1007.7	11.9	١٥١٦٢.	38,54u	38. J25	,3ñ ° ŏ³ξ.	<del>-0</del> -090	38°63S	
100/=2	( <b>þ</b> ••)	ë#1⊅3	28,387	28.486	28,43(	#0-000	28,437	
100/-2	(a*5	• u1 49	22.992	53°032	23.014	#0 <u>*</u> 000	23.014	~
10015%	/8 <u>*</u> 4	,014	17.597	17:594	17.595	404000	17.596	
1001-5	[8.9	.0008	10,810	10,849	10 65	#0 <u>*</u> 000	10.829	
100/42	19:0	• 00òa	10.694	10.792	10./44	70,000	10.743	 N
100152	18•7	10105	17.887	17.994	17.24	-0 <u>.</u> 000	17.941	
1001°3	10.4	.0144	21.890	~ 22.003	21.947	<b>=</b> 0*000	21.247	
1004.0	ìg∓0	<u>.</u> 019.	27,575	27.739	5].601	-0.000	27.657	_ <u></u>
1004.4	1124	.0177	38*366	38.609	38,487	<b>₩0</b> <u>4</u> 000	38.488	
1004-9	16.6	+0243	48, 391	49.452	49.174	#0±000	49.172	
1004=5	<u>(5≛8</u>	•05ĂI	62.407	63 <u>°</u> 085 . —	eś•ijō	#0 <u>*000</u>	62,716	 1
1000-0	(5 <u>.</u> 1	·0344	,3°665	74.704	Ť4 <u>.</u> 298	-0.000	74.298	•
TÖÖÖĞÖ	14 <u>∗</u> 3	• 4:304	88,342	89.224	89.783	-0±000	88.753	
1000-2	/ <sub>3</sub> *5	<u>•</u> 0447	103.744	103.744	103-144	₩Q.000	103:744	

TARE DIFF. PRESS = -1.64000E-04 \* -1.26930E-02 (ACEM) \* 2.48070E-01 (ACEM), 2 \*

PAGE: \$ | DATE: 8/2/76 -

# FLOW RATE VERSUS DIFLERENTIAL PRESSURE

LESI MABEK 6 PART 3A CLEAN CONDITION-EMPACT/FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. FLOW RATE VERSUS
DIFFERENTIAL PRESSURE DATA PRIOR TO CN.
IMPACT CYCLES. TEST SPECIMEN (S/N 021)
INLET PRESSURE 1000 PSIA (NOMINAL).

	***	****	******	TE <u>P</u> T S	PECIMEN INL	enganantingus EI ConDillous	****	****	***	*****	NET DIFFERENT	AL' PREDO
ı	*********		******	LEMPER ATURE	****		*******	****				
	KR\ZO ČW		ń <u>eg</u> K	ŊE <u>Ġ</u> , Ç	Ų€ <u>G.</u> F	LITERS/	ACFM_	SCFM	κρίμμ Gμs	UN2 LB5/HR	KGZSO CM DIFFERENTIAL	- — — — — — — — — — — — — — — — — — — —
	712144	ˈtňjř‡ž	299 <u>°</u> 3	59 • f	79-0	Bo.4	.0412	, <u>787,</u> ş	\$ <b>•</b> 489	12.028	6.9611	- 35 * å f <u>ö</u>
	71.144	1011-2	298.8	25 <u>•</u> {	,8°5	74.2 .	<u>. 0379</u>	2.570	5,060	11.156	622027	88,423
lř	7 <u>4.144</u>	Tājjēg.	298.5	25.4	?7 <u>.6</u>	65.6	. p3 <u>36</u>	2,277	- <u>4,483</u> .	9.884	5,3074	75,490
	jörábá	100\%Z	298.4	\$5•3	".7.±5	2€•0 ″	. <u>.v22</u> 0_	1.959	31451	8.502	4.3719	62.183.
	70.555	1001.3	298 14	25,4	77,5	47 <u>.1</u>	±0244.	1,652	_ 3:25<_	7.170	3:4969	49.(38
	70.225	₹Ãô₹₹	298.7	25,5	<u> 17.9</u>	37.8	<u>0197</u>	1,334	2.021	5.792	2.7161	38,532
	<u> </u>	Fô0}**	298-7	25 <u>.</u> 5 .	. ?p.0	بي وج	<u>. v153</u>	1,037	2-041	<u> </u>	1_9993	28:337
	<u> </u>	Foolas	298.8	25.!	78.2	24.5	<u>•6129</u>	.872	1:/1/	3.785	1.6180	. 23 <u>. 014</u>
ľ	70.465	1001.5	29 <u>8</u> 9	25,8	78.4	. <u>19.5</u> _	0104	.700	1:375	3 <u>•037</u>	1.2371	17,596
	7v°ãēà	1461.5	299.2	\$6°1	78.9	<u>12<u>*</u>1</u>	. <u>.0068</u>	459	•202	1,992	17614	10,529
	70.555	Ť00\#Z	299.3	26 <u>∗</u> 1	79:0	ĵš•p	• 0 0 <u>6 8</u>	<u>. 456</u>	*#55 #454	1.982	<u>.</u> 7553 .	10-143
	70°₽₽⊅	100/02	299 <u>. 1</u>	. 26.Y	78.7	19.8	0105	. 707	1.491	3.067	1.2614	17.741
	70.555	îñŏ\∓g	299,0	Š2°A	78.4	23.4	0124	.834	1.244	3.620	1.5430	. 21.847
	<u>1,6*≯≅</u> 5	<u> </u>	298,7	25,0	78.0	28.4	10150	1,011	7*X5A	4.388	1,9445	27,257
1	70.585	1004.0	298.4	25.4	!7·4	37.7	• 197	1.327	2.016	5 759	2.7060	38.488
	70.555	T004=5	<b>298</b> ,0	24.4	76.6	<b>46</b> •9	.0243	1.637	3:556	7.104	3.4571	49.172
	Žή*÷ặδ	100475	297,5	24.4	75.8	56_2	ិតនិនីរ	1.966	3,471	6 534	\$2 <u>405</u> 4	98#[10 ]
	7 <u>0•</u> 40;	រកប់ពិទុក	297:1	. 23.2	ļ <u>5.1</u>	64.1	<u>•0334</u>	2.248	4:421	9:760	5 <u>•2237</u>	74.498
	70.30 (	1000-7	29616	\$3.5	<u> 7</u> 4•3	7424	- • 0 384	2,589	24753	11.441	0 • 2 · 2 1	6 <u>0. (83</u> .
-	70 du/	1000 0	296.2	23.U *****	[3.5 *****	83.1	<u>• 427</u>	2 <u>.887</u>	<b>÷</b>	75 <sup>2</sup> 230	7 <u>.</u> 2340	103.155
	70.155	Ţñóĕ*B	298.4	25.2	77.4		······································				the second was well as the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the second was a second with the secon	
	řštř	₫•₽	•7	• ?	1.2	DEALVILONE						

TABLE 20 FLOW RATE VERSUS DIFFERENTIAL-PRESSURE FAGE: 1 -- DATE: 8-24-76

TEST NUMBER 6

m .

PART 3G

CLEAN CONDITION - IMPACT/FLOW RATE VERSUS
TEST DESCRIPTION DIFFERENTIAL PRESSURE. FLOW RATE VERSUS
DIFFERENTIAL PRESSURE DATA AFTER 100 HIGH PRESSURE GR2 IMPACT
CYCLES. TEST SPECIMEN (S/N 021) INLET PRESSURE 415 PSTA NOMIN

CYCLES. TEST SPECIMEN (S/N 021) INLET PRESSURE 415 PSIA NOMINAL.

IEST SPECIMEN INLET CONDITIONS: FLOWMETER .CONDITIONS FLOWMLTER ONE FLOWMETER TWO AVG AVG. ELOW RATE ÉLDN RĂŤE (ACEM) PRESSURE TEMP. FLOW RATE .. PRESSURE . TEMP PRESSURE. TEMP. (PSIA) (DEG. F) (PSIA) (DEG. F) (PSIA) (DEG. F) (ACEM) .85 50.2 76:4 .91 48.3 78.0 420.8 77.2 ·1031 76.B •76 00.4 76.2 •80 48.9 77.4 420.1 .0923: 76.4 .67 419.5 .0800 50.1 76.1 •70 48.7 76.6 .58 49.9 76.8 419.5 76.5 .0697 48.9 76.1 •60 84:5 .0579 • 49 49.9 419.5 .49 49.3 77.3 76 B 76:3 .40 **19**•5 77.2. .0462 58.4 .40 49.9 77.8 76.6 77.6 .30 54.4 .30 419.5 76.8 50.1 78.4 . 0350 • 26 49.9 77.) • 25 49.9 78.9 419.5 78.0 .0302: •21 .0245° 50.1 77.3 .20 49.9 79.2 119.5 78.2. .14 50.Z 79.3 420.1 .0156 77.6 78.5: .13 50 . 1 .13 50.1 78.3 .13 50.1 79.5 420.B 78.9 .0135 . 22 79.1 49.9 49.9 · 0257 1: 78•4 .21 79.9 420.8 ittii <u>•</u>25 50.2 78.5 .24 50.1 79.9 8.054 79.2 .0293: .32 50.S 49 • 9 420.1 79.2 . 0375 78.4 •31 80.0 .0479 • 40 56.2 78.2 •40 49.9 79.9 420.1 79.1 36 โยร \_ •49 50.4 78.0 •50 49.7 79.B 419.5 78.9 ·0594 •5B 50.1 418.8 78.8 77.8 •60 49 - 1 79.7 .0698: 79.5 .67 50.1 •70 77 • 6 48.7 418.8 78.6 .0803. • 0919 •76 78-3 20.2 77:3 •80 48•5 79.2 **+18-2** į iosi 50 4 . 84 77.3 .90 48,5 79.0 417.5 78.1 31. 88 Þ

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2

•	TEST SP	ECTMEN INLET C	CONDITIONS -		A11 F AND AND AND AND AND AND AND AND AND AND	DIFFERENTIA PRESSURE GN	L PRESSURE. FLOW L PRESSURE DATA A 2 IMPACT CYCLES. NLET PRESSURE 415	FTER 100 HIGH TEST SPECIMEN
		,,,,,	**************************************			., -, -, -, -,		
		AVG .	AYG	GROSS	GROSS DIFF. PRESS .	AVGBROSS	ÍARE	NEŤ
	PRESSUME (PŠĪA)	TEMP (DEG. F)	FLOW RATE	PRĪMARY (PSID)	SECONDARY (PSID)	DIFF. PRESS	DIFF PRESS	DÍFFL PRESS' (PSID)
	420 <u>•</u> B	?7.2	,1031-	135,057	135_057	135-057		135+056
	420·1	76.8	- · .6923	•	113,250	113,250		113-248
	419.5	76.4	+0800	- 90.847	91,443	91.145:		91;143:
	419.5	76.5	0697	- 74,443.	75.008	74.726		
	419.5	76.8		57', 184	57,626	57.405		57.404
	419.5	77.2	.0482	45,213	<b>↓5_3</b> 95	45 <sub>•</sub> 30 <u>4</u> ·		45:302
	-419.5 .	77.6	0360	31,,133	31.224		000	31.177
	<u> </u>	. <u>78</u> ±0	0302	24.8764-	24-908	24.892		24-890
	419 <u>.</u> 6	7 <u>8</u> •2		19.024	19.005	- 19-014		
	420.1	78 <u>.</u> 5		11,144:	11.172	-11+15 <u>@</u>	:=0.000	- 11:156:
	∳50∓ត	78 <u>∙</u> 9		11.144	11.229	11.186	:=0+000	11-185
	420 <u>.</u> 8	79.1	+0257-		20.437.	20-36B		20.366
	420 B	79 <u>.</u> 2	•0 <b>5</b> §3	24+064	24.162.	24.113		<u> </u>
	420 <u>-</u> 1	19.2		32.755	32.891	32.823		32.422
	<del>*</del> 50*†	?9 <u>•</u> 1	·0 <del>47</del> 9	45_039	45,222	45,130	000	45 <u>-</u> 125
	419-5	78 <u>.</u> 9	0594	59+315.	59 <sub>+</sub> 838	. 59.576		59,575
	_ <u>418-</u> 8	78.8 .		74 <sub>+</sub> 816 <sub></sub>	75+640	75+228		75,227
	<del>ijä⁵</del> ā	a≛e		<u> 91,33</u> 4_	92,391	31 <b>-</b> 8ēš		91,261
	<u> </u>	7 <b>6.3</b>	0919	- 112,302.	112,302	115 <del>-3</del> 05		<u> </u>
	41725	78 <u>.</u> 1	· — <del>-1031</del>	134,741	134,741	134.741		<u></u>
		TARE DIFF. P	RESS = =3 <u>.4</u> 0000E <u>=0</u> 5	_+ =4.44000E=04 (	AÇEM) + 1.50993E≘01	(ACFM) ##2 -+-	0 (ACEMS)	#é2
		AA**A		THE THEOREM PROPERTY AND A	užžiu , stankažezaš	in graff, Arriger in 19 and		7 2

FLOW-RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3

TEST NUMBER 6

PART 3G

CLEAN CONDITION - IMPACT/FLOW RATE VERSUS
TEST DESCRIPTION DIFFERENTIAL PRESSURE FLOW RATE VERSUS
DIFFERENTIAL PRESSURE DATA AFTER 100 HIGH PRESSURE CN2 IMPACT

DIFFERENTIAL PRESSURE DATA AFTER LOU HACH PRESSURE 415 PSIA NOMINAL.

CYCLES. TEST SPECIMEN (S/N 021) INLET PRESSURE 415 PSIA NOMINAL.

NET DIFFERENTIAL PRESS: TEST SPECIMEN INLET CONDITIONS TEMPERATURE PRESSURE FLOW RATE GN2 KGYSD CM LITERS/ KG/HR KG/SQ CM MIN LOS/HR DIFFERENTIAL PSIp. PSIA **ACFM** SCFM DEG. K DEG. C DEG. F 135.056 .1031 5.735 29.584 420.5 298.3 25.1 77.2 83.7 2.913 124643 9.4953 29.538 420.1 298.1 76.8 2.605 5-129 7.9622 113.248. 24.9 74.7 .0923 11.308 9.798 91:143. 29.493 419.5 297.8 24.7 76.4 64+4 .0800 2.257 4=444 6-4080 .0697 29-493 419.5 297.9 24.7 76.5 56.0 1.966 3.871 8.534 5.2536 74.724. 7:079 29,493 419.5 298.1 24.9 76.8 .0579 3.211 4.0359 57.404 46.2 1.631 29.493 419.5 298.3 1.358 2.674 5.895 45.302; 25.1 77.2 38.3 .0482 3, 1851 28.4 44402 25.3 31.177 29.493 419.5 298.5 77.6 .0360 1.014 1.997 5. 1050 29.493 419.5 298.7 25.5 78.0 23.9 .0302 .850 1.675 3.691 1.7500 26.890 25.7 .0245 .687 1.353 419.5 2.983 19, 913 29.493 298.8 78.2 19.0 1,3367 .7B44 29.538 299.0 25.8 .440 11.156 420.1 78.5 12.0 .0156 -865 1.909 420<u>.</u>8 .858 29.584 299.2 78.9 1.492 .7864 11.165 26.1 11.9 .0155 .436 29.584 420.5 299.3 79.1 .0257 .724 1.425 8-144 1.4319 20,366 26.2 20.3 26.2 .0293 .825 29.584 420.8 299.4 79.2 23.0 1.624 3.580 1.6952 24, 112; 29.538 .0375 1.052 420.1 299.4 79.2 2.072 4-569 2.3076 32,822; 26.2 29.5 29.538 420.1 299.3 26.1 79.1 38.O .0479 1.345 2.648 5.839 3.1729 45, 129 29.493 419.5 299.2 78.9 5.74 .0594 1.666 3.280 7.232 4-1885 59,975! 26.1 29.447 418.5 299.2 26.0 78.8 55.8 -069B 1.957 3.852 8.493 5.2890 75.227 2.251 29.447 418.5 299.0 25.9 78.6 64.3 .0803 4.432 9.771 6.4584 91.861. 29.402 418.2 298.9 25.7 2.574 5.068 11:174 7.8955 78.3. 73.8 .0919 112-300 29.356 417.5 2.884 298.8 78.1 5.680 25.6 83:1 12.522 9.4731 134+ 739 •1031 ####÷ \*\*\* **使性療性特別** כבנט .29.504 419.6 \_78+1.. 298.8 - 25-6 DEVIATIONS. Þ

PAGE: 1 DATE: 8=24-76

186.

### TABLE 21 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 6 PART SE-

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			<b></b>	******	FLOWMETER TWO	****	**********	FLOWMETER ONE	*******
 	FLOW BATE: 	. TEMP (DEG: F)	PRESSURE (PSIA)	ŤĖMP (DEG. F)	PRESSURE:	FLOW RATE	ŤEMP (DEG• F)	PRESSURE (PSIA)	FLOW RATE (ACFM)
	<del></del> ō6ōġ	<del>71</del> +0	719.6-	73.4	47.4	•92	6A•7	49.5	.88
- <b>-</b> [	+ö <b>5</b> 39 <u></u> -	- · ~ ~ <del>-</del> 7ō+ó	715.7	72.4	47.8	- •81	67 <b>.</b> 6	49.5	.78
- <del></del>	- ō473	69.7	7īs <sub>v</sub> ỹ	72. ·	48.3	•Ŷē	67.4	49.5	.69
		69 <u>-7</u>	775.7	72+ñ	48,5	•60	67.5	49.5	•60
_		ŽÕ. <u>Ī</u>	715.7	72.2.	48.9	511	67.9	49.7	.50
_  <del></del> }		- <del>- 7</del> 0.5'	7 <u>11.</u> 8 -	72.6	49.1		68+4	49.7	•41
	0ŽĮŠ'	- <del>- 7</del> 1.3	7 <b>11.</b> +8	73.2.	49.7	30	69•3	49.9	.31
ļ		-7ī₊é	711.8	73 <b>.</b> 6	49.9	.25	69.0	50.1	.26
_	.0145	7ž <sub>+</sub> ś	711.8-	74-3	49.9	•50	<b>7</b> 4.€	49,9	.21
_		- <u>- 73.</u> 2	715.7 -	74.B	50.4	·i3	7ĩ•6	50.4	.14
-fn:	šėôò+	<del>7</del> 4.ä	715.7	75.7	49 <b>,</b> Š	13	72.8	49.7	.14
_		<del>-7</del> 4•2	7·15.7.	75 <b>.</b> 7	4949		72•7 -	50.1	.22
_¦			715 <del>-7</del>	75.7	· · · · 50 • Ī~	•26-	72.5	50.4	•27
101		·74 • ō	7.15.7	75.6	49.9	31	72.3	50.5	.32
_ <del></del> ∔		<del></del> 73.6	<del>-7</del> 15.7	75 <b>+4</b>	49.9	40	ŤĨ•8	50.2	•41 -
		73.3	. 715.7	75.2-	49.3		71.3	50.1	50
		72.8	. 7jš.7	74 <b>+</b> 8	48.9	•60	7n.8	49.9	•60
<del>-</del>	ò4ĕž	<u>7ž</u> +3′	7īī-8	74-4	48.7	· <del>-</del>	76+2	50.1	•69
		-71+7:	711.8	73+8	48.5	<b>.</b> 80	69•6	50.2	.78
		7ī.è		7̂3•2.	47.9	•90	69.2	49.9	.87

1.1			1	FLOW RATE VERSUS DI	FFERENTIAL PRESSÚ	RE CLEAN COND.			
13	TEST SP	ECIMEN INLET CON	TESŤ NUMBER 6	PARŤ ŠF.	TEST DESCRÌP	TION DIFFERENTIA	TIONIMPACT/FLO L PRESSURE. FLOW L-PRESSURE-DATA-A 12 IMPACT CYCLES. NLET PRESSURE-700	RATE VERSUS	
	PRESSURE (PŞIA)	AVG TEMP (DEG. F)	AVG Flow Rate (4CFM)	OROSS OIFE PRESS PRIMARY (PSID)	GRASS . DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS. (PSID)	TARE DIFF+-PRESS (PSID)	NET DIFÉL PŘESS (PSIO)	- ; - ;
	719.6	71.0	.0603	63,110	63,525	63,317	-0.000	63,318	·····
	715.7	70.0	.0539	54,327	54,676	54 <b>.</b> 502	-0,000	ŠĂ, SôŽ	ł
	715.7	69.7	,r473	46,159	46.143	46,151	-0.001	46,131	<del> </del>
.5	715.7	69.7	.0409	38,269	38,339	38.304	-0.001	38.304	";
	715.7	70.ĭ	• ñ345	30.727	30.802	30.765	-0.001	30.765	
	711 <b>.</b> 8	70.5	, n281	23,476	23,455	23,465	-0.001	23,465	
	711.8	71.3	,1215	16.804	16.811	16.80B	-0.001	16.806	<del>-  </del>
	711.8	71.8	. 181	ĩ3,556	13.6 9	13.582	*0.00Î	Ĩ3•383°	
	711.8	72.5	, ^145	10.249	10.239	ī0.244	-0.001	10.244	
	715.7	73.2	.ñn95	6.304	6,313	6.303	-0.001	6,304	<del></del> †
٠,	715.7	74.2	\$600.	6.13.	6.189	6.159	-0.001	6.159	
	715 <b>.</b> 7	74.2		10.829·	10.924	10.877	=0.01	ĨÓ.877	_
	715.7	74.1	.^188	14.310	14,4å9	14.360	-0.001	14,360	<del> </del>
ñ	715.7	74.0	.rŽ19	17,384	17.498	17,441	-=0.001	17.441	
	715.7	73.6	284	23.882	23,971	23,926	-0.001	ž3.9ž6	<del></del>
	715.7	73.3	.0350	31,307	31,434	31.371	-0.001	31.371	<del></del>
	715.7	72.8	.0411	38,617	38,8ññ	38.709	⇒0.00ī	38.709	<del> </del>
	711.8	72.3	.0482	47°.087	47.091	47.089	-0.00 <u>0</u>	47.089	
	711.8	71.7	• ^549	55 <sub>4</sub> 457	55,940	55,698	÷0.00ô	55,699°	<del> </del>
.,	711.B	71.2	.06^8	63,611	64.157	63,884	-0.000	63,864	-  33 <u>:</u>

TARE DIFF. PRESS = -3.60000E-04 + -3.31610E-02 (ACFM) + 6.33359E-01 (ACFM) ++2 +-Õ (ÄČFM) ++3.

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PAGE: 3 DATE: 8-24-76 TABLE 21 FLOW RATE VERSUS DIFFERENTIAL PRESSURE CLEAN CONDITION - IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA AFTER 100 HIGH PART -3F-TEST DESCRIPTION TEST NUMBER- 6-PRESSURE GN2 IMPACT CYCLES. TEST SPECIMEN (S/N 021) INLET PRESSURE 700 PSIA NOMINAL NET DIFFERENTIALI PRESS! TEST SPECIMEN INLET CONDITIONS TEMPER TURE FLOW RATE. PRESSURE \*\*\*\*\*\*\*\*\*\*\*\*\*\* GNŻ KB/SQ CM LÍŤERS/ ŘŠIĎ: KÖ/HR - LBS/HR-DIFFERENTIA - SGFM . KG/SQ CM PSIA MIN · CFM DEG. K 63,378 21.7 -71.0 2.947 5.802. . . . . . . . . . . . 791 50.594 719.6 294.9 83.6 .0603 54.562 50.318 715.7 -21-1 - - - 70-6 74.3 .::539 2.626 5.171 --11.401 294.3 46-151 715.7 65.2 -0473 -2-305 50.318 294-1 1.991 3.921- - -69.7-50.318 715.7 294-1 21.0-56+0 .0409 3.310\_\_ \_Ť-29Ť ž.ĭċġñ 30.765 .50**.3**18 -.0345 1.681 ---715.7 294.3 22.465 \_2.676...\_ -A28i 1-359--50-041-711.8 294.5 -16.506 . - 1-039. -2+045. ... -4+508. --... -21.8------ · 71.3 ----0215 50.041 711.8 295.0 28-8 3.789 ī3:503 -22-1----71.8 .aīBī 1.718\_\_ 50.041 711.8 295.2 <u> 70,244</u> --698 . -1.375..... 3.632 50.041 711.8 295.7 . 145 \_\_\_\_ \$0.0 .... \$0.0 J 6.304 50,318 715.7 \_\_22\_9\_\_\_\_\_\_73\_2\_ - \_\_\_ 12.5 .0095. 296.1. 6.159 ,433ī -0092 Š0.318 715.7 296.6 10.877 \_0150-50.318 715,7 1.0096 . **14**~260. .715.7 -25-1 - . -0188 - -----50,318. -<u>ī7.44ī</u> Ĩ.2Ž62 1.056. \_.2.080. \_Š0.318 715.7 .0219 ---296-5 ž3.926. 2.702 5.956 Ī-682Ž -1284 \_50.318\_\_\_\_\_715.7 . 296.3 31.371 7.347 Ž.ŽnŠa 47.5 \_\_\_a35n\_ .ī.692 3.332 50.318 ... 715.7 296.1 2.7215 -7ž<u>-</u>8-.041Ï 1.992 .... 3.922.... -8-648 38.759 56.0 . . 50.318 715.7 295.8 3.3107 <del>47</del>, 089. <u> 78-891</u> 65.5 -0482 2.325 4.577 \_50.041 · 711.8 -- 295.5.

.0549

.0608...

74.9

83.2.

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2.650.

...5.218\_ .\_ \_11.504

3.9160

55,699

يَفَقَاهُ خَدُهُ

22.0.... 71.7

71.2

72.1

1.4

....2<u>1</u>,8.

22.3

.8

50.041

50.041

50.235

.135

JU

711.8

711.8

714.5

1.9

295.2

294,9

295.4

•B

PAGE: 1 DATE: 8-24-76

### TABLE 22 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER ... .... PART .3E.

ENTIAL PRESSURE

CLEAN CONDITION - IMPACT/FLOW RATE VERSUS

DIFFERENTIAL PRESSURE. FLOW RATE VERSUS

TEST DESCRIPTION. DIFFERENTIAL PRESSURE DATA AFTER 100 HIGH
PRESSURE GN 1 IMPACT CYCLES. TEST SPECIMEN
(S/N 021) INLET PRESSURE 1,000 PSIA NOMINAL.

• • • • • • • • • • • • • • • • • • • •	FLOWMETER ONE		444444444	LOWMETER TWO						
****	**************************************	**************************************		***	· 我你你你会会会会		(			
FLOW RATE (ACFM)	PRESSURE (PŠĮA)	ŤEMP (DEG <u>•</u> — <del>F.</del> )	FLOW RÅTE (AĞFM)	PRESSURE, (PSIA)	TEMP. {DEG↓-F}	<del></del> .	PRESŠÚŘE – (PŠIĂ) —	TËMP' 	FLOW BATE	
•84	50.1	8 <u>2</u> .0	•91	47.9	85.9		ī4ī5.9 -	ėi.		
•75	49.7	8ĩ <u>.</u> 4 -	81-	47 <del>.</del> 9	85+6		ī -15.9	63.5	ō375!	
• 66	49.7	8 <u>7•</u> 1	· 70- ·	48.3	85•Ž		-Ĭ4 <u>Ŧ</u> 5 <sub>#</sub> 9;			
• 58	50.2	80•9 -	61	49.3	85 <u>.</u> ñ		1015.9-	63.0	ōĕġĪ`	
<b>.</b> 49	50.1	81.1	50	49.3-	85 <sub>•</sub> a -		-1a15.9:	83+ò	0ŽĂ3:	
•40	49.9	8 <u>1</u> •s· ····	40	49•3	84+9		-1415.9			
•30	49.5	8ī•7 · ·	30	49 <b>•</b> Ĩ	85 <b>.</b> 2.		īnīš.9 -	83.5	<del></del>	
•25	49.9	82.2		49.5	85 <b>.</b> 4		1015.9	63+8		
•21	5,1	82•6 · ·	<del>-</del> <u>21</u>	49.9	8 <b>6.7</b>		1=15.9		÷ōĪōž:	
•15	49.7	83 <u>•</u> 3		49.3	86+4 -	- ,	-1015.9.	84.6		
•17	49.5	84•6	76	49.3	86+5		- 1015+9 -	85.6:	ŏöśō	_
•55	49.5.	84•7	22	49•ĩ	86+8		inīs.,9	ėš•ė	ōīō <del>7</del> '	
•26	. 50-1	-84•8	<u>.2</u> 6	- 49.9	- 86.9		— Ĩ÷ĨŠţ9———	85 <del>.</del> 8		
.30	49.9	84.5		49.5	86.7		Ī015.9	85+6·	8ĂĨŎ	_
40	50.2	-83 <b>-</b> 9	40	49 <sub>+</sub> 9	- 86.5			05.ž	•ii99	_
• ∳8	50.4.	-83•Ž		. 49 <b>.</b> 9	86+2		_1:15.9	— ė <b>i.</b> 7		
<b>∙</b> 58	50 <b>.</b> 2	87•2	60-	49.1	85.6		- 141549	83.9		
•67 -	50.4 -	-8 <del>1:</del> 4		·49+1	·85		—Ï-\Ī5 <b>v</b> 9——	<u></u>	<u> </u>	
.75	50.4	80.7	+80	48.7	84.6		īaīś.9	85.4	. 6379 <sup>1</sup>	
84	50.4	- Ĩ•ñ8		48.3.	19 <b>3.</b> 9		<u>Inī</u> 5.9	<u></u>		

-		AL 18.2000 E	W. Z J				PAGE: 2	-24-76
_		<del></del>		TABLE 22		lĎc		
		_	ESŤ_NUMBER_6	PÄŘŤ jE	TEST DESCRIP	DIFFERENTIA DIFFERENTIA PRESSURE GN	TION - IMPACT/FLO L PRESSURE. FIOW L PRESSURE DATA A 2 IMPACT CYCLES. NLET PRESSURE 1,0	RATE VERSUS FTER 100 HIGH TEST SPECIMEN
	TEST SP	PECIMEN INLÉT CON	DITIONS <del>Amaricania</del>					
	PREȘSURE	AVĠ -TEMP	ÁVG ÉLOW-RATE	DÍFE: PRESS		ĕVe GROSS.	TARE!	Dīķeļēķes:
	(PŠIA)	(DÉG. F)	(ÃĈFM)	(PSID)	(PS10)	(PSID)	(PSIO)	(#51D):
	1015,9	83.9	.0420	45,946	45.769	45,85 <u>8</u>	-å.ōoā	4546591
	1015,9	8 <b>3.</b> 5	.0375	39,689	39.8 7	39,748	ô.ōoō	39°746:
_	1015.9	83.1	.0327	33,315	33,367	33,341		334341.
	1015.9	83.0	.0291	28,622	28.6°Ž	28.612:	. <b>⇔</b> 0 <b>6 0 0 0</b>	ŽŠ+6ŽŽ:
	1015.9	83.0	.0243	ŽŽ;,ŤŤ?	22,758	22,764·	.÷ô.√ô.0ā	'ĕĕijŤġ <del>ŏ</del> '
	1015.9	83.1	•ò194	ĨŤ.3Ž4·	17.324	Ĩ7.32 <u>*</u>	-0.000	ĬŤŗĠŹĂ:
	1015.9	83.5	.0146	ĨŽ,16Ť	12,128	ĨŹ <b>.</b> 148	. <del>-</del> อ๋⊌อ๊ออ์	řž. į 40.
• •	1015.9	83.8	.0124	9,968	9,984	9,906	0-000	÷690\$1
-	1015.9	84.2	.0102	<b>Ť</b> :88ô	7.852	'7.866'	·=0.000	7.866·
•	1015.9	84.6	.0079	5.852	5.859	5.855'	·=0.000	5,256,
•	1015.9	85.6	.0080	ś <b>.</b> 852'	5,859	5,85 <del>5</del> ,	ò.jōōō	54856
-	1015.9	85.8	.0147	8,343.	8.365	8.354	-0.000	·\$\\\$\\\
	1015.9	85∙8	.0127	īō.197	10.246	Ĭ0.222	·+0.000	Ĭô,ŽŽŽ;
	1015.9	85.6	•ñĨ48	īž;jai	12.413	12.377	-04000	ĨŽJ <del>Š</del> ŤŤ
	1015.9	85•2	.õĩ98	ĨŤ.6Ĩ4	17.667	17.640	-0.000	Ĭ7:640
	1015.9	84.7	.0242	22.712	22,758	ž2,735:	·÷0000	žŽ.735
	1015.9	83.9	.0289	Ž8.564∙	28.66ñ	ž8.612	.÷0.00â	`žĎ+61Ž:
-	1015.9	83.3	. 8335	34,532	34,631	34,581	·=0 6 0 0 0	ĠĂĻŞŶĔ:
	1015.9	82.6	. ñ379	40.326	40.44ō	40.38 <u>3</u> .	·#0 • Ö00	40.3\$4·
•	1015.9	82.0	.ò424	46,873.	47.032	46.953.	-0,000	464995:

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			FLOW RAT	TABLE 23 E VERSUS DIFF	ERENTIAL PRESSURE	CONTAMINATED CONDITION PRESSURE. DATA ACQUIR OF SYNTHETIC CONTAMINA	ED AFTER THE AL	DDITION OF 7.9 MG	<del>-</del>
		TEŞT-NUMBE	EK 10 PART	<del>5</del> 46.	TĒSĪ DĒSCRIPĪIO	CYCLES. TEST SPECIMEN			
*****	****	FLOWMETEF	CONDITIONS	******	· 传生并在在农业中的	TEST SPEC	IMEN INLET	ONDÍTIONS:	
****	ELOWMLTER ONE	*****	****	ELOWMETER TW	******		AV6:	ěvo.	
OW RATE	PRESSURE (PSIA)	TEMP (DEG. E)	FLOW RATE	PRESSURE (PSIA)	TEMP (QEG, E)	PRESSURE (PSIA)	TEMPI (DEB F)	FLOW HATEL (ACEM)	_
	>u_5	69.9.		49.2	70 <u>e</u> B	<u></u>	7p_3	07,8 <u>4</u> .	
<b>-</b> ₹60	<u> </u>	69.9	•éj	49.2	70.9	413.7	70 <u>±4</u> -	<u>*4759'</u>	 nu
<u> </u>	<u> </u>	69 <u>*</u> 8	50	49.5	70.9	413,7	70.3	<u>•0607'</u>	
<u>i</u>	żō* <u>j</u>	8 <u>_</u>		49.3	70-9-	41327	7ņ <u>.⊬3</u> :	*0491	
•31	>u.5	69.49	•30 <u> </u>	49.9	71 <u>•</u> ?	<u> </u>	70 <u>-5</u> 1	<u> •0371</u>	00 
	<u> </u>	69*6	-25	49.9	71:2	413.7			
- <u>\$2</u> }	<u> </u>	70.20		49.9	71 <u>+</u> 2	413.7	70 <u>+6</u>	±025p	<del></del>
-14	<del>5</del> 1.1	70•2	<u>.13</u>	5 <u>0.</u> 5	71.4	<u> 413.7</u>	<u> 70±8</u>	*0192	<del></del>
	26.3	7.11 = 4	<u></u>	49.9	71 <u>•</u> 7	<u> </u>	71-0	-ojéś	<del></del>
∓šš	<u> 49.7</u>	7.0.≛4		49_3	71 <u>.</u> 7	<u> </u>	<u> </u>	*05èë:	_
	<u> </u>	7 <u></u> 3	<u></u> 2 <u>6</u>	49.5	71 <u>.6</u>	413.7	70 <u>-8</u>	-0315	
<u>•31</u>	#X*ō	7::21		49 <u>.</u> 3	71_6	\$13.7	70 <u>•9</u> ′	0374	_## " "
- <u>*</u>	26°J	69 <u>.</u> 9		49.43	71 <u>. 4</u>	<u> </u>	70 <u>.6</u> .	- <u>•0468</u> :	
- ₹ō	20-1	69.7	<u>5</u> }	49.0		413-0	70 <u>±</u> 5′	<u> •</u> 060ǯ.	
<del>2</del> 55	⇒ō <sup>-</sup> 3	69.7	60	<u>49.0</u>	71 <u>*</u> 1	412,4	70 <u>-4</u> -	<u>, ợ ỹ ỹ ỹ '</u>	_
*ē5	<u> </u>	69_9		4 <u>9.±</u> 2		<u>\$11.7</u>	70 <u>±4</u>	-ēģ <u>1</u> 26.	
					1				<del>_</del>
است بالکائیبی و وییویوبراند		articologia accessor della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della constitución della const		Free transcriptions in the Philippine	4				
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		<del></del>							-01123 -
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			····						PAGE:	3 <del>9-14-76</del>	
				LIANE LABORATION	TABLE 23			-contaminated-	CONDITIONF	LOW RATE VERSUS DIF	FERENTIAL
				FLOW RATE	VERSUS DIFFE	RENTIAL	PŖESSŲŖĘ	OF-SYNTIETIC	<del>CONTAMINANT A</del>	FTER THE ADDITION O	IMPACT
		TE	ST NUMBER 10	PART :	27C	TEST_0	ESCRIPTION	CYCLES. TEST PSTA (NOMINAL	appendix to f	N 027) INLET PRESS	URE = 415
										*	09
***	***	***	TEST S <del>A############</del>	PECIMEN INLE	ET CONDITIONS	***	***	*****	*****	NET DIFFERENT	***
PRESSU	, ,,,,		LEMPERATURE				FLOW RATE	·			
***	****	****	មិនិងមមិស្ <sup>ង</sup> និ <del>មីស្តីស</del>	***	****	****	****	****			
kō/zō čw	PSI A	DEG K	DEG. C	ĎE <b>Č</b> É	LITERS/ MIN	ACEM	SCEM	ĸĕ́ĶĤŘ· ĜŅS	F₽ <mark>2∖Ĥ</mark> Ġ. ĜNS	DIEEEBENTIAL KONSOCCH	- SEYOI -
3 <del>ă • 1</del> 5g	<u> </u>	294.5			62 <u>*</u> 6	. <u> </u>	<del>5•5}</del> 0	<u> </u>	ă <sup>2</sup> 2ă5	<del>Si* jáss</del>	.39 <del>4.838.</del>
29≛083	4131/	294.5	<u> </u>	<u>7</u> 0•4	58 <u>.</u> 1	0729	2-051	<u> </u>	6.905	<u> </u>	255 <u>1 157</u>
<u>\$9,083</u>	413./	294.5	21,3	70,3	48_3	20607	1.706	3.359	7 <u>.</u> 406	12,7555	<u> </u>
- \$ĕ^^0 <u>8</u> 3	<u> </u>	294 5	21 <u>_3</u>		39 <u>*</u> j	- <u>*</u> 0491	<del>1.38</del> 1	<u> </u>	5 <u>.995</u>	<u>-8</u> -₹36 <u>1</u> 6	<u>ijążyą777;</u>
รล้ จ์ฐิรั	413./	294_6	21.4	7 <sub>0.5</sub>	29.5	20371	1.043	2.054	₹-258	<u>्रवे वर्षवस</u>	912566 BIII
\$ <u>\$</u> 083	413./	294.6	21,4		24-4	<u>*</u> û307.	865	1.698	<u>a_74a</u>	·5 <u>*_0786</u> :	72.225
29_083	413./	294.6	<u> </u>	70.6	19•9	0250	Z0Ž.	1,4382,	34047 _	<u>3 3 8 3 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8</u>	<u> </u>
29 <u>+083</u>	413./	294.7	51+ <u>ė</u>	70+B	13 <u>•</u> \$	<u>•</u> 0165	-465	<u>.915</u>	3-017	<u> </u>	· jággsá.
29-083	413.1	294 <u>.</u> B	21.7	71.0	12•9	<u>•1162</u>	-455	897	1.977	<u>\$4</u> 408₹	345520·
−ร์อั•์งชีวี	<u> 413./</u>	294-8		<u>71</u> +0	20 <u>*</u> \$	<u>\$</u> 0258	.723	1.424.	<u>3°1₹0</u>	<u> </u>	28F4581
<u> 58.083</u>	413./	294.8	<u>\$1.6</u>	70.9	25 <u>.</u>	0315	.884	1.740	3-836	<u> </u>	744901:
5 <u>8 • 083</u>	413,/	294_8	21.6	70.2	<u> 29•7</u>		1.051	2.069	4,561	. <u>6⊁2208.</u>	93-175: 18
29.037	<u>413.0</u>	294•6	<u>21.5</u>		38-8	•0488	1,369	2.695	<u>2•845</u>	9+4183	j:33 <u>~959;</u>
<u> </u>	413.0	294.6	<del>2</del> 1• <del>,</del> 4	70.5	48.3	<u>. 0607</u>	1.704	3.355.	7,397	13*0835	1866172;
28,992	412.4	294.5	21.3	70.4	56,9	.0717	2.011	3.954	8.729	17.6058	253 <sub>3</sub> 258:
28.946	411./	294 <u>.5</u>	21.3	70.4	60.9	.v7.69	2.151	4.236	9.338	śj*3śjŏ	3032255:
śã•0 <u>e</u> e	413.4	294,6	21.4	70.6							
• 037	.4	:1	•1	-5	DEVIATIONS						
											<del> </del>

				FLOW RATI	TABLE 24 E VERSUS DIFF	ERENTIAL PRESSURE	CONTAMINATED CONDITION PRESSURE. DATA ACQUIE OF SYNTHETIC CONTAMINA	ED AFTER THE AD	DITION OF 7.9 MG	
-			TEST NUMBE	H 10 PART	270	Ţ <u>Ē</u> ŞŢ <u></u> DĒŞCRIPŢĻON	CYCLES. TEST SPECIMENT PSIA (NOMINAL).	(S/N 027) INL	ET PRESSURE = 100	<u>o</u> វារា
 	********	********		CONDITIONS	*****	***	TEST SPE	CIMEN INLET C	****	
 		ELOWM: TER ONE	•		FIDWMETER TW	0				
<u> </u>		*********	<u> </u>		*********		No-cello-	TEMPI.	FLOW RATE	
	FLOW RATE	PRESSURE	TEMP (DEG. F)	FLOW RATE	PRESSURE (PSIA)	TEMP (DEG. E)	PRESSURE (PSIA)	(DEG F)	(ACEM)	
 	86	70-1	65 <u>+</u> 6		47 <u>_</u> 8	70 <u>+</u> 2	-1013+2	<u> </u>	<u>.0</u> 426₁	
_		50.5	64.0	.81	48 <u>.</u> 4	59.2	<u>ini3-s</u>	<u> </u>	*038Ž.	 
	69	<u> </u>	63.5		49.0	68.7	1013*S	6661	<u>.03+1</u>	
 	.60	49.9	63 <u>•</u> 2	.60	4 <u>8_8</u>	68.4	1013-2	6 <u>5</u> <u>8</u>	* 0\$ <b>8</b> 3;	
_	51	54 <u>.4</u>	63.1		49.5	68.3	1013-S	65.7	<u>ី០នទុំសិ</u>	40 
_		49.9	63.3	40	49 <u>+</u> 2	68.5	<u> </u>	65 <u>'-</u> 9'		
_	.31	50.4	63 <u>.</u> 8	.30	49.9	68.7	j013 <u>+</u> S	66-2:	Tojąć:	<del></del>
_	-26	50.2	64 <u>*2</u>		49.9	68 <u>.</u> 9	j.013-S	66-61		
_		50.1	64.27		49.9	69.2	1017-2	ĕĕ≓ŏ.		
ļ 	15	<u> </u>	65_4	13	49_9	69.5	1017.2	67.4	-007p	
Ĺ	15		66•6		50_1	70.2	1017-2	68è 4·		
ļ_	55	49.9	66.5		49.5	70.1	1017.2	68.3	,0 <u>1</u> 05'	<u>п</u>
 	27	29.7	66 <u>*</u> 3		49.3	7.000	1017.2	68.2	•0130	
İ.	32	50.1	65.9		49.5	69,9	1017.2	<u>.67 • 9'</u>	•015 <del>\$</del> ·	
_		49.9	65•1	.41	49.2	69,5	1017.2	67:-3	,0\$0j	
 	• <u>\$</u> 0	50.4	63 <u>.</u> 8		49.5	68.7	1017.2	66.3.	0247	
Ĺ	60	<u> </u>	63 <u>•</u> 0	60	49.0 -	68•2	1017.2	65 <u>*6</u> '	• 0583	<del></del>
   		<del></del>	62 <u>+1</u>		48 <u>.</u> 8	67•5	1017.2			
  -	.78	49.7	60=9		48.0	66.3	1013.2	63,66	*ožuj	
Ĺ	87	50 <u>1</u>	60-2	91	48 <u>+</u> 0	65.4	1013.2	65*B;	- 04±0:-	
	<b>-</b>		~	•						—i≀i

							PAGE: 2 DATE: 9-14-76	· · · · · · · · · · · · · · · · · · ·
				TABLE 24 FLOW RATE VERSUS DI	FEERENTIAL PRESSURE		ONDITION - FLOW RATE A ACQUIRED AFTER THE	
			Е <u>рт ип</u> мв <u>е</u> й јо	PART_270	ŢĒZĪ ŌĒŽCŔĬŖĪI		CONTAMINANT AND PRIOR SPECIMEN (S/N 027) 1	TO THE GN <sub>2</sub> IMPACT NLET PRESSURE = 10
	***	ECIMEN INLET CON	nitions			·		
			•••	6R0S <b>S</b>	GR/\SS			
	PRESSUKE	AVG Temp	AVG FLOW RATE	DIFF. PRESS	DIFF. PRESS SECONDARY	AVG GROSS	TAREI DIFF PRESS	NET NIFEL PRESS
	(PSIA)	(pĒģ. F)	(ACEM)	(bžíů)	jbžio)	OÎFF. PRÊSS (PSIÔ)	(AZID)	(hēiģi.
	1013.4	67.9	.0426	113,603	113.603	113,603	*0 <u>*</u> 000	113 <u>+</u> 603.
_	1013.4	<b>66</b> •6	.0387	100.628	100,628	joó•ešā	-0-000	100-ë\$ <i>ë</i> ,
_	1013-4	<u>06.1</u>	•034 <u>1</u>	76.592	87.021	81.607	#0°000	67.803.
	1013.4	65 <u>.</u> 8	•0293	62.171	72.149	67.160	#0 <u>#</u> 000	67-160
_	\$.E101	65.7	.0249	49.674	59.807	54.741	<b>≈</b> 0€000	54.741
	1013-2	<u> </u>	•6199	35,624	45,568	40.596	·#0 • 000	-40-596c
_	1013.4	66.2	.0152	33,547	33.623	33.585:	=0°00ô	33.588
	1013.2	ō6•6	.0127	27.464	27.467	27.465	=0 <u>=</u> 000	'27'-465!
	1017.4	66.9	.0104	21,959	<u>22.011</u>	21,985	<b>-</b> 0 ≠ 0 0 0	21: 965:
_	1017.2	<u>97.4</u>	•0070	13,964	13.989	13.976	=0 <u>=</u> 000	13,976
	1017.4	68.4	•0070	13,906	13,989	13,947	#ó•000	13-947
	1017:4	<u>68•3</u>	•0105	22.017	\$5.183	55.100	-0·000	šš⁼jóo.
	1017.4	68.2	•0130	28.101	ŻВ • Э29	28,215.	=0.000	\$8F\$12;
	1017:4	67.9	•6154	38.133	34.199	36.166	-0 <u>+</u> 000	354156
_	1017.4	<u>67.</u> 3	.0201	50.55 <u>\$</u>	46.517	48.53 <u>4</u> ,	-0 <u>-</u> 000·	48 <u>5</u> 53 <u>5</u> !
	1017.4	66.3	.0247	63,166	59,491	ej• <u>35⊊</u>	-0.000	617355,
	1017:4	65•6	•0293	76.105	72.465	74.285	-0 <u>-</u> 0 00	74-285
	1017:4	64.8	•0338	89.397	85.389	87.893	#0±000	87-893:
	1013.2	63 <u>.</u> 6	•038j	99,996	99.996	99,996	-ó•óòo	33733ē:
	1013.4	ē5•8	•0430	116.451	116.451	116.451	#0 <u>*</u> 000	11 <u>6×45</u> 1.
_		LAGE DIEE DO-	1 ////	04 ( ) 5(0205 00 11	CEN A DAGETAGE	(4054) ##*		
		TEACH RALL € GRE	25 = -1 <sup>5</sup> 64000F=(	04 + -1.26930E-02 (A	FILMS + 5-480\0Embj	1955 Link A.A.S. +	O (ACEM)	<b>严重者</b> ( 1 1 m

PAGE: 3

		TES	T. JUMBER 10	-,	TABLE 24 VERSUS DIFF	ERENTIAL		PRESSURE. D.	ATA ACQUIRED .  CONTAMINANT .  CONTAMINANT .	FLOW-RATE-VERSUS-DI AFTER THE ADDITION AND PRIOR TO THE GN /N 027) INLET FRES	OF 7.9 MG 2 IMPACT
			******		T CONDITIONS					NET DIFFERENT	IALI PRESS
******	**********	*****	*****	**********	*******	****	*****	****	*#\$#####	**********	****
PRESSU	RE	1	EMPERATURE	******	******	****	FLOW RATE	***	****		
KGZSQ CM	PSIA	OEG = _K	DEG. C	DEG.E	LITERS/	CEM	SCEM_	<b>κ</b> ₫\મ∺ ⋳⋈5	GN2 La <b>S</b> ZHR	KG/SO CM DIEEERENTIAL	bà'lò —
71.235		293.1	19.9	<u>67.9</u>	83.5	- 9426 <u>-</u>	2.950	<u> 5,6,8</u>	<u>12.804</u>		<u>113•ĕ03.</u>
71.235	101324	292.4		_	76 <u>.</u> u	387	2.685	5.285	11_653	7.0749	100-629
71.235		2921	12.3	66.J	. 67. <u>1</u> .	341	2.370	4.665	10_288	5 <u>.</u> .75 <u>1</u> 6	81.807
71 <u>•23</u> 5		2919	18 <u>.8</u> .	65.8	57_6	293	2.033	4=104	<u>ชัก</u> ธรุ	4.7218	<u> </u>
71.235	101326	291.9	18.7.	65.7	49:1	249	1.733	3,412	7.522	3,8487	<u>54×741</u>
71,235	1013.5	292	18.8	65.9	39 <u>*</u> 0	<u>.</u> 199	1.379	2.715	5,986	5 <u>-8545</u>	40_596:
71.235	1013.4	292,2	19	66,2	29_8	-•0152_	1.053	2.073	4.569	5-3613	33 585
71 <u>*535</u>	1113.4	292.4	19.2	- 66.6	25_0	•u127 _	588	1,736	3.828	1.9310	27.465
71.514	1017.6	292.6	19.4	26.9	<u> </u>	<u>4</u>	.726	1:424	3,151	1.5467	21,985
7 <u>1.514</u>	1 <u>u</u> 1 <u>7.e</u> e	292	19• [	<u>. 6</u> 7.4	13 <u>.</u> 7	<b>e</b> il <b>0</b> 70	484	•954	2.101	<u>*8</u> \$\$	13.976
<u> 71.514</u>	1017.4	293.4	20.2	68.4	13 <u>.</u> 7	• 207a	<u>485</u>	955	<u>2•</u> 10 <u>5</u> .	9806	13-947
71 <u>•</u> 514	1.17.4	293.3	20.2		20 <u>*</u> 7	<u>.</u> 0105	731	1.440	3,175	1.5538	55. ¥00
.7 <u>].514</u>	101744	293.2	2v= <u>1</u> .	60.2	25.6	41130	903	1.779	34921	1.9837	28,215:
7 <u>] •</u> 514	1417.4	293.1	19.9	67.9	30 <u>*</u> 3_	. • 0154	1.070	<u>\$•jo;</u>			36 <u>, 166</u>
7 <u>1.514</u>	1017.4	292.8	19.6	67.3	.39 • 6,	4261	1.398	2.753	6.070	3,4123	48,535
71.514	1017.4	292.2	19a1	. 66.3	49 <u>.</u> 8	247	1_722	3.391	7.475	4.3118	61,329
7 <u>1</u> ±51 <u>4</u>	1017.4	291.8	18.7	<u>\$</u> 5.6,	57 <u>.</u> 8	·1223	2.042	4 <u>2 Ų 2 Ų</u>	B <u>.</u> B63	5 <u>.2228</u>	74,285
71 <u>.</u> 51 <u>4</u>	111744	44	18.2	64.8 .	66 <u>•</u> 9 .	633د و	5•3ē4	<u>4.65</u> 5	10,262		87-663
71.235	101306	7 <u>.</u> nes	17 a 2	63.6	75 <u>∗</u> 3.	•u351 .	2.659 <u></u>	5.236	11:593	_7 <u>•</u> 0304	99.996
71 - 235 ####	1013.c	29(1.3 *####	17-1 ######	62.8 *****	<u>85*1</u>	<u>•</u> 0430	3.005	<u>2•8iï</u>	13:044	6,1873	116 <u>4</u> 51
71:375	1015•\$	292.3	19• i	66.4		<del></del>					······································
.140	2.0	• 6	• 6	1.1	PEVIATIONS						

— <del></del> ยะ			TEST IUMBE	R 10 PART	27F		CONTAMINATED CONDITION FRESSURE. DATA ACQUITOR SYNTHETIC CONTAMIN (10,000 PSIA NOMINAL)	RED AFTER THE AT	DITION OF 7.9 DESCRIPE
	****	****	FLOWMFTER	CONDITIONS	****		(S/X 0277**REET TREE	CIMEN INLET C	ONDITIONS:
	********	FLOWMETER ONE		*****	FLOWMETER TW				
	FI'ON RATE	PRESSUPE	TEMP_	FLOW RATE	PRESSURE	TEVP.	PRESSURE	AVG TEMP	FLOW BATE
	(ACEM)	(PSIA)	(DEG: F)	(ACĘM)	(PSIA)	(DEG. F)	(PSIA)	(DEG+ E)	(ACFM)
	<u>•</u> 85	49.9	63.6	•90	47.6	68.8	1011.9	66+2	.042Î
	<u>.</u> 76	50.2	62.9	.81	48.3	68.1	1011.9	65,5	,0381
	,66	50.2	62.5	.70	48.7	67,9	1011.9	65.2	.0333:
	. •57	50.8	68.5	.59	49.5	67,8	1007.9	65,1	.ŋż89º
<u>"H</u>	.49	50.2	62.8	.50	49.3	67.9	1007,9	65.4	. 02 <b>45</b> 1
	.40	50.6	63.4	•40	49.9	68,2	1007.9	65 <u>°</u> 8	•02000
_	•30	<del>50.2</del>	63.4	.30	49.7	68,3	1007.9	65, 8	.0149
	•56	50.2	64:1	• 25	49.7	69.7	1:07.9	66 - 9	•0127.
_	.21	50.2	65.4	•20	49.9	70.0	1007.9	67.7	•0103°
	:14	49.9	66•4	•13	49.5	69.7	. 1107.9	68.1	• 0066
	.14	49.9	66+8	.13	49.5	71.9	1011.9	69.44	.0056
 J3	<u>.</u> 21	49.9	66+6	•20	49•5	72.3	1411.9	69 • 4-	•0100
	.26	50.1	66.3	.26	49.5	71.6	1011.9	69.0	•0159'
_	•30	50.1	64.8	•30	49.7	70.2	1707.9	68.5:	.0149
 88	40	49.7	66•6	•41	48,9	7a•1	1007.9	68.4	,0197
	.49	49.9	65.6	•50	48,9	69.6	1007.9	, 67,6	.0242
	•57	50.1	64:3	•60	48.9	59•5	1007.9	66.9	+0287
_	<u>.67</u>	49.9	63•1	•71	48.3	69.4	1007.9	66.2	+0337
	<u>.</u> 75	49.9	67.3	.81	47,9	69,6	1907.9	66.0	.0379
-	.84	50.1	62•3	.91	47.B	68,6	1407.9	65,4	•0485°
 2:U								<u> </u>	· · · · · · · · · · · · · · · · · · ·
_									
		······································					<u> </u>		<del></del>

		7A	ELOM RATE TABLE 25	ieecrential_eress	URE	PAGE: 2 DATE: 9-14-76	1
<del> </del>	~ . т	-ST U .HE' 10	₽\AT 27F	TEST DESCRI		CONDITION - FLOW RATE TA ACQUIRED AFTER THE	
					OF SYNTHETIC	CONTAMINANT AND AFTER	10 HIGH PRESSURE
***********	TWEN INTEL COM	**************************************		,		N <u>ominal) Gn2 impaci</u> Et pressure = 1000 ps	
****		x 4 44	rR SS	38 5S		AADDINGTON ON	
PŘESSUŔĘ	TEMP	FLO" RITE	DIFF.PRFSS . PRIMARY	DIFF PRESS SECOND, RY	Ditt. butes	DIFF. PRESS	DIFF. PRESS
(PṢĨĄ)	(DEG. F)	(_cFa)	(LISq)	(55tr)		(PSIO)	(PSID)
- 1011-9	56.2	421-	292,659	3984659	292.659		292+659
1011,9	95•≴	381	24 <b>7.</b> 464	247,464	247.464	000,000	247.464
1011.9	55.2	EEE	197.529	197.529 .	_ 197.529	=0.000	197.529
_ 1007.9 _	65.1	289	155.,12?	156,127	156.12%		<u>1</u> 56,127
	r5.4		125,414	12., 41/	120,414	0-000	120,414
1007.9	€5.8	4154	. 25.071	88.17.7	87•42 <u>4</u>	= = D + O O O	87.424
1007.9	65 <b>.</b> 8	149	56,617.	57,52	57 <b>.</b> n69	-0.000	57.069
1007.9	26.9	.127	44.5.8	45.195	44.851	-0.000	44.851
1007.49,	67.7		32,6.8	33.335	32.971		32: 972.
1007.9	58.1	nu56	1858	. 18.112	18_085.		184085
1011.9	69.4.		17.942	18,112 .	1827		18.027
	. 69.4.		31 981		32.341		32.342
101149	99. <sub>.</sub> .		46.26	4791	46.675		46.676
1007-9	•	-	<u> 56_493</u>		56.849		56.840
1007•9		·	85.74	-	-	•	86,643
4			120_414		•	• • • •	120.414:
			156,759		<del>.</del>		156,759
1007-9		. 1337	•	•	202.270	Ť	202•270
1007.9		379	Ÿ	•	246.832		2464832
1007.9				-	•	,	•
						•	
(*							

PAGE: 3 TABLE 25
-ELOW RAIF VERSUS DIFFERENTIAL PRESSURE. ` DATE: 9-14-TEST DESCRIPTION PRESSURE. DATA ACQUIRED AFTER THE ADDITION OF 7.9 MG TIST UIRER 1" P. 9T 27F OF SYNTHETIC CONTAMINANT AND AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GW IMPACT CYCLES. TEST SPECIMEN (S/N 027) INLET FRESSURE = NET DIFFERENTIAL PRESS TEST SPECIMEN INLET COMDITIONS 1000 PSIA (NOMINAL) PRESSURE TERMERATURE FLOY RATE \*\*\*\*\*\* 我的我还在我的心理的人,我们可以我们的,我们就是我们的一个人,我们就是我们的,我们就是我们的人,我们就是我们的,我们就是我们的,我们就会会会会会会会会会会会会会。 \_\_KG/SD\_CM\_\_\_ DIFFERENTIAL ĸĠ∕ĦŖ LITERS/ GN2. LRS/HR KG/SQ CM PSIA EG. C DEG. F CEM SCFM PSID DEG. K MÍN 71.144 66.2 5.750 12.677 20,5760 292,659 1011.9 292.1 19.0 2.7 . 1421 2.920 71.144 1011.9 291.8 65.5 2,645 5.208 11.482 17,3985 247,464 . 381 13.6 74.9 197.529 71.144 4.551 10.432 13.8877 1::11.9 391.6 65.2 **65.4** . 333 2.311 18.5 19.4 70.865 8,690 1907.9 3,942 10,9768 65.1 . ,289 156,127 291.5 36.7 2,002 120.414. 1447 70.865 3.334 1 107.9 1.691 8,4659 291.7 (0,5 65.4 . 245 7.342 +7.9 5.987 70.865 1007.9 291.9 18.8 1,379 2.716 6.1465 87.424 65 R 39.1 n2ec 70.865 1007.9 18 8 65 A 1.031 4.478 57,069 292.1 29.2 . 1149 2.031 4.0124 70.865 1007.9 292.5 9.4 66.9 24.7 .. 127 .873 1.720 3.791 3.1534 44.851 70.865 1407.9 293.r 1 .395 32-972 19.8 67.7 20.1 .0103 .708 3.975 2.3181 70.865 1007.9 293.2 .454 .893 1.969 12.8 . p66 1,2715 18, 085 20. 68.1 2 .3 71.144 69.4 Ĩ#11.9 293.9 . 066 .452 891 1.964 1.2674 18.027 12.8 71,144 294.4 1,363 1011.9 21.8 69.4 692 3.004 2,2738 32,342 19.6 .31 -71.144 69. 1.757 1011.9 293.7 • 129 .892 3.874 3.2816 46.676 2 ,5 ?4.3 70.865 293.5 ...140 3.9969 56. B49 1007.9 68.5 28.9 2. 11 4,434 2 .3 1.021 70.865 1307.9 293.4 . 197 2.668 5.883 6.0916 86,643 68.4 39.4 1.355 2. .. inhee 1007.9 3,285 70.865 292.9 47.2 242 19 B 67.6 1,669 7.243 8,4659 120.414 70.865 1007.9 . 287 1.978 3.894 8.585 156.759 292.6 19.4 66.9 6.5 11.0213 . 337 70.865 1007.9 292.2 19. 66.2 65.8 2.324 4.576 10.089 14,2210 202,270 74.1 5,152 11.358 70.865 1907.5 292.4 18 9 66. . 379 2,617 17,3540 246.832 1007+9 70.865 291.7 14.6 65.4 2.942 5.793 21.3759 304-037 33.3 ..425 12.771 \*\*\*\* \*\*\*\* 好好好好处 ... \*\*\* \*\*\* 3333 70.949 1009.1 292,6 ..... 19.4 66 9..

\_DEVIATIONS

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. . . . . . . PAGE: 1 DATE:--9-14-76 TABLE 26. ---CONTAMINATED-CONDITION-- FLOW-RATE-VERSUS-DIFFERENTIAL FLOW RATE VERSUS DIFFERENTIAL PRESSURE PRESSURE. DATA ACQUIRED AFTER THE ADDITION OF 7.9 MG OF SYNTHETIC CONTAMINANT AND AFTER 10 HIGH PRESSURE (10,000 FSIA NOMINAL) GN2 IMPACT CYCLES. TEST SPECIMEN
RART 27G ... JEST DESCRIPTION(S/N 027) INLET TRESSURE - 415-PSIA (NOMINAL). .ន្ធន្ធ រ ១ស FLOWMETER CONDITIONS TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\* FLOWMETER ONE \_\_ELOEMETER\_TWO\_\_\_\_ \*\*\*\*\* \*\*\*\*\*\* AVG. TEMP FLOW RATE PRESSURE FLOW RATE PRESSURE TEMP FLOW RATE PRESSURE TEMP (PSIA) (ACEM) (DEG. E) (ACEM) (ESIA) (DEG. E) (DEG. F) ១០ .\_\_75.5.\_\_ 40367 8333 75.9 50.1 76.6 75.7 49.3 76.6 .025D 75.8 49.3 76.8 412.5 76.3 .0305! 49.9 412.5\_ .0373 49.9 .75+8\_\_\_\_\_\_.76+9\_\_\_\_\_\_\_ 411.8.... 75.9 49.2 77. 411.8 76.4

					<u></u>		— DATE:—9-14-76		
				FLOW RATE VERSUS D		JRE PRESSURE, DATA	NDITION - FLOW RATE V ACQUIRED AFTER THE A NTAMINANT AND AFTER 1	DDITION OF 7.9 MG	
			TEST YUMBER 10	PART 276	TEST_DESCRIP	(10,000 PSIA NO	MINAL) GN <sub>2</sub> IMPACT CY T <del>PRESSURE = 41</del> 5-PSIA	CLES. TEST SPECIMEN	า 
<del></del>	TEST SP	ĘCĮMEN INLET	CONDITIONS						
	******	*****	********						
	PRESSURE	AVG TEMP	AVG ELOW BATE	GROSS DIFF: PRESS PRIMARY	DIFF. PRESS SECONDARY	AVG GROSS DIEF. PRESS	TARE DIFF. PRESS	NET DIFF. PRESS	
	(PSIA)	(DÊĞ, F)	(ACEM)	(PSID)	(PSID)	(P\$IQ)	(PSID)	(PSID)	
	413.8	74,5	+1449	393,931	303,931	303•33Í	•000	303,931	
	413.1	74.6	, 1428	259,685	259,685	259.685	•000	259.664	ពុ
•	413,1	75.0	•n367	180.357	180.357	180.357	•000	180.357	
	413.1	75 <u>.</u> c	.,315	133.898	868.551	133.898	•000	Ï33.898	
	413.1	75.2	. 1254	91,487	93.128	92.308	•000	92.308	Я
	413 <u>.</u> 1	75.9	-0157	49.137	49.830	49.483	.000	49.483.	
	413.1	76,3	, 1167	48,512	49,198	48.855	.000	48, 855;	
	413 <u>.</u> 1	76,2	•0250	89.294	90.916	90.060	•000	90.060	
	412.5	76.3	.0305	128.841	128,841	128.041	•000	128 <b>.</b> 841	_
	412.5	76,3	.0373	190.154	190.154	190.154	•000	190.154·	
	411.8	76,3	•n425	257,788	257.788	257.788	•000	257,788	
	411.8	76.4	•: 441	291,921	291,921	291.921	•000	291.921	
					4 4				<u> </u>
		IARE DIFF. 1	PRESS = -3.40000E-	05 + -4.44000E-04 (	ACFM) + 1.50933E-	01 (ACFM) ##2 +	0 (ACFM)	*43	
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	· w to the same constitution cons	*************************			,				
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· <u>-</u>		<del></del>							PAGE: DATE:		
				FLOW RAT	TABLE 26 VERSUS DIFF	ERENTIAL	PRESSURE	PRESSURE. DAT	A ACQUIRED AF	OW-RATE-VERSUS DIFF TER THE ADDITION OF D-AFTER 10-HICH-PRE	7.9 MG
<u></u>	-	TF	ST_UMBER_10	PART	276	TEST_0	ESCR <del>IPȚI</del> O		OMINAL) GN2	IMPACT CYCLES. TES	
****	**********				T CONDITIONS		*********	*************	ANAMELEE.	NET DIFFERENT	I <sub>A</sub> LI PRESS
- PRESSU	RE	·	IEMPERATURE ####################################		******	·	_FLOW_RAT				<u>'</u>
KG/SQ_CM	PSIA	DEG. K	neg. c	DEG+_F	LITERS/		ScFM_	GNS RĞ\HB	GN2	KG/SQ CM DIFFERENTIAL	PŠĮ
_55°035	413.5	296.8	<u>23.</u> 6 .		4 .	449	<u>_1.252_</u>	2.465	5,434	21.3685	3 <sub>0</sub> 3; <u>931</u>
29.046	413.1	296.8	23.7	74.6	33.8	428	194	2.351	5,182	18.2576	259,684
	413,4	297	23.9	75.0	28.9.	0367	1.022_	21013	4.437	12±6803	180 <u>-357</u>
29 0 46	413.1	297	23.9	75.p	24.8	315	.877	1 . 7 2 6	3.805		133-888
2 <u>9.046</u>	413.1	29.7 • 1	24	75.2	20.0	254		1.393	3.071	6,4899	<u> </u>
<u> </u>	41341	297.ń	24.4	75.9	1342	167	.465	<u>-915</u>	2,018	3.4790	<u> </u>
29.046	41 -	297.8	24.6	<u>76,3</u>	ـ ـ. 13ـــــــــــــــــــــــــــــ	6167	463	<u>-913</u>	2,012	3,4348	48,855
29.046	413,1	29 <b>.</b> 7	24.5	7.6.2	19 . 7	. <u>•</u> 1256	695	1.369	3,019		- 30 ÷ 600
29 ooi	412.5	297.8	24.6	76.1.	23.2	0305	845	1,663	3_667	9.0584	128_841
5à°00j	412,5	297.8	24.0	7á.3	29.3	_ <b>.</b> 0373	1.035	2.039	4.494	13.3692	190.15 <u>4</u>
28.955	411.8	8	24.6	76.3	33 <sub>9</sub> 3	•J425 .	1.17.7	2:317	5-109	18.1243	25 <b>7.78</b> 8
28 <u>.955</u>	411.8	297.8	24.7	76.4	34,6	441	1.222	2,406	5,305	20.5241	<u> 291.921</u>
29.028	412,9	297.4	24.3	75,7			·•	<del></del>	<del></del>		
•033	•5	•4	•4	•7	DEVIATIONS						**
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		_,	FLOW RATE	TABLE 27	ERENTIAL PRESSURE	CONTAMINATED CONDI		
		TSTUMBE	R 13 PART.	27.1.	TEST DESCRIPTION	DIFFERENTIAL PRESSI THE ADDITION OF 15 AND AFTER 20 HIGH GN2 IMPACT CYCLES.	.8 MG OF SYNTHE PRESSURE (10.00	TIC CONTAMINANT O PSIA NOMINAL)
		FLOW/ETER	CONDITIONS		90448449944	INLET PRESSURE = 10 TEST SPEC	000 PSIA (NOMIN IMEN INLET C	ML). Onoitions:
,	FLOWM=IER-ONE			ELOWMEIER TU				
LOW RATE	PRESSURE	Temp	FLOW RATE	PRESSURE	TEMP	PRESSURE	AVG TEMP	FLOW RATE
	(Pala) 	(DEG: F)	(:GF,H)	•	(DEGF)		(126. F) 73.1	(ACEH) .0097:
-	<u>5u,4</u>	_ 72.n	.18	_ 5n_2.	74-1	1315.9	73.0	.0088
<u></u>		7.2	15	54+2	74•3	1.15-9	73-1	• 007A:
<u>.</u> 1.		7241		50.1.		1.15.9	<u>73,3</u>	_006B!
12	<u> 50.2</u>	72-4	•11	49.9		1:15.9	73.5	•00 <u>\$7</u> *
12	<u> </u>	72,5	.11	50.2	73.5	1515.9	<b>73.</b> 0	.0058
<u></u> 14	<u>49•7</u>	72	.13	49.5	73.5	1:15.9	8.SŤ	.0067
16		72	15	49.9	75.1	1:15,9	73.5	, 007Å:
18	<u>49.7</u> -	71 <u>.</u> 8		49+3	74+8	1 15.9	73.3	
19	bk.1	71.18			73.3	1:11.9	72.5	.0094:
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				Minimum with the MINIMUM or of		PAGE: 2 DATE: 9-14-76	,	-
			FLOW RATE VERSUS DI	IFFERENTIAL PRESS	URE CONTAMINAT	TED CONDITION - FLOW F	RATE VERSUS	_
	IF	SST JUMBER 10	PART 271	TEST_DESCRI!	THE ADDITI PTION AND AFTER GN2 IMPACT	TION OF 15.8 MG OF SYNT 20 HIGH PRESSURE (10, TOYCLES. TEST SPECIA	NTHETIC CONTAMINANT 0,000 PSIA NOMINAL) IMEN (S/N 027)	<u> </u> 
TEST SE	PECIMEN INLET COND	)ITIONS	n. v. y 6 Arresse w. e. e.	r 4 r 4 w 20 4	INLET PRES	SSURE = 1000 PSIA (NO	MINAL).	
			cRoss	GRASS.	anage			
RESSURE	AVG L. JEMP	AVG LELOW_RATE	DIFF. PRESS	DIFF. PRESS SECONDARY	AVG GRUSS	TARE OIFE_ PRESS	NET DIEF PRESS	<u>i</u>
(PŠĮĄĮ	(UEG, F)	(ACFM)	(pSI <sub>ii</sub> )	(PSID)	(PSIO)	(PSID)	(PSID)	
1015.9	73.1	.0097	3)2,772	3,2,772	302.772	-0.000	302.772	
1015.9	73.0	.0098	26.) 422	261,422	260.422	-0.000	260.422	· 1
1015.9	73.1	.0078	214,595	214,595	214,595	-0,000	214,596	i
1015.9	73.3	\$400.	173,825	173,825	173,825	-0.000	173,826	
1015.9	73.5	.0057	134,004	134.004	134,004	<b>⊷0.00</b> 0	134,004	[ ]
1015,9 -	73,0	, <sub>0</sub> ,58	134,636	134,636	134,636	-0,000	134,636	
1015.9	72.8	•01 67	168,769	168.769	168.769	-0.000	168-769	_
1015.9	73.5	.0078	210.171	210.171	210.171	-0.000	210.171	-
1015.9	13.3	,0038	259,474	259,474	259.474	-0.000	259,474	· <u>-</u> -
1011.9	72.5	,0,1,94	290,445	290,446	290,446	⇒0.000	290,447	
					LANGER Williams up on oil book of William or history			  195
	(ARE OIFF. PRES	(S = -1.64000E-0	4 + -1.25936E-62 (A	ACEM) + 2.48070E	-01 (ACF4)*#2 +	G (ACFH)	**3	
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				\				PAGE	: 3 : 9-14-76	
		,		TABLE 27			CONTANTA		ON - FLOW RATE VERS	IIS
<del></del>			FLOW RATE	VERSUS DIF	LEKENITYL I		DIFFEREN	TIAL PRESSURE		FTER ,,
		TEST : UMBER 11	PART_2	27.1	IEST_D	SCRIPTION	AND AFTE	R 20 HIGH PRI	SSURE (10,000 PSIA	NOMINAL)
					<u>-</u>	51Fuggggggggad 1.7			TEST SPECIMEN (S/N D PSTA (NOMINAL).	
	***	<del>*************************************</del>	PECIMEN INLE	ERREGERATERS CR	(5) 克奇斯森斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯斯	R#####################################	法主义教育法律专业社会	****	NET DIFFERENT	INT AKEDO
, - PRESSURE		TELLER_TURE_			-,	FLOW-RITE-				
**************************************	***	·		****	************					
Kā'so čw — ESI7 —	DEGK.	EG. C	DEGE	Liters/ minl.	GEM	SCEM	— <mark>кё^нё</mark> еи5	<u>r⊌ģ^нв</u> GNS	KG/SA CM <u>Differential</u>	psip
71.4231015.9	296	22.8	73.1	. 18.9.	. 1097	666	1 <u>=31</u> i	2.891	21.2870	302.772
71,423 1015.7	296.2	. 22.8	73	17.2.	3088	607	1 <u>.194</u>	2.633	18,3095	260.422
71.423	296	22.9	73+1	15.1.	078	535	1 <u>+</u> c5 <u>3</u>	2.321	15.0876	214.596.
71.423 1015.9	295.1	22.5	73.3 _	. 13,3	n6d	469	<u>. 92</u> 3	2 <u>34</u>	12.2212	173.826
<u>71.423</u> 1u15.9	296.2	23,	73.5	11.2	57	394	<u>.775</u>	1,709_	9,4214	134_084
71.423 1015.7	295.9	22.8	73	11,2		.396	780	1,720	9,4658	134.636
	295 ಕ್ಕ	22.0	72.3		i057	463		2-008	11.8656	160.769
71,423 1015,9	. 296.2	23.1	73.5	15.1		533	1 <u>_050</u>	2.314	14.7765	2184171
71 <u>.423</u> 1015.9	. 296.1	22.9	73.3	17 <u>.</u> u _	ep88.	602	1.185	2.611	18.2428	259.474
71.144 1011.7	295.7 #####	22.5 *****	72 <u>,5</u>	18.3	•.109.4	647	1.275	2.810	20,4204	290 <u>*\$\$</u> Z_i
71,395 1,15.5	296 • (	22.8	73.1					, <del></del>	and the Address water promoter	· ' '
.050	• l	• 1	•5	DEVITATION	s					
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							V.	<u> </u>		

### TABLE 28 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 11 PART 22A

TEST DESCRIPTION

PAGE: 1 DATE: 9-10-76

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 16.3 MG
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 1000
PSIA (NOMINAL).

r,	****	***		CONDITIONS	*****	***	TEST SPE	CINEN INLET C	CONDITIONS		
ľ	****	FLOWMETER ONE		你你你你你你你你你	FLOWMETER TWO	***	,				
	FLOW RATE	PRESSURE (Psia)	TFMP (DEG F)	FLOW RATE (ACEM)	PRESSURC (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA).	TEMP (DEG • F)	AVG FLOW RATE (ACFM)		
	.87	50.2	82•4	•91	48 • n	86+5	1013•2	84•4	0433		
	7 <u>B</u>	56.2	81 <b>÷</b> 2	• {	48•4	85•8	1913-2	83,5	0388		
	•70	àù•S	80 <u>•</u> 5	.71	48.6	85.2	1009.2	82 <b>•</b> 8	.0344		
	•59	50 <u>.4</u>	8r <b>±2</b>	•60	49.2	84.9	1)09+2	82.5	•0295		
•	<u>.</u> 50	<b>ວິບ</b> • 1	80.2	•50	49 • n	n4+9	1:09.2	82.5	.0245		
	• 41	ำ ≥กํ+รั	80-3	• 4 1	49.5	84.9	1009.2	82.6	,0201		
	•31	à₫*5	80.7	.31	49,5	95.0	1009.2	65∙8			
	•26	5 v . 2	8n•9	•26	49.7	85+1	1)09.2	83.0	•012 <u>9</u> ′ _		
	•51	>្.6	81:2	-21	5()•3	85.2	1009+2	83.2	.0165		
	•14	<b>90∙1</b>	81 •9	•14	49.5	85.6	1009+2	83•7	0069		
	<u>. 14</u>	ğ. u و	82.5	•14	50 • 1	<b>ដ</b> ទឹ+មិ	1009+2	84•1	•0 <u>07</u> 0		
	•\$1	49.7	82.3	•21	49 • 2	85.7	1009+2	84.0	<u>•0104·</u>		
	•26	42.7	82 <u>±</u> 4	• 26	49.2	85 <b>.6</b>	1:09-2	<b>83</b> ∓8	.0129		
	<u>.</u> 31	<b>50.1</b>	81 <u>+</u> 6	•31	49.3	85.4	1309+2	83,5	• 015 <u>2</u> .		
,	<u>.</u> 40	49.9	80.7	• 40	49 <u>•</u> 2	84.9	1)05•3	82.8	•0197		
	<u>.</u> 50	49.9	79•8	•50	49.0	34.4	1905.3	. 82•1	0246		
	• 59	50.4	78 <u>±</u> 8	<u>•</u> 61	49+2	83.7	1:05+3	81 - 5	.0296		
	• 68	50.1	78±1	•71	48•4	83 <b>•</b> u	1005+3	.80.5.	•0340		
	• 76	49.9	77•2	•80	48.0	82.3	1001.3	79.7	.0381		
	.85	<b>50,2</b>	76•4	.92	48.0	81.4	1901.3	78,9	.0433		

PAGE: 2 DATE: 9-10-76

TABLE 28 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

11

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 16.3 MG OF SYNTHETIC CONTAMINANT ADDED. TEST TEST NUMBER 11 PART 22A TEST DESCRIPTION SPECIMEN (S/N 022) INLET PRESSURE = 1000 PSIA (NOMINAL).

TEST SPECIMEN INLET CONSITIONS \*\*\*\*\*\*\* GROSS DIFF. PRESS GR ISS DIFF. PRESS AVG GROSS AVG ΑVG TARE NET DIFF. PRESS PRESSURE I EMP FLOW RATE PRIMARY SECONDARY (PSID) OIFF. PRESS (PSID) DIFF. PRESS (PSIA) (DEG F) (PSID) 133,205 1013.2 84.4 133,205 133.205 .0433 133.205 -0.000 115.213 115,213 115.213 1013.4 83.5 .n388 115,213 -0.000 1009.2 82.8 .n344 99.43. 99,430 99.430 -0.000 99,430 82.429 1009.2 62<u>.</u>5 .r295 82.157 82.7 1 82.429 -0.000 65.607 1009.2 82.5 65,971 65.607 .0245 65.243 -0.000 1009.4 52,398 52.001 52.001 82.6 .0201 51.604 -0.000 37,983 1009-4 82.8 .0151 37,884 38,981 37.982 -0-000 31.409 1009.2 **83•€** .0129 31.345 31.472 31.408 -0.000 1009.2 83.2 24,632 24,7 15 24.668 24.669 .0135 -0.000 15.378 1009.4 83.7 .0069 15.374 15,381 15.377 -0.00ŏ 1009.4 15,667 15.636 15.636 84.1 .0075 15.675 -0.000 1009.2 84.0 .0104 24.401 24,533 24.467 -0.00ŏ 24.467 1009.2 8.88 .0129 31,644 31.552 -0.000 31.553 31.461 -0.000 1009.2 83.5 38.058 38,253 38,155 38, 156 .0152 ~0.000 1005.3 .0197 50.728 51,451 51.089 51.090 8.58 1005.3 66.918 66.581 82.1 66.243 -0.000 66.581 .0246 83.896 1005.3 81.2 .1246 83,513 84.279 83.896 -0.000 1005.3 100.062 80.5 .0340 100.062 100.062 100.062 -0.000 ال. 1001 79.7 .0381 115,528 115.528 115.528 115.529 -0.000 1001.3 78.9 .04J3 137,308 137,308 137.305 -0.000 137.309

IARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM) \*\*2 +

0 (ACFM) \*\*3

PAGE: 3 DATE 9-10-76

## TABLE 28 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST LUMBER 11 PART 22A TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 16.3 MG
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 1000
PSIA (NCMINAL).

1	***	***	****			ET COMDITION:		***	***	****	NET DIFFERENT	
'	PRESSI		*****	TEMPERATURE			***	FLOW RATE	***	***		
	Kē/so cm	PS1 <sub>A</sub>	DEG₊ K	NEG. C	DEG∙ F	LIT#45/ MIN	4 ÇFM	SCEM	KG/HH GNS	₽₽\$\HB €N5	KG/SQ CM DIFFERENTIAL	PSID
	71,235	1013:2	302.3	29.1	84.4	85.2	. 433	2.904	5.718	12,605	9.3653	133.205
	71.235	1013.4	301.8	28.6	83.5	73•9	.0388	2.605	5,130	11:310	8.1003	115.213
i	70 • 956	1009.4	301.4	28.2	82.8	65.3	. 1344	2,308	4-544	10,018	6.9907	99.430
•	70.956	1009,4	301.2	28.1	82.5	56 <sub>•</sub> 1	• 29b	1.979	3 • 89 à	8,593	5.7954	82.429
	70.956	1009يٰذِ	301.2	28.1	82.5	46.5	. 245	1.642	3•53\$	7 <u>.</u> 126	4.6127	65,607
	70.956	1009•4	301.3	28.1	82.6	38.1	.9201	1.345	2.044	5 <u>.</u> 838	3.6560	52,001
	70,956	1009.4	301.4	28.2	8.58	28.7	.3151	1.915	1.999	4.408	2. <u>6</u> 704	37,983
	70.956	1009,4	361.5	28.4	<b>43.</b> 0	24•4	129	.862	1.695	3,744	S•Š0āS	31,409
,	70.956	2،90	301.6	28.5	83.2	50.0	•01uS	.706	1*38Ă	3 <u>.</u> 063	1.7344	24,669
	70.956	1009 <u>•</u> 4	301.9	28.7	83.7	13•2	•1069	.464	<u>•</u> 915	2:016	1.0812	15.378
	70.956	1009:4	302.1	29.0	84.1	13.3	.0070	.469	•454	2,038	1.0993	15,636
	70.956	1009:4	302.1	28.9	94 • v	19•7	•0104	• 6 6 6	1-370	3.019	1.7202	24.467
	70.956	1009.4	301.9	28.8	83.8	24.5	•0129	.865	1.704	3 <u>•</u> 756	2,2184	31.553
	70•956	1009.2	301.8	28.6	83.5	28.8	.0152	1.016	s•00ô	4.409	\$•ē8 <u>\$</u> 6	38,156
4,	70.677	1005-4	301.4	28• <u>5</u>	82.8	37 <u>.</u> 2	• 3197	1.315	2,588	5.706	3.5920	51.090
	70.677	1005-4	301.0	27.8	82.1	46.6	• )246	1.645	3 <u>.</u> 240	7 <u>.</u> 142	4.6811	66,581
	70 • 677	1005,4	300.5	27.3	81.2	56•2	• 1296	1.985	3,908	8.615	5 • 8 9 8 5	83.896
	70.677	1005.2	300.1	27.6	80.5	64.5	• ø34g	2.278	4.485	9.889	7:0350 <u> </u>	100.062
	70.398	1001,3	299.7	26.5	79.7	72.2	•u3H1	2,550	5 02 L	11:069	8.1225	115,529
	70.398	1001.3	299.2	26•1	78.9 *****	85∙0	• 0433	2.897	5 <u>•</u> 7₀5	124577	9.6538	137-309
	70.872	1008 ខ្មែ	301.3	28.1	គី5 • 6			•			·	
	•17 <u>3</u>	2.5	•6	• 6	1.1	DEVIATIONS	5					

TABLE 29
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PART 228

TEST Um3En 11

TEST DESCRIPTION

	***	FLOWMELER ONE	***	***	FLOYMETER TWO	*******
	FLOW RATE	PRESSURE	TEMP (DEG. F)	FLOW R TE	PRESSURE (PSIA)	TEMP (DEG <sub>•</sub> F)
	• 5₿	49.9	72:9	• <b>6</b> tr	48.8	74.3
	• 49	50.2	72 <u>:</u> 8	•51	49•3	74.3
	<u>•</u> <u>4</u> 0	50.4	72 <u>.</u> 8	#4d	49 • 9	74.5
	•31	÷(•6	73+1	•30	50 • 1	74.6
	<u>• 26</u>	49.7	73:1	• 25	49 • 3	74+7
	•šī	គំ <b>ព</b> ិន	73 <u>.</u> 1	•2u	49.9	74.8
	<u>. 14</u>	50,4	73.5	<b>.</b> 13	50.3	75 <b>.</b> 0
	<u>•</u> 14	42.9	73•8	413	49.7	75.4
	• S2	49.9	73.7	•24	49.5	75.4
	<u>•</u> 27	49.7	73+0	∎2ô	49.3	75.4
14	•35	•0•2	73.5	•31	49.7	75•3
	<u>.</u> 41	\$0 <b>∗1</b>	73 <u>*</u> 3	" •41	49.3	75•2
	<u>*</u> 20	⊅υ•1	73 <u>•</u> 1	51 .	49 • 2	74.8
le	•57	<b>ວ</b> ທູ6	73 <u>*</u> 1	•59	49.5	74• €
	<u>•</u> 57	∌ព • 6	73:3 .	. 59	49.5	73.6

PAGE: ]	<u>                                   </u>	
DATE: 9	9-10-76	
		-
CONTAMINATED CONDITION -	FLOW RATE VERSUS	
DIFFERENTIAL PRESSURE.	TOTAL OF 16.3 MG	ны
OF SYNTHETIC CONTAMINANT		9 I
SPECIMEN S/N 022) INLE	T PRESSURE = 415	
PSIA (NOMINAL).		
		_
TESŤ ŠPECÍMEN	INLET CONDITIONS	
	****	

417•7 417•3	73.6	
417.0		
	73.6	_
416.4	73.7	
416.4	73.8	<b></b> .
415.7	73,90304-	
415.7	74.0.,0250	
415,7	74.30164	
415.7	74.6	
415.1	74.50265	
415.1	74.5	
415.1	74.40378	
413.8 .	. 74.2	
413.1	73.9	
412.5	73.60703	
412.5	73.6 .0703	

Þ

#### TABLE 29 FLU + PATE VL. SUS DIFFEHEILTIAL PRESSURE

DATE: 9-10-76

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF -16.3-MG-OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE --415-PSIA (NOMINAL). TEST DESCRIPTION P.RT 228

TEST	SPECIMEN	INLET C	ONNTT.	, N 5 1444444444444
****	*****	***	***	<b>ት ፋ ቅ ፋ ፉ ፉ ፉ ፉ ፋ ፋ ቀ ቀ</b>

TEST UBER 11

PRESSURE (PŠĨÁ)	AVG Temp (Deg. f)	VG FLOW RATE ( CFM)	AR.SS DIFF• 2PESS PRIM.YY (PSIU)	JR SS DIFF• PRESS SECONDARY (PS[i])	AVG GRUSS DIFF. PRESS (PSIL)	TARE DIFF. PRESS (PSIO)	NET . DIFF PRESS (PSID)	. !
417.1	73.6	.07.2	343,240	3,3,246	303.246	•001	303,246	- 4
417.0	73.6	. 1397	211.9.9	211,7 9	211,957	.000	211,908	
416 <u>.</u> 4	/3 <u>•</u> 7	485	15 ,912	15 .912	150.914	.000	150,911	- 1
416.4	/3.8	. 368	1. 2.557	1 2.537	1,2.557	•000	102.556	<u>;</u> n.
415.r	13.9	4، وب.	79,661	B. •118	79.889	•090	79.888	i
415.	[4.u	.025c	61,445	61.7 7	41,616	.000	61,615	1
415.	74:3	• 164	37.8 6	37,898	37.654	-0.000	37.851	 
415 <u>.</u> 7	74.6	·· 161	37,111	37,322	37.215	-0.000	37,215	;
415 <u>.</u> ţ	74.5	,4265	67,178	67,476	67.277	•000	67,276	-
415.1	74.5	. 2317	<b>33.98</b> c	44.542	84.264	•000	84.263	!
415.1	14.4	378	1.6,660	110.466	196.666	•000	106.665	j 14
413.5	14.2	. 488	152,492	,52,432	152,492	•000	152,492	
413.1	73.9	.06 2	215,345	215 <b>.</b> 345	215.385	•000	215.385	
412.5	73.6	.07 3	307,039	307.,39	307.039	.001	307.038	<u> </u>
412.5	73.6	.07 3	-0_0v1	ſ	-0.00u	.001	-0,001	"
- <del>-</del> ·	•	_						i

TARE DIFF. PRESS = -3.4.000E-05 + -4.44000E-04 (ACF.) + 1.5.933E-01 (ACF.) +42 +

PAGE: 3 DATE: 9-10-76

# TABLE 29 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION TEST JULIER 11 PART 22B

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 16.3 MG
OF SYNTHETIC CONTAMINANT ADEED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 415
PSIA (NOMINAL).

		****	***	FLON RATE.	****	****	***	TEM: ERATURE	****	****	PRESSU
PŞĬQ	KG/SQ CM DIFFERENTIAL	GN2 LBŞ/HR	ĸĕ∖Hば ਫ਼⋈Ş	SCFH	ACFM	LITERS/ MIN	DEG. F	εEG. α	DEG• K	PSIA	KG/SQ CM
3 <sub>0</sub> 3,246_	21.3203	. 8 <u>.</u> 695	3 <u>.</u> 903	1.982	•9732	56.1	73.6	23.1	296.3	417.1	29.365
211.208	14.0986	7:301	3:314	1.682	• J597	47•6	73.6	23•1	296+2	417±4	58•350
150,211	. 10,6101	5,920	2.685	1,364	.0485	38,6	73.7	23,1	296,3	416.4	29,274
. <u>102,</u> 55 <u>6:</u>	7.2104	4.487	2.037	1.034	. ყვნი	29.3	73,8	23.2	296.4	416.4	29.274
79,888	5_6167	3 <u>•</u> 710	1.083	.855	.03,4	24.2	73.9	23.3	296.4	415.	29.229
61,615	4.3320	3043.	1.380	.701	•925j	19.8	_74 <sub>*U</sub>	23.3	296.5	415.	55.55
37,851	2,6612	2,400	<u>.</u> 90?	.461	•v154	13:0	74.3	23.5	296.6	415: /	29.529
_37,215	2.6165	1.963	<u>•</u> 89v	.452	.4161	12.8	74.6	23.7.	296.8	415.	29.229
67,276	4,7300	3,227	1.464	.743	• J265	1.15	74,5	23.6	296.8	415.1	29.183
84:263	5.9243	3,853	1 = 745	.868	. 3317	25,1	74.5	23.6	296.8	415.1	Sà•183
106,665	7.4993	4,597	5 • 185	1.659	. 3378	30.0	74,4	23.5	296.7	415.1	29.183
152.492	10.7212	5.920	5•ē8ఫ	1.364	• 0488	38∙6	. 74.2	23,5	296.6	413° ä	5ã* ó ò Š
215,385	15,1431	7•292	3 <u>*</u> 30#	.1,680	•0632	47.6	73,9	23.3	296,5	413-1	29.046
307,038	21.5869	6.508	3.859	1.960	.07 <sub>0</sub> 3	55 <u>.</u> 5	73,6	23,1	296.3	412.5	5ā•00J
-0-001	-0.0001	8.509	3 <u>.859</u>	1,96g	•6763	55 <u>•</u> 5	73,6	23.1 ******	296•2 ****	412.5	29.001
							74.0	<b>23.</b> 3	296,5	415.4	29.189
					i .	OF VIATIONS	.3	•s	.2	1.2	<u>•</u> 085

16

### TABLE 30 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 9-10-76

TEST VUMBER 11

255 TP16

TEST DESCRIPTION

CONTAMINATED CONTROL - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 32.0-MG OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE = 1000 PSIA (NOMINAL).

ŤEST SPECIMEN INLET CONDÍŤIONS FLOWNETER CONSITIONS 

****	FLOWMETER ONE	****	*****	FLOWMETER THO	***			
FLOW RATE	PRESSURE (PSIA)	TEMP (DEG: F)	FLOW RATE (ACFH)	PRESSURE (PSIA)	TEMP	PRESSURE T	AVG TEMP FLOW RATE TG- F) (AGFM)	
• <b>9</b> 4	⇒0 • j	68.2	.91	47 <b>.</b> 8	75•2 <sub>.</sub>	1'15,9 7	11.70420	
<b>.</b> 76	50.1	57.4	•31	48.i	74.8	1 (15.9	11-1 0378	
<b>.</b> 67	50.4	66+5	<b>.</b> 70	48.9	74+1	1:11.9 ~ -7	0+2	
•56	50,1	65.0	•50	48.7	73.8	1-11-9	·0289`	
•49	50.1	66+3	<b>.</b> 5√	49.1	74.1	1:11.9 7	0.2 02440	:
<b> 40</b>	50.2	67.3	•40	49.5	75.1	1.11.9	1.2	
•30	50.2	69.1	.30	49.7	74.2	1015.9 7	2,6	
.26	49.9	69.7	• 25	49.3	76.5	1915.9 7	3.1 .0124	
.22	<b>#9.9</b>	74+1	•21	49.3	76.6	115.9	3.3	
<u>.</u> 14	54.2	71 • 4	.)3	49,9	7A.4	1015.9 7	3.9	
.14	50.2	72•5	.13	49,9	76.3	1015.9 7	4+4	
•22	50.1	72 <u>•</u> 2	•55	49.7	76.2	1/15.97	4.2	;
<u>.</u> 26	⇒o•s	72.0	.26	49.9	76.0	1015.9 7	'4+00129' —	
<b>.</b> 31	50.1	71.6	•31	49.5	75.8	1415.9 ž	9.7 .015Ż	
41	5J.Z	70+8	•41	49.5	75.2	1915+9 = 7	00\$0	
.49	49.7	70.2	•50	48.7	74.1	1915.9 7	2.1, .0241	
•58	50.2	69.5	•69	48.9	73.2	1:15.9 7	1.4 .0289	
•67	49.9	68.8	•71	48.3	72+3	1415.9	.0.6	
•76	50.1	67.7	•81	48.3	7] •6	1(15.9 6	9.70379'	
.84	50.2	67 • 2	•91	47.9	70.9	1015.9 6	9.0 .0423.	_,

PAGE: 2 DATE: 9-10-76

17

### TABLE 30 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONTROL - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 32.0 MG

OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE = 1000 TEST DESCRIPTION TEST FUMBER 11 PART 22C

PSIA (NOMINAL).

## TEST SPECIMEN INLET CONDITIONS

PRESSURE (PSIA)	AVG TEMP (DEG F)	AVG FLOW RATE (ACEM)	GROSS DIFF• PRESS PRIMARY (PSID)	GRCSS DIFF. PRESS SECONDARY (PSIn)	AVG GROSS DIFF. PRESS (PSIC)	TARE DIFF. PRESS- (PSID)	NEŤ -DÍFF¥ PRESS (PSID)	-
1015,9	71.7	.0420	137,940	137,949	137,940	→0.000	137,940	_
1015,9	71.1	• i)378	119,632	119,632	119,632	-0.000	119.632	7.
1011.9	70.2	.0336	103,218	173.218	193.218	-0.000	103,218	-
1011.9	69.9	.0289	84.837	85,542	85,174	-0.000	85,175	-
1011.9	70.2	.0244	68,661	69.443	69.n52	-0.000	69.052	371
1011.9	71.2	.0198	53.006	53,661	53,333	<b>~</b> 0.000	53,334	-
1015.9	72.6	•1149	38.916	39.197	39.012	-0.000	39.0i2	-
1015.9	73.1	.^124	31.326	31.453	31.390	-0.000	31.390	_
1015.9	73.3	.01.5	25.59.	25,653	25.622	-0.000	25.622	-
1015.9	73.9	.0166	15.1.13	15.115	15.109	-0.000	15.109	_
1015.9	74.4	.0166	15,103	15.229	15.166	-0.000	15.166	-
1015.9	74.2	.0110	26.865	26.973	26.919	<b>~</b> 0.000	26.919	
1015.9	74.0	.4129	32,659	32,833	32.746	-0.000	32.746	→ i
1015.9	73.7	. 1152	39,554	39.799	39.676	-0.000	39.677	-
1015.9	73.0	.0200	53,883	54,292	54.1188	-0.000	54.088	-
1015.9	72.1	.~241	67.911	68,496	68.204	-0.000	68.204	-
1015.9	71,4	. 1289	85,300	85,857	85.578	-0.000	85 <sub>•</sub> 579	-
1015.9	70.6	.n334	102.9.12	102,902	102,902	-0.000	102,903	_
1015.9	69.7	, 9379	121,210	121,210	121,210	-0.000	121.210	-
1015.9	69.0	.0423	141,728	141,728	141.728	-0.000	141,728	

TARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2,48070E-01 (ACFM) ##2 +

0 (ACFM) ##3

PAGE: 3 DATE: 9-10-76

TABLE 30
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST USPER 11

1.3

• 8

.089

PART 220

TEST DESCRIPTION

CONTAMINATED CONTROL - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 32.0 MG....
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 1000
PSIA (NOMINAL).

		i zuili) i	EDIA (NO								
	NET DIFFEREN	ទំពង់ដូនដូចជង.	****	****		T COMDITION		TEST S	****	***	***
		***	****	FLOK RATE	***	***	***	TEMPER, TURF		PRESSURE	
PS.ID	KG/SO CM DIFFERENTIAL	GN2 L8S/HR	KG/HR GNS	SCFM	4CFI4	LITERS/ MIN	DFG. F	nEG. C	DEG. K	PSIA	K@∕Sū ÇM
137.240	9,6981	<sub>]</sub> 2.565	5.699	2.894	•6420	82.0	71.7	22•1	295.2	. 1015,9	71,423
.119.632	8.4110	11.312	5.131	2,606	•4378	73•8	71 • 1	21.7	294.9	1015.9	Ť1.423
103.218	7+257.0	10.034	4•55 <u>1</u>	2,311	•1336	65•4	74.2	21.2	294.4	1011:9	71 <b>-</b> 144
85.175' -	5.9884	8.626	3.913	1.987	•289	58•3	69.9	23 • 1	294.2	1011-9	71•14 <u>4</u>
69,052	4.8549.	7.277	3.301	1.676	. :244	47.5	7: .2	21.2	294.4	1611.9	71.144
53\ <u>3</u> 34	3.7497	5.897 .	2.675	1.359	.:198	38•5	71.2	8.15	294.9	1011.9	71.144
39;012	2,7428	4.460	2,023	1,028	•J149	29.1	72,6	22,6	295,7	1015.9	71.423
31,390	2.2069	3,696	1,676	.851	•124	24.1	73.1	22.8	296.0	1015,9	71,423
25,622_	-1.8014	3.127.	1.415	.720	.0145	2n.4	73,3	23.0	296.1	1015.9	71.423
15,109	1.0623	1.962	•89ti	.452	•.)066	15*8	73.9	23.3	296,4	1015.9	71.423
15-166	1.0663	1.961	.490	.452	•.)n66	12.8	74.4	23,6	296.7	1015.9	71.423
26. <u>919</u>	1_8926	3,264	1.480	.752	.0110	21.3	74.2	23,5	296.6	1015.9	71,423
32.746	2.3023	3.849	1.746	.887	•0129	25.1	74	23.3	296.5	1015.9	71.423
39,677_	2.7895	4.533	2•156	1.044	.0152	29.6	73.7	23.2	296.3	1015.9	71.423
54_088	3.8028	5.965,	2.706	1.374	•0200	38.9	73.:	8.52	295.9	1015.9	71.423
68.204	4.7952	7.207	3,269	1.660	•0241	47.0	72.1	22.3	295.5	1015.9	71.423
85,579	6.0168	8.648	3.923	1.992	*9588	55.4	71.4	21.9	295.0	1015.9	71.423
102-903	7.2348	10.012	4.541	2.306	.0334	65.3	75.6	21.4	294.6	1015.9	71.423
121.210	8.5219	11.390	5.166	2.624	•0379	74.3	69.7	20.9	294.1	1015.9	71.423
141.728.	9.9645	12.728	5 <u>•</u> 7 <b>7</b> 3	2.932	•#423	d3•0	69 <b>.</b> n	20.6	293.7	1015.9	71.423
-	24,043	107120	-2.1-	-,,,,	******	~~~	***	4.88444	****	*****	***
*** ** ******	MARK 27 4124 THE INSTITUTE OF AS	•					72.0	22.2	295.4	1015.1	71.367

DEVIATIONS

1.5

PAGE: 1 DATE: 9-10-76

TABLE 31
FLOW RATE VCRSUS DIFFERENTIAL PRESSURE

TEST UMBER 11 PART 220 TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 32.0 MG OF SYNTHETIC CONTAMINANT ADDED, TEST SPECIMEN (S/N 022) INLET FRESSURE = 415 PSIA (NOMINAL).

FLOW/ETER CONDITIONS TEST SPECIMEN INLET CONDITIONS.

FLOWMEIER ONL			****	****		1	
FLOW RATE	PHESSURE (PSIA)	TEMP (DEG: F)	FLOW RATE (ACEM)	PRESSURE (PSIA)	TEMP (DEG. F)	PRESSURE	TEMP FLOW RATE
<u>.</u> 55	عَنْ وَحَ	81 • 6	•56	49.2	o2•4	416.9	82.0
<b>.</b> 50	90.6	81 ±6	•51	49.5	82+4	<b>416.</b> 2	82.0
<u>•</u> 40	5,0 4	81.0	• 4 !!	49.7	B2.5	415.2	82 <u>41 •0484</u>
.31	ຈຸບຸ•ຸຂ	81 <u>.</u> 6	•31	49 • 7	82∙7	415.6	82-1
•56	à5•€	81.7	<u>.</u> 25	5υ <u>•</u> 1	85•3	415.6	82 <u>•3</u>
•śj	÷õ*5	51 <u>.</u> 9	.20	49.9	43.,.	415.6	82.5
<u>•14</u>	무있 <del>:</del> 1	82 <u>•</u> 2	•1 <del>4</del>	49.9	83.3	415.6	82 <u>.</u> 8
214	42.9	82 <u>.</u> 5	- +14	49,3	63•ౖ5	415.6	,83_00166
•\$5	47.5	B2 <b>±</b> 5	• 22	49.5	b3 <b>.</b> 5	415.6	83.00265
<u>•</u> 27	47.9	82 <u>±</u> 4	• 26	44.3	<b>83</b> •5	415.6	82.9 .0316
<u>.3</u> 1	47:1	8 <u>2 ±</u> 4	<u> </u>	49.2	33.5	415.6	83.0
<u>•</u> 41	47.5	82 <u>•</u> 3	•41	49.2	n3•5	415.6	82.9 .0487
<u>•</u> 50	àã≆T	82*1	. g5v.	49.2	r3•3	414,3	82.7 .0599
<u>•54</u>	àñ∙s	82.4	• 55	49 <sub>•</sub> 2	53•4	414.3	82.9
	FLOW RATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE:  AATE	FLOW RATE (RSIA)  (ACEM)  (55)  150  140  140  141  14  14  14  14  14  14	FLOW RATE PHESSURE TEMP (DEG: F)  150 PU.6 B1.6  150 PU.6 B1.6  140 PU.4 B1.0  131 PU.2 B1.6  126 PU.6 B1.7  121 PU.8 B1.7  121 PU.8 B1.9  124 PU.9 B2.2  14 PU.9 B2.5  127 PU.9 B2.5  128 PU.9 B2.4  14 PU.9 B2.4  150 PU.1 B2.1	FLOW RATE (ACEM)         PRESSURE (DEG: F)         TEMP (ACEM)         FLOW RATE (ACEM)           :55         PU: C         81:6         :56           :50         PU: C         81:6         :56           :40         PU: C         81:6         .51           :40         PU: C         81:6         .51           :40         PU: C         81:0         .40           :31         PU: C         81:0         .40           :31         PU: C         81:0         .40           :26         PU: C         81:7         .25           :21         PU: C         81:7         .25           :21         PU: C         81:9         .20           :14         PU: C         82:2         .14           :14         PU: C         82:2         .14           :22         42:5         82:5         .22           :27         42:9         82:4         .26           :31         42:1         .41           :41         42:9         82:3         .41           :50         PU: L         82:1         .50	FLOW RATE (ACEM)         PHESSURE (DEG. F)         FLOW RATE (ACEM)         PRESSURE (PSTA)           155         DU. C         81.6         .56         49.2           150         DU. C         81.6         .51         49.5           150         DU. C         81.6         .51         49.5           140         DU. C         81.6         .31         49.7           131         DU. C         81.6         .31         49.7           131         DU. C         81.7         .25         50.1           121         DU. C         81.7         .25         50.1           121         DU. C         81.9         .20         49.9           14         DU. C         81.9         .20         49.9           14         DU. C         82.2         .14         49.9           14         DU. C         82.5         .14         49.9           122         DU. C         83.5         .22         49.7           14         DU. C         83.2         .22         49.7           15         B3.2         .22         49.7         49.2           27         DU. C         82.4         .31	FLOW RATE (ACEM)         PHESSURE (PSIA)         TEMP (DEG: F)         FLOW RATE (ACEM)         PRESSURE (PSIA)         TEMP (DEG: F)           :55         DU:C         81:6         :56         49:2         52:4           :50         DU:C         81:6         :51         49:5         82:4           :40         DU:A         81:0         .40         49:7         82:5           :31         DU:C         81:6         .31         49:7         82:5           :31         DU:C         81:7         .25         50:1         82:8           :21         DU:C         81:7         .25         50:1         82:8           :21         DU:C         81:9         .20         49:9         83.3           :21         DU:C         81:9         .20         49:9         83.3           :14         DU:C         82:2         .14         49:9         83.3           :14         DU:C         82:5         .22         49:7         53:5           :22         DU:C         83:5         .22         49:7         53:5           :27         DU:C         82:4         .26         40:3         83:5           :31 <td< td=""><td>FLOW RATE (ACEM)         PRESSURE (ACEM)         TEMP (ACEM)         FLOW RATE (ACEM)         PRESSURE (DEG. F)         TEMP (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSUR</td></td<>	FLOW RATE (ACEM)         PRESSURE (ACEM)         TEMP (ACEM)         FLOW RATE (ACEM)         PRESSURE (DEG. F)         TEMP (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSURE (DEG. F)         PRESSUR

770



TABLE 31 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 9-10-76

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 32.0 MG OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE = 415 PSIA (NOMINAL). TEST NUMBER 11 TEST DESCRIPTION PART 220

ESSURE PSIA)	AVG LEMP (DEG. F)	TOW RATE	DIFF. PRESS PRÍMARY (PSID)	DIFF. PRESS SECONDAPY (PSIO)	AAG ČKOSŠ Dille ŠKOSŠ OKOSŠ	ȚARE D <u>IFF</u> PRESS (PSID)	NET DIFF. PRESS (PSID)	<b>.</b>
416.4	\$2.0	•1,664	307.129	3,,7,129	397• 124	•001	307.128	
416.2	82.3	.46 6	242,730	242.736	242.736	•000	242.735	
416.2	82 <u>*</u> 1	. 484	163.823	199.823	16á*9Să	.000	163.823	•
412°ë	¤2•1	. 309	111,425	111.425	111.425	• 000	111.424	٠
415.0	¤2 <u>•</u> 3	.03 8	86,935	87.435	87.185	•000	87.185.	
415.9	b2.5	. 125.	66.214	66.918	66.561	•000	66,560	
415.0	8. se	. 167	41,234	41.413	41.324	.000	41,323	
415.6	a3 <sup>*</sup> ំ	• L166	40.770	44.952	40.561	• 000	40.861	
415.6	ط3 ≛،)	. 1265	71,576	72.284	71.93ų	•000	71.990	
415.0	82 <u>.</u> 9	316	98°655	9 ,,592	90.109	• 0 0 0	90.108	
415.0	83.0	. <sub>1</sub> 366	113,794	111,794	110.794	.000	110.793	
415.0	85 <b>∓</b> 8	•0487	165.086	165, ,66	165,085	•000 "	165 085	
414°4	7ءِ5	, ;5ÿ9¨´	238,940	<u>ئ3</u> 8،948	238,945	.000	238,948	
414.2	ø <u>z•</u> 9	6 <del>5</del> 3	295.760	295.766	295.766	-001	295.765	

J.

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13

48

PAGE: 3 DATE: 9-10-76

TABLE 31 FLOW RATE VERSUS DIFFLRENTIAL PRESSURE

TRET 'UMBER II PART 220 TEST DESCRIPTION CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 32.0 MG OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE = 415 PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS NET DIFFERENTIAL PRESS \*\*\*\*\* PRESSURE LEM-ERATURE FLOW RATE \*\*\*\*\*\*\*\*\* KG/SQ CM LATERS/ 6145 GNZ KG/SQ CM LH5/HR DIFFERENTIAL PSAD PSIA DEG. K ยธิG. . L OCG. F MIN 1CFN SCFM Kg/HK 29.311 21.5933 \_\_\_ \_307.128 416.9 300.9 52.2 7.995 27.8 32., . 664 1.842 3.020 29.265 416.4 300.9 27.0 g2. 47.5 • 4694 1.678 3:303 7.282 17.0660 242./35 11.5179. \_\_\_163.823. : in 27.265 416.6 301 • 0 27.0 52.1 • 1454 1.341 2:240 5.820 38 e g 29.219 415.0 301.0 27.0 82.1 28.9 و ۲۰۵۰ و 1.019 4.424 7.6339. \_\_\_111.424 2100! 29,219 415.0 1,575 27 9 .851 6.1297 87.185 301.1 82.3 24.1 . 439.1 3,694 29,217 415,0 1.35% 2,997 301.2 58. g2.5 19.5 690 4.6797 66.560 ...250 58.518 415,0 301.4 29.2 82.B .907 13.1 . 157 .462 2.004 29.219 415,0 2.8728 40.861 301.5 211.4 83.0 13.0 .0166 .458 .401 1.987 29,219 412.9 301.5 20.4 ₫3., 20.1 ...205 .732 1.441 3.178 5.0572 71.930 29.219 415.0 3().5 82.9 1:717 3.791 6.3353 \_\_\_ 90.108\_ 21.5 64.7 . 316 .873 29.219 415.0 301.5 28.5 83.0 •0366 1.985 4.379 7.7895 110.793 28.6 1.009 29.219 415.0 3 1 . 4 24.3 32.9 33.0 · . 487 1.343 2.045 5.331 11.6066 165.085 29.128 414.5 52.7 . 599 16.7997 238,948 361.3 24.2 . 46.7 1.648 3.245 7.154 29.128 414.3 301.4 20.7943 295.765 5H.3 82.9 50.9 , a653 1.796 3.535 7.795 \*\*\* \*\*\*\* \*\*\* \*\*\* 29,219 415.0 301.3 29. 1 4,50 .026 .4 DEVIATIONS .4

PAGE: 1 .... DATE: 9-10-76 .

## TABLE 32 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST WUMBER 11 P4RT 22E1 TEST DESCRIPTION

CONTAMINATED CONTROL - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE, TOTAL OF 53.2 MG
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 1000
PSIA (NOMINAL).

.1	*****	***	FLOWMETER	ŤESŤ SPE	T SPECIMEN INLET CONDITIONS				
	FLOWMLTER ONE			****	FLOWMETER TWO	****		*	, 
	FLOW RATE (ACFM)	PRESSURE (PSIA)	ŤEMP (DEG• F)	FLOW RATE (ACFM)	PRESSURE (PSIA)	ŤEMP (DEG. F)	PRESSURE (PSIA)	_AVG_ TEMP (DEG•_F)	FLOW RATE
	.87	50·1	66 • B	•91	47.8	72•4	1009.2	69•6	0432
	•78	49.9	65 • 9	•81	48.9	7i•6	1009.2	68.8	. •0385
η	•67	<b>50.5</b>	65•6	•71	49.7	71.1	1009.2	68•4	• 0338
	•58	50.1	65.7	.60	48.8	71.1	1009.2	68,4	.0290
	•49	>0.3	65.8	•51	49.3	71.1	1409+2	68.5	.0247
	<b>.</b> 40	50.1	66.3	.40	49.3	71.3	1909.2	<del>5</del> 8*8	
	.30	49.7	. 67•0	▶30	49.2	7 <b>1.</b> 8	1009.2	69 <u>.4</u> ·	0149
	•26	49.9	67•4	• 26	49.3	71.8	1009.2	69,6	.0127
1	•21	50.1	67.9	.20	49.7	7 <b>i.</b> 8	1009.2	69.8	
	•14	49.7	68•7	• ī 4	49•3	71.8	1909.2	70.2	•0068
	•14	49.7	69•9	•14	49•3	Ž2•8	1009.2	71.3	· 8600•
	•22	49.4	69+5	•22	48.8	72.6	1009.2	Ť1•0 "	10108.
	.27	49,9	69•5	, 26	49.3	72.9	1009.2	71 <b>.</b> 2	.0130
	.31	50.1	69•4	•31	49.5	73.1	1009.2	Ť1•2 .	•0151
t	<b>,</b> 41	49.9	68•8	.41	49,2	73.0	1009,2	70,9	10201
	.49	49.5	68•1	•51	48.6	72.6	1009.2	70.3	0243
	.58	50.1	67.5	.60	48.8	72.2	1009.2	69.8	.0290
	<b>.</b> 67	50.5	66.6	.71	49.0	71.5	1005.3	69.0	0341
	.76	49.9	65•7	.81	48.2	7n•9	1005.3	68,3	.0383
	.84	50.3	65.1	.91	48.0	70.2	1005.3	67. <sub>•</sub> 7	0427

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FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 9-10-76

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 53.2 MG OF SYNTHETIC CONTAMINANT ADDED, TEST SPECIMEN (S/N 022) INLET PRESSURE = 1000 TEST NUMBER 11 TEST DESCRIPTION PART 22E1

PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*

PRESSUME (PSIA)	AVG TEMP (DEG. F)	AVG FLOW RATE (ACFM)	GROSS DIFF∙ PRESS PRIMARY (PSID)	GROSS DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF: PRESS (PSIU)	TARE DIFF• PRESS (PSID)	NET DIFF. PRESS (PSID)
1009.2	69.6	. 9432	148.963	148,963	148.963	-0.000	148,963
1009.2	68.8	.0385	128.104	128.104	128.104	-0.000	128.104
1009.2	68.4	.0338	110.405	110.405	110.405	-0.000	110.406
1009.2	68.4	.0290	90.309	91.127	90.718	-ò.000	90.718
1009.2	68.5	. 9247	73,371	74.n6b	73.716	<b>~</b> 0•000	73.716
1009.2	68.8	.n197	55,457	56,362	55.909	-0.000	55.909
1009,2	69.4	.0149	40.172	40.426	40.299	-0.000	40.299
1009.2	69.6	.0127	33,277	33,4-0	33.364	-0.00ō	33,364
1009.2	69.8	.0103	25.861	25,915	25.888	-0.000	25.868
1009•2	70.2	.0068	16.185	16.164	16.174	-0.000	16.175
1009.2	71.3	.0068	16.011	16,221	16,116	-0.000	16.116
1009.2	71+0	.0108	27.251	27,409	27.330	-0.000	27.330
1009.2	71.2	+0130	34.030	34.257	34.143	-0.000	34.144
1009.2	71.2	.0151	40.867	41.177	41.022	-0.000	41.022
1009.2	70.9	.0201	56,461	56,994	56.727	-0.000	56.727
1009.2	70.3	.n243	7ĭ.998	72.48n	72.239	-0.000	72,239
1009.2	69.8	.0290	90.309	91.127	90.718	-0.000	90.718
1005.3	69.0	.0341	111.354	111.354	111.354	-0.000	111.354
1005.4	68.3	.0383	129,684	129,694	129.684	-0.000	129,685
1005.3	67.7	.0427	151,491	151,491	151.491	<b>~0.00</b> 0	151,492

IARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM) \*\*2 +

0 (ACFM) ##3

PAGE: 3
DATE: 9-10-76

## TABLE 32 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 53.2 MG. OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE = 1000.

TFST WUMBER 11

PART 22E1

TEST DESCRIPTION

PSIA (NOMINAL).

NET DIFFERENTIAL PRESS TEST SPECIMEN INLET CONDITIONS

11	***	***************************************										04040460000000000000000000000000000000		
	PRESSURE		TEMPERATURE			****	*****	FLOW RATE	****	***				
	KG/SQ CM	PŞIA	DEG. K	DEG. C	DEG. F	LITERS/ MIN	\CFM	SCFM	GN2 K₫∕H₽	GNŹ LB <b>S/</b> HR	ŘG/ŠQ ČM DIF <u>Fer</u> ential	PSID		
	70.956	1009:2	294+1	20.9	69.6	84.0	.0432	2.966	5.839	12.874	10.4732	148.963		
	70.956	1009,2	293,6	20.4	68,8	75.1	.0385	2,652	5,221	Ĩ1.511	9 <u>.0066</u>	128.104		
ţı	70.956	1009.2	293.4	20.2	68,4	65.9	.0338	2,327	4.581	10 • 100	7.7623	110.406		
	70.956	1009.2	293.4	20.2	68,4	56.5	.0290	1.996	3•33j	8.667	6.3781	90.718		
	70.956	1009.2	293.4	20.3	68,5	48.1	• 1247	1,697	3.342	7.368	5.1827	_ <u>7</u> 3,716		
	70.956	1009.2	293.6	20.4	68.8	38.3	•)197	1,353	2 • 665	5.875	3.9308	55.909		
	70.956	1009.2	293.9	20.8	69,4	29•0	•0149	1.024	2:015	4.445	2.8333	40• <u>299</u> _		
	70.956	1009•4	294.1	20.9	69.6	24•7	.0127	.873	1.719	3.789	2.3457	33+364		
ţ	70.956	1009,2	294.2	21.7	69,8	20.0	•0103	.705	1,387	3 • 058	<u>1.820í</u>	25.888		
	70.956	1009.2	294.4	21.2	70.2	13.2	.0068	.465	•916	2.020	1.1372	, 16 <b>.1</b> 75		
	70.956	1009.2	295.0	21.9	71.3	13.2	•0068	.464	•915	2.016	1.133i	ĩ6. <u>1</u> 16		
	70.956	1009.2	294,8	21.7	71.0	20.9	.0108	,739	1 • 455	3.208	1.9215	27,330		
	70.956	1009.2	294.9	21.8	71.2	25+2	.0130	.890	1.753	3.865	2.4005	34.144		
	70.956	1009.2	295.0	21.8	71.2	29 • 4	•0151	1.037	2 <u>•</u> 04]	4.501	2.6841	41.022		
	70.956	1009.2	294.8	21.6	70,9	38.9	.0201	1.374	2.706	5.966	3,9883	56,727		
	70.956	1009.2	294.5	21.3	70.3	47.2	.0243	1,665	3,279	7.230	5,0789	72.239		
	70.956	1009.2	294.2	21.0	69,8	56.4	+0290	1.991	3.920	8.643	6.3781	90.718		
	70+677	1005.3	293.7	20.6	69.0	66•2	•0341	2.339	4 <u>•6</u> 05	ĭ0•152	7,8290	111,354		
	70.677	1005.3	293.3	20.2	68,3	74.3	•0383	2,625	5,170	11+397	9.1177	129.685		
	70.677	1005.3	293•0 ****	19.8 *****	67.7 *****	83•0	•0427	2.931	5.770	í2•722	10 <u>+</u> 6509	151,492		
	70.914	1008.6	294•1	20.9	69.6						<u></u>			
	•071	1.0	•5	•5	•9	DEVIATION:	s					~ ·		

# TABLE 33 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 11

FLOWMETER CONDITIONS

PART 22F

TEST DESCRIPTION

PAGE: 1 DATE: 9-10-76

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 52.2 MC OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE = 415 PSIA (NOMINAL).

# TEST SPECIMEN INLET CONDITIONS

FLOWMETER ONE			***	*****	FLOWMETER TWO	****			
	FLOW RATE (ACFM)	PRESSURE (PSI <sub>A</sub> )	ŤEMP (DEG• F)	FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG. F)	PREŚŚURE (PSI <sub>A</sub> )	AVG TEMP (DEG. F)	FLOW RATE (ACEM)
	•53	50.1	76 • 2	•54	49•n	77.4	416.2	<del>7</del> 6∙8	
	<b>•</b> 50	50.4	76 <u>•</u> 4	•51	49•3	77.5	4ī5•6	76+9	0603
l	•40	50.4	76•5	• 40	49•Ť	77.7	415•6	77+1	•0485
	•31	50.4	76+7	•30	49.9	77.8	415.6	<b>77.2</b>	0368
	.26	50.4	76.8	•26	50.Ï	77.9	415.6	ŤŢ•3	.0313
	•21	<u>5</u> 0.4	76.9	•20	50 <b>.</b> 1	78.1	415.6	77.5	.0249
	.14	20°5	7Î.2	.ī3	49.9	78 <b>.</b> 5	415.6	ŤŤ•8.	0164
	-14	50.1	77•6	•13	49.9	78.8	415.6	<b>78</b> ∙2	•0163 <u> </u>
	•22 .	49.9	77•6	•21	49.3	78•9	4 <u>1</u> 5.6	78.3	0256
	•26	50.2	77 <u>°</u> 6	•26	49.9	79 • n	414.9	78.3	•0316
	•31	49.9	77•7	•31	49•3	79•2	414.3	78•4	•0373
	•41	50.1	77.6	•41	49.3	79.2	413.7	78.4	
	•49	50.2	77 <u>•</u> 6	•50	49•2	79.3	413.0	78.4	• 0599 <u>'</u>
	•53	49.9	77.9	•54	49.0	79.4	413.0	78.6	•0639

PAGE: 2 DATÉ: 9-10-76

# TABÎE 33 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PART 22F TEST NUMBER 11 TEST DESCRIPTION

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CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 52.2 MG OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (8/N 022) INLET PRESSURE = 415 PSIA (NOMINAL).

416.2		(ACFM)	PRIMARY (psid)	SECONDARY (PSID)	DÎFF. PRESS (PSID)	DIFF PRESS (PSID)	NET DIFF• PRESS (PSID)
	76.8	•0642	306.919	306.919	306.919	•001	306.918
415.6	76.9	.0603	259,571	259.571	259.571	•000	259.570
415.6	77.1	•n485	172.451	172.45î	172.451	•000	172.450
415.6	77.2	.0368	i15.634	115,634	115.634	•000	115.633
415.6	77.3	•ñ313	92.101	92.59i	92.346	•000	92.346
415.6	77.5	•0249	68.121	68.602	68.361	•000	68.361
415.6	77.8	.a164	41.562	41.759	41.661	-0.000	41.660
415.6	78.2	.n163	41.273	41.471	41.372	÷0.000	41.371
415.6	78.3	. 1256	7à.619	71.442	71.031	•000	71.030
414.9	78.3	•ñ316	92,587	93.53 <u>ê</u>	93.062	•000	93.062
414.3	78.4	. 1373	117.528	117.528	117.528	•000	117.527
413.7	78.4	•ñ492	175.292	175.292	175.292	•000 °	175.291
413 <u>.</u> 0	78.4	• 0599	255,467	255,467	255,467	.000	255.467
413.0	78.6	•n639	306.919	306,919	306.919	•00Î	306.918

### TABLE 33 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 9-10-76

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 52.2 MG OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET FRESSURE = 415 PSIA (NOMINAL).

PART 22F TEST NUMBER 11 TEST DESCRIPTION

	******	****	*****	TEST S	PECIMEN INL	T CONDITIONS	5 *******	***	***	***	NET DIFFEREN	NTIAL: PRESS	
•	PRESSL	RE	****	TEMPERATURE	***	****	*****	FLOW RATE	***	***			
	KG/SQ CM	PSIA	DEG. K	DEG. C	DEG. F	LITERS/ MIN	ACFM	SCFM	KĞ∖HĞ GNS	GN2 LBS/HR	KG/SQ CH DIFFERENTIAL	PSID	
	29.265	416.2	298.0	24.9	76.8	5g•8	• 9642	1.795	3 • 53 <del>4</del>	7.792	21,5785	366×918	
	29.219	415.6	298•1	25.0	76.9	47.7	•0603	1,684	3.316	7-310	18,2496	259,570 _	
į	29.219	415. <u>6</u>	298.2	25•1	77.1	38•3	• 485	1.353	2 • 665	5.874	12.1245	172.450	
•	29.219	415.6	298.3	25.1	77.2	29•1	•0368	1.027	2.022	4.457	9+1298	115.633	
	29.219	415.6	298.3	25.2	77.3	24.8	•#313	.874	1.721	3,795	6,4925	92.346	
	29.219	415.6	298.4	25.3	77.5	19.6	•a249	.694	1 <u>•</u> 36 <u>6</u>	3.011	4.8062	68,361	
	29,219	415.6	298.6	25,5	77,8	13.0	.0164	.458	•90\$	1.988	2.9290	41.660	
	29 <b>,</b> 219	415.6	298.8	25.7	78.2	12• <sup>9</sup>	•0163	.454	.894	1.971	2.9087	41.371.	
r	29.219	415.6	298.9	25.7	78,3	20+2	.0256	.712	1.401	3.089	4,9939	71,030	
	29.174	414.9	298.9	25.7	78.3	24.9	. 1316	.878	1.728	3.810	6,5429	33*065	
	29.128	414.3	299.0	25.8	78.4	29.3	.0373	1.035	2 <u>•</u> 038	4.494	B.2630	<u>"</u> "7,527_"	
	29.083	413.7	298.9	25.8	78,4	38.6	• 0492	1.362	2,683	5.914	12.3242	175,291	
	29.037	413.0	299.0	25.8	78.4	46.9	• 0599	1.656	3 <u>•</u> 260	7•188	17.9611	255,467	
	29,037 ****	413.U	299.1	25.9 *****	78,6	50.0	.0639	1,765	3.476	7.663	21.5785	306.918	
l,	29.177	415.0	298,6	25.5	77.8								
	.061	.9	•3	•3	•6	DEVIATION	s					,	

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL\_OF\_74.3\_MG. -

PAGE: 1 DATE: 9-10-76

OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE = 1000

TABLE 34
FLOW RATE VEPSUS DIFFERENTIAL PRESSURE

TEST JUMPER 11

PART 22G

TEST DESCRIPTION

PSIA (NOMINAL). TEST SPECIMEN INLET CONDITIONS

į.	****	****		CONDITIONS	*****	***	TEST SPE	TEST SPECIMEN INLET CONDITIONS			
	****	FLOWMETER ONE	****	*****	FLOWMETER TWO					1	
	FLOW RATE (ACFM)	PRESSURE (PSIA)	TFMp (DEG+ F)	FL <sub>O</sub> W RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG• F)	PRESSURE (PSIA)	TEMP (DEG. F)	FLOW RATE		
	•87	49.7	76 <u>•</u> 7	•91	47.4	81.7	1913.2	79+2	. #0426		
	.78	50.4	74.7	•81	48.4	`6•2	1013+2	77.5	<b>•</b> 0388	-	
ŀ	•69	50.4	74•4	•71	49 • D	79+9	1)13.2	77•2	• 0343		
	.60	50.2	74+3	•61	49• ^	79.7	1913.2	77+0	. +0297		
	.50	50.1	74+5	•50	49•2	79.6	1^13.2	<b>77</b> +0	+02 <b>4</b> 6 "	1	
	.41	56.1	74.8	•40	49.3	79.8	1 13.2	77.3	02ól		
	•32	50.4	75•5	•31	49+9	რ <b>ე ⊕</b> 3	1/17+2	77•9	+0157		
	•27	49.9	76•2	• 25	49.3	80.6	1413.2	78•4	•0128		
i,	•22	50.2	76•9	•20	49.9	71.1	1:17.8	79.0	49194		
	•15	49.9	77.8	•13	49.5	8j•6	1:17.2	79.7	.0068		
	.15	49.5	79•7	.13	49•:	82.8	1 -17.2	81.3	.0068	j	
	•55	49.5	79 <u>+</u> 7	•51	49.^	82.6	1/17.2	81.3	.0106		
	.28	49.9	79.5	. 26	49.3	82.6	1017.2	81.1	.0131		
	•32	50.2	79+1	•31	49.7	82.5	1,17.2	80.8	.0154		
ž	.42	49.9	78 <u>•</u> 6	•41	49.2	82.3	1,17.2	<u>80.4</u>	.0201		
	,52	50.2	77.6	•51	49.2	81.7	1 13,2	79.7	• 025Ź		
	.60	50.4	76+9	•61	49+2	91.3	1 13.2	79+1	•0298	1	
	.70	56.1	75•9	+71	48•4	80.6	1913.2	78.2	341		
	•76	50.2	75•1	•81	48.4	79•8	1413.2	77•4	.0380		
	.84	50.1	74.5	.91	47.8	79.2	1013,2	76.8	.0423.	-	

PAGE: 2 DATE: 9-10-76

TABLE 34 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 74.3 MG. .\_ OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 1000\_\_\_\_\_\_ TEST NUMBER 11 PART 226 TEST DESCRIPTION PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*

PRESSURE (PŜĨA)	AVG Temp (Deg. f)	AVG FLOW RATE (ACFM)	GROSS DIFF• PRESS PRIMARY (PSID)	GR'SS DIFF• PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSIU)	TARĒ DIFF• PRESS (PSĪD)	NET DIFF. PRESS (PSID)	Ų
1013.2	79.2	. 1426	153.617	153.617	153.617	<b>-0.000</b>	153.617	-
1013.2	77.5	. 1388	135.941	135.941	135.941	-0.000	135.941	-
1013.2	77.2	. 1343	115.739	115.739	115.739	-0.000	115.739	***
1013.2	77.0	.6297	96.169	96.169	96.169	-0.000	96.169	
1013.2	7 <b>7.</b> 0	.n246	75,314	75,967	75.640	-0.000	75.641	. 1
1013.2	77.3	.0201	58.187	58.646	58.396	-0.000	58.397	•
1017.2	77.9	.0157	43,767	44.009	43.888	<b>-0.000</b>	43,888	-
1013.2	78.4	.0128	34.103	34,271	34.187	-0.000	34,187	
1017.4	79.0	•9104	26.523	26.629	26.576	-0.000	26.576	
1017.2	79.7	.0068	16.454	16.544	16.499	-0.000	16.499	
1017.2	81.3	.0068	16.164	16.315	16.240	-0.000	16.240	· 1
1017.2	81.3	•01-16	27.275	27.49n	27.382	-0.000	27.383	
1017.2	81.1	.0131	35,145	35,422	35,283	-0.000	35.284	2740
1017:2	80.B	.0154	42.552	42.797	42.675	-0.000	42.675	
1017.2	80:4	.0231	57,936	58.290	. 58.113	<b>-0.000</b>	58.114	•
1013.2	79•7	.0252	76.806	77.229	77.018	-0.000	77.018	•••••
1013.2	79.1	.0298	96.169	96.169	96.169	-0.000	96.169	1
1013.2	78.2	.0341	114,792	114.792	114.792	-0.000	114.792	,
1013.2	77.4	.0380	135.941	135.941	135.941	-0.000	135.941	
1013.2	76.8	• 0423	159.299	159.299	159.299	-0.000	159.299	
						••		

IARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM) + +2

0 (ACFM)\*\*3

PAGE: 3 DATE: 9-10-76

### TABLE 34 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 11 PART 226

OF SYN

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE, TOTAL OF 74.3 MG
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 1000
PSIA (NOMINAL).

									TOTA (HOLLI				
	***	***	***	TEST S	PECIMEN INLE	T CONDITIONS	S pp###########	****	***	***	NET DIFFEREN	TIALI PRESS	
ii	PRESS	JRE		TEMPERATURE				FLOW RATE	****				
	KG∕SQ CM	PSIA	DEG. K	DEG. C	DEG. F	LITERS/ Min	ACFM	SCFM	KG\H <sup>k</sup> G⋈5	CH2/HB	KG/SQ CM DIFFERENTIAL	esio	
	71.235	1013.2	299.4	26.2	79.2	81.6	.0426	5.883	5.676	12.514	10.8004	iš3. <u>6</u> 17	
	71.235	1013.2	298.4	25.3	77.5	74.6	88E <sub>1</sub> .	2.635	5.189	11-440	9,5576	. já5•941	
	71+235	1013+2	298•3	25+1	77.2	66•1	•n343	2.336	4.599	i0•139	. <u>8:137</u> 3	115.739	
ι,	71.235	1013.2	298.2	25.0	77+0	<b>57∙</b> 2	•0297	2.019	3.976	8.765	<u>6.76</u> 13	96.169	
	71•235	1013-2	298•2	25•0	77.0	47•4	• v246	1.674	3 <u>•</u> 29 <u>6</u>	7.266	5.3181	75 <u>.6</u> 41	
	71.235	1013.2	298.3	25.2	77.3	38.7	•0201	1.365	S•688	5,925	4.1057	58,397	
	71.514	1017.2	298.7	25,5	77.9	30.3	.0157	1.071	2.109	4,649	3.0857	43,888	
	71.235	1013.2	298.9	25.8	78.4	24.5	•:128	.866	1.706	3.761	2.4036	34.187	
1	71.514	1017.2	299.3	26.1,	79.0	20.0	.0104	.70 <del>6</del>	1,390	3.065	1.8685	26,576	
. '	71.514	1017.2	299.7	26.5	79.7	13•1	•0068	.464	914	2.015	1,1600	<u>16.499</u>	
	71.514	1017.4	300.5	27.4	81.3	13.0	.0068	.458	•903	1.990	1.1418	16,240	1
	71.514	1017.2	300.5	27.4	81.3	20+4	-0106	.719	1.416	3.121	1.9252	27.383	
	71.514	1017.2	300.4	27.3	81.1	25.2	•0131	.890	1.753	3 <sub>*</sub> 864	2.4807	35,284	
	71.514	1017.2	300.3	27.1	80.8	29.6	.0154	1.047	2.062	4,545	3.0004	42,675	
ı	71.514	1017.2	300.1	26.9	80.4	38.6	.0271	1.363	2,684	5,918	4.0858	58,114	•
	71.235	1013.4	299,6	26.5	79.7	48,3	.0252	1.706	3,359	7.405	5,4149	77.018	
	71.235	1013.2	299,3	26.1	79.1	57.1	.0298	2.016	3 <u>.</u> 970	8.752	6,7613	96.169	Ĵ
	71,235	1013.2	298.8	25.7	78,2	65,6	.0341	2,317	4,563	10.059	8.0707	114;792	
	71.235	1013.2	298,4	25.2	77.4	73.2	.038n	2,585	5.091	11.223	9.5\$76.	.135.941	
	71.235	1013,2	298.1	24_9	76 8	81.4	.9423	2.876	5.063	<u>1</u> 2.485	11;1998	<u>159,299</u>	-
	71.347	1014.8	299.2	26.0	78.8					•			•
	.134	1.9	•7	•7	1,3	DEVIATION	S						

TABLE 35
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

FLOW RATE VERSUS DIFFERENTIAL PRESSUR

TEST NUMBER 11

PART 22H

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 74.3 MG
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 415
PSIA (NOMINAL).

PAGE: 1 DATE: 9-10-76

TEST SPECIMEN INLET CONDITIONS

FLOWMETER ONE			****	FLOWMETER TWO	· 保险性动物会会会会会		• 5-	1
FLOW RATE (AÇFM)	PRESSURE (PSIA)	ŤEMP (DEG. F)	FLOW RATE (ACFM)	PRESSURE (PSIA)	ŤЕМР (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	FLOW RATE
•53	49.9	82.6	•52	48 • 8	83.7	418.8	8 <b>3•</b> Ĩ.	0 <u>6</u> ž1
•47	50.1	82.6	•46	49.2	83.7	418.2	g3.Î	, <b>"</b> 05\$3
.42	50,4	82.6	.40	49.5	83.7	418.2	83.1	.0490
•32	50.2	82+5	•30	49.7	83.5	417.5	83•0	0372.
•27	50.2	82•3	•25	49.9	R3•4	4j7•5	82.9	.0313
.22	50.6	B2.5	•20	50.i	83.5	416.9	83.0	0255
+14	50.8	82+6	•13	59+3	83•7	416.9	83•1	0169
•14	50.2	82•9	•ï3	49.9	A3.9	416.9	83.4	.0166
•55	50.1	82.7	•21	49.7	83.9	416.9	83.3	0257
•27	50.2	B2•6	•25	49.9	83.7	416.2	83.1	sīÉo.
•32	50.1	82-1	•31	49.3	83.5	415.6	82.8	.0378
•42	49.9	81.9	•41	49.2	83.3	415.6	82.6	
•46	50.1	8 <u>1</u> .6	.45	49.2	83.0	415.6	82.3	•05¥8
.51	49.9	81.6	.50	48.8	82.9	414.3	82.Ž	.0602

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PAGE: 2 DATE: 9-10-76

### TABLE 35 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PART 22H TEST DESCRIPTION TEST NUMBER 11

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE, TOTAL OF 74.3 MG
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 415
PSIA NOMINAL.

PRESSURE (PŠIA)	AVG TEMP (DEG. F)	AVG FLOW RATE (ACFM)	GROSS DIFF. PRESS PRIMARY (PSID)	GROSS DIFF. PRESS SECONDARY (PSID)	AVG GROSS Diff• Press (Psid)	TARE DIFF• PRESS (PSID)	DIFF PRESS (PSID)	
418.8	83.1	•n621	307,445	307,445	307.445	.ooi	307.444	
418,2	83.1	•n553	230.741	230.741	230.741	.000	230.741	
418.2	83.1	•0490	186.550	186.55n	186.550	.000	โ <del>ล</del> 6.55ชั	
417.5	83.0	•0372	122.788	122,788	122.78B	.000	122.788	
417.5	82.9	•n313	95.958	95.958	95.958	•000	95.958	V
416.9	83.0	• 0255	72.442	73.231	72.836	•000	7Ž.836	
416,9	83.1	•0169	43,594	43.894	43.744	•000	43.743	
416+9	83.4	•n166	42.841	43.086	42.964	•000	42.963	
416.9	83.3	.0257	73.064	74.178	73.621	• 0 0 0	73.621	
416.2	83.1	• • 312	95,327	95.327	95,327	•000	95,326	
415.6	82.8	•1378	124.682	124,682	124.682	•000	124.682	(
415.6	82.6	•0499	190.969	190,969	190.969	•000	190.969	-
415.6	82.3	•n548	228,216	228,216	228.216	•000	228.216	
414.3	82.2	.0602	282.508	282,508	282,508	•000	282.508	

TARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM)\*\*2 +

0 (ACFM) \*\*3

TABLE 35
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 9-10-76

TEST NUMBER 11

PART 22H

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF J4.3 MG
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 415
PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS NET DIFFERENTIAL PRESS \*\*\*\*\*\* PRESSURE TEMPERÄTURE FLOW RATE KG/SQ CM LITERS/ GN2 GN2 KG/SQ CM PSIA DEG. K DEG. C DEG. F MIN ACFM SCFM KG/HR LBS/HR DIFFERENTIAL PSID 29.447 418.8 301.6 28.4 83.i 48.9 .0621 1.727 7.497 32401 29.402 418.2 16.2227 \_\_ 230.741 301.6 28.4 83.1 43.5 0553 1.536 3.025 6,669 29.402 418.2 13.1157 186.550 301.6 28.4 83.1 38.5 .0490 1,361 2.680 5,908 ž9.356 417.5 2.031 8.6329 122.788 301.5 28.3 83.0 29.2 .0372 1.031 4.478 29.356 417.5 6.7465 95,958 28.3 82.9 .867 1.708 3.766 301.4 24.6 .0313 29.311 416.9 83.0 5\_12n9 72\_836 301.5 28.3 20-0 .0255 .705 1.388 3,060 29.311 416.9 3.0755 301.6 28.4 83.i 13.2 .0169 466 .91B 2.025 43,743 29.311 416,9 301.7 28.6 83.4 13.0 .0166 .459 .903 1,992 3.0206 42,963 416.9 29.311 28.5 5:1760 73,621 301.7 83.3 20.2 .0257 .712 1.402 3.090 29.265 416.2 301.6 28.4 .861 1.696 3.739 95,326 83.1 24.4 .0312 6.7021 124-682 29.219 415.6 .0378 301.4 28.2 8,58 29.5 1.043 2.053 4.526 8.7660 29.219 190,969 415.6 301.3 28.1 82.6 .0499 5.979 39.0 1.377 2.712 13.4264 29.219 27.9 415.6 301.1 82.3 42.8 .0548 2.979 6,568 228.216 1.513 16.0452 29.128 414.3 27.9 301.1 82.2 47.0 .0602 1.659 3.267 19.8623 282.508 7.203 \*\*\*\* \*\*\*\* \*\*\* \*\*\* \*\*\* 29.304 416.8 301.5 28.3 82.9 .067 1.0 .2 .2 DEVIATIONS .3

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PAGE: 1 DATE: 9-10-76

#### TABLE 36 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST -- UMBER 11

PART ?21

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 105.2 MG OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE - 1000 PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS

. FLO4 ETER COUNTITIONS	
· 特殊的特殊的现在分词的现在分词的现在分词的现在分词的现在分词的现在分词的现在分词的现在分词	

FLOWIATIER ONF			****	0kI P3T <u>5</u> H40J4 ********		
FLOW RATE	PRESSURE (PŠĪ <sub>A</sub> )	T:MP (DEG• F)	FLOW RATE	PRESSURE (RSIA)	TE 1P (DEG. F).	PRESSURE TEMP FLOV RATE
·-•88	45.9	76.7	• #5	47.5	6 at a 3%	1-11-2 - 78-6 0434
• <b>7</b> 8	50.2	74.0	• 14 ]	48.4	-14-6-3	1-11-9
-+69	àu•J	78 <u>.</u> 9	•71	48 <sub>*6</sub>	79•7	1-11*5
<u>*</u> 60	51.0	7**7	•ភិម	49+9	70.	1 11.0 77.6
•50	49.7	7₹.0	• <del>4</del> 9	48.8	79.7	1-11.9 77.+8
<b>.</b> 41	56.4	7?	•40	. 49.9	.o., a	1-11,9 78,0 ,0201
.32	49.7	76.8	.3U ·	49.2	*1	1.15,9 78,40151
<b>₽27</b>	49.9	77.2	.26	49.3	• 4	1-11.978.80130
22	49,9	78.4	+2]-			
- •15	58+5	79.6	• 1 <b>4</b>	.49.9	81.5	1.15.9 80.5
•15	50.2	83	•14	49.9	42.4	1-15.981.1
22.	១០ ១៩	₽3	20	50.3	. 61.9	1_15.981.1
•26	54.4	84.41	• 25	49.9	1.9	1-15-9 81-0 •0125
<u>•</u> 32	១៧.4	79.7	•31	49.9	81.8	1_15.980.8
.42	58+1	7d+9	•41	49.3	81.£	1_15_980_30202
•50	⊃v . 4	78 <u>+</u> 2	•4 <del>9</del>	49.5	S1 . 4	1.15.9 79.80244
<b>.</b> 60	50.2	77.2	.60	49.2	B 9	1 15.9 79.1
•69	50.2	75.9	•70	48.A	-560 <b>- ]</b>	. 1.11.9
78	50.2	75.4	•81	48.4	79.3	1 11.9 77.2
.87	50.1	74.4	,91	47.8	78 <sub>*</sub> 8	1-11,9 76,6
				3.1		3.



### TABLE 36 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 9-10-76

TEST MUMBER 11

ISS TRAS

TARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM) \*\*2 +

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 105.2 MG OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE. = -1000 PSIA (NOMINAL).

0 (ACFM) \*\*3

			aROSS	GR .SS			
PRESSURE (PSÎA)	AVG TEMP (DfG. F)	AVG FLOW R:TF ( ACFM)	DIFF. PRESS PRIMARY (PSID)	DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PS(L))	TARE OIFF	NET DIFFPRESS (PSID)
1011,9	78.6	. 434	168,453	68,453	168,453	-0,000	168.4 <del>5</del> 3
1011.9	78.1	. 385	143.232	143,232	143,232	-0.000	143,232
1011.9	77.8	. 341	121,479	121.479	121.479	-0,000	Ī21.480
1011.9	77.6	.n3.1	102,554	1 2.564	192,564	-0.000	102.564
1011.9	77.8	242	77.29	77.659	77.474	-0.000	77.474
1011.9	78.0	.0201	60,449	64.950	60.499	-0.000	60,700
1015.9	78.4	, 151	43,594	43.741	43.687	+0.000	43.687
1011.9	78.8	.013	36.471	36.182	36.126	-0.000	36.127
1015.9	79.7	•.1 5	27.796	27.846	27.826	-9.000	27.826
1015.9	44°±	.a .71	17,843	17.838	17.84.	<b>→0.000</b>	17.840
1015.9	81.1	. 10 71	17,785	17.952	17.868	-6.000	i7.869
1015.9	81.1	.81 5	27,622	27.799	27./11	-0.000	27.71i
1015.9	81.0	, 125	34,161	34,343	34.252	=0.000	34,252
1015.9	80.8	.8156	44.404	44.741	44.322	-0.000	44.323
1015.9	30.3	.02.2	61.075	61.580	61.328	-0.000	61,328
1015.9	79.8	. 244	77.538	77.974	77.756	-v.000	77.756
1015,9	79.1	. ~292	99,796	99.,96	99.196	-0.000	99.096
1011.9	78.0	.0341	121,164	121.164	121.164	-0.000	121.164
1011,2	77,2	.0385	143.863	143.863	143,863	-0.000	ĩ43.863'
1011.9	76,6	, 431	i70,029	170.029	170.029	=0.000	ī70,029

PAGE: 3 DATE: 9-10-76

NET DIFFERENTIAL! PRESS

#### TABLE 36 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST WIMBER 11 PART 221 TEST DESCRIPTION

TEST SPECIMEN INLFT CONDITIONS

101149

1913.9

2.0

297.9

\*\*\*

299.3

•7

24.8

26.1

.7

\*\*\*

76.6

70.0

1.2

\*\*

83.0

DEVIATIONS

44,431

2.930

5.770

71-144

71.283

•139

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 105.2 MG
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 1000
PSIA (NOMINAL).

PRESS						***	FLOW RATE	****	****	444#444		
- KG\20- €W	PSIA	DEG. K	HEG. C	056 F	LTTFRS/ HTN	+CFM	Sef#	K@∖HK Gws	GN2 	KG/SQ CM DIFFERENTIAL	PSĮD	
71+144	1011+9	299.1	- 25.9 -	- 78.6	- 83+3 -	434	2942	5.792	. 12.770	11.8434	_168. <del>4</del> 53	
71 • 144	1011.9	298.8	25.6	78.3	·· · 7-4 • 1	• 1-384-	2-618-	-5-156	11+366	<del>10+0702</del> -	<u>i</u> 43+535	
71-144	1911:9	298+6	2F+4	. 77.8	656.	341	2-315	4 <u>.</u> 55 <u>B</u>	10+P49	8.5409	<u>121.∳80</u> —	
71.144	1"11:9	298.5	25,3	77.6	57.9	•430}	2.043	4.023	8+869-	7+2110		
71.144	1-111-9	298.6	25∙4	77.8	46.5	•242	1.642	3.234	-7-+1-30	5+4470	77-474	
71-144	1511.9	298.7	ىئى،25	7.81 -	3A.5.	+4241	1.360	. 2.678	5.905	A-2676	<del></del>	
71.423	1015,9	299.3	25.5	78-4	29.1 .	151	1.027	2.022	4.459	3,0715	43-687	
<del>71 •</del> 144	1011,79	299.2	25- <del></del>	78,8		,134	879	- 1-730-		Z_5400·	36-127	
71,423	1015.9	2.99 <sub>-</sub> .6	- 24-2	79.7	20.2		712	1.40 <u>1</u>	3 <sub>+</sub> n9ŋ	1.9564	2 <b>7.</b> 826	
. 71,423	.1015.9	300.1	27 - 4	. 84.5.	13.7	071	484	952	2.100	1,2543	<u>17.840</u>	
71.423	1015.9	300.5	27.3	81.1	1347	•1071	483	.951	2.497	1.2563	<u>ī7.869</u>	
71.423 _	1015.9.	304.4	27.3	81,1	20.1	0105		. 1.396	3.079	1,9483	27.71117	
71.423	1015.9	300.4	27.2	<b>81.</b> a	_23.9	125	846	1.665	3,671	2,4082	34.252	
. 71.423	1015.9	300.2	27.1	80.8	. 29.9	<b>-1156</b>	1.055.	2.478	.4.582		65€+44	
Ž1 <u>4</u> 423	1015.9	300.0	.26.⊄	80.3		0202	1.373	2.703	5.959	4.3118	61.328	
71.423.	1015.9	299.7	26.0	79.8	46.9	244	1.656	3.261	.7.188	5.4668	77.756	
71.423	1315.9	299.3	26.1	79.1	56.3	292	1.987	3.912	8 • 625	6.9672	99.096	
71.144	1311•9	298.7	25.6	78.a.	65.4.		2+3p9	4.546	<u>i0•/22</u>	8.5187	121-164	
71+144	1-111-9	298.3	25+1	77.2	74-1	385	2+617	5.153	11.360	10-1146	143 <u>+</u> 863	

TABLE 37

FLOW PATE VERSUS DIFFERENTIAL PRESSURE

TEST UMPER 11

Les TRAG

TEST DESCRIPTION

PAGE: 1 DATE: 9-10-76

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 105.2 MG OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE. = 415 PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS

FLOW/ETCR CONDITIONS	
<del>你你你你你你你你你你你你你你你你你你你你你你你你你你你你你你你你你你你你</del>	

FLOWMETER ONF			***	FLOUMETER TWO				
FLOW RATE (ACEM)	PRESSURE (PSIA)	TEMP (DEG: F)	FLOW RATE (ACEM)	PRESSURF (PSIA)	TE .P (DEG. F).	PRESSURE	AVG- TEMP 	FLOW RATE
+51-	>0 • j	76	<b>+5</b> ±	49+2	71+9	419 <b>+5</b>	71+3	-+0600
•41	ხ•3	75	-41	49=7	73.49	418.2	71-3-	0493
+31	50.3	7. •6	+31	·49+9	7 <del>2</del>	418+2	71+3	+0371
.26	5v.3	7: •7	<b>,</b> ?5	49.9	72.2	417.5	71 <sub>4</sub> 4 -	
.21	46.8	70.9	*5n	49.5	72.3	417.5	-71-6	ρτ
.14.	49.9	71-)	.14	49.7	72,5	4-17 ¥5	<del></del>	<del></del>
.14	49.7	71.4	.13	49,3	72.B	417.5	72-1	
*55	±0,3	71.3	- •51 ~	49-9-	70 <u>.</u> B.	43745-	· -72-1	•0258
,27	, bu,1	71+2 -	<del>26.</del>	49 <b>-</b> 5	<del>7</del> 2.8	416-9-	<del>72.</del> ()	
,31	49.7	71+1	<b>.</b> 31	49.2	72.9	416.9	7 <del>2</del> -0	0368
•41	bu+3	79	• 41	49 • 5	7 <b>~•7</b>	416#2	71+8	
50	50.5	71+4	. +5u	· 49+5	72.5	415.6	<del>71.7</del> _	

TABLE 37
\* FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION

USS THE

PAGE: 2 DATE: 9-10-76

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSIBE. TOTAL OF 105.2 MG OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 022) INLET PRESSURE = 415 PSIA (NOMINAL).

TEST SPECIMEN INLET CONSTIT NS

TEST . UNREA II

PRESSURE (PŠÍA)	AVG Temp (Deg. f)	.VG FLAJ ≋ATF ( C°·)	ARGSS DIFF. ARESS PRIMARY (PSI))	#R SS DIFF. PRESS SECO4DyRY (PSI))	.VG GR SS DIFF. PRESS (PSI:)	TARE DIFF+ PRESS_ (PSID)	NET DIFF+-PRESS (PSID)
419.6	71.3	4.16 B	290.81.	291, 410	290. 11	.000	290,809
418.2	71.3	. 493	192,713	192./13	192.713	•000	192,712
418.2	71.3	. 371	124,673	124, 178	124,678	.000	124,678
417,5	71.4	. :31	96.510	90.515	96.515	•000	96.514
417.5	71.0	. 245	7 .665	71.516	71. 91	• 0 0 0	71.090
417.5	71.8	166	43.761	43.91	43.836	•00a	43.835
417.5	72.1	. 164	43,355	43.504	43.459	-0.000	43.459
417,5	72.1	. 258	75.159	75.946	75,553	•000	75,552
416.9	72.1	. 31.	130,312	167,312	107.312	•000	100,312
416.9	72.	. 368	123,412	123,412	123,412	•000	123,412
416.2	71.8	. 492	193.729	193. 29	193. 129	•000	193.029
415.6	71.7	.06 4	3. 5.835	3 .2.835	302,835	.000	302,834

ARE DIFF. PRESS = -3.4 000E-05 + -4.4400 E-14 (ACF) + 1.50933E-01 (ACF) #82 + 0 (ACFM) ##3

ORIGINAL' PAGE IS

# TABLE 37 FLO' RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3. . DATE: 9-10-76

TEST WUMBER 11 PART SPJ

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 105.2 MG
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 022) INLET PRESSURE = 415
PSIA (NOMINAL).

204555554444	***	***	AS TEAL Babbbbbbbbbb		olTinhoo T.		5000000000000	******	******	NET DIFFEREN	TIAL PRESS	
PRESSU		TEYPER \TURE			FLOY					<u> </u>		
KG/SQ CM.	PSIA	DEG• K	n∈G• C -	DEG. F.	LITTES/	eF4	Sef-M	<b>Κ@\H</b> Κ	 	KG/SQ CM	PSID	
29+493	419.5	295	21 • ¤	71-3	48-4	•641-	1.7.48	3+362	7+412 -		290+ <u>809</u>	
29+402	418:2	295	2] +8	71.7	34+6	·+493	- 1+398-	2•753 .	- 5+469	13+5490	<del>192+712</del>	
29-402	418.2	295+#	21*5	-7 h-3	-29+8-	371	1+054	275	4-575	8.7657	124.678	
29+356	417.5	295.1	21.9	71.4	24.9	•31	<b>₽878</b>	1.729	3.812	- 6.7856	96-514	
29,356	417:5	295.1	55.	71.5	19.7	•246	.697	1.372	3+424 .	- 4.9981	<b>71-090</b>	
2 <del>9+</del> 356	417.5	295.3	22+1	71-3	13+3	1706	+479	ئۈچە	2+A38	3+0819	43.835	
29.356	417-5	295.4	22.4	72.1	14.1	164	.464	•913	2.413		43.459	
29,356	417.5	295,4	55.3	72.1	2a•1.	,.,25 <u>4</u> .	,73.	1-2438	3-1.79	5,3118	75,552	
. 29,311	416.9	295.4	22-2	72-1	25,4	315		1.768	3,898	7_0526	100,312	
29,311	416.7	295,4	22.2	72,.1	29.4	36P	. 1 <u>.</u> n39	2.45	4,509	<u> 8,6767</u>	123,512	
29,265	416.2	295,3	22.1	71.3	39.3	•492	1.388	2.734	6.527	-13.5713	193,029	
29,219	415.6 ****	295 <sub>*</sub> 2	22.1	71 ******	48.2	. عيفليد .	1.72.	3 <sub>4</sub> 35 <u>1</u>	7.387	21,2914	3n2 <u>,834</u>	
29,349	417.4	295,2	22.1	71.7							* <del>***</del>	
i , •048	+]	.1	•1	.3	UFVI-TION	vs -	3.5			-		

The second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of th

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PAGE: 1 DATE: 9-15-76

TABLE 38 FLOW RATE VLASUS DIFFERENTIAL PRESSURE CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAM) AFTER THE ADDITION OF 5.2 MG OF 설션 PEST DESCRIPTION SYNTHETIC CONTAMINANT AND AFTER 2 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST TOST WUMPER 12. PART 28F SPECIMEN (S/N 028) INLET PRESSURE = 1000 PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS FLOUMETER CONSTITIONS \*\*\*\*\*\*\*\*\* FLOWM: TER ON: FLOWMETER TWO AÝĠ: FLOW RATE FLOW BATE FLOW RATE PRESSURE (PSIA) PRESSURE TE\*IP TIPING TEMP (DÉG. F) (ACFM) (DEG\_ F) (DÉG. F) . 84 49.7 54.6 . .94 . 7 . 6 09.6 1-11.9 .0420 .76 DU . 4 48.5 68.9 1:11.9 66.3 .0382 63.8 67 50.2 63.1 44.7 58.4 1 11.9 65.7 0334 0290 .58 2.50 1 11.9 . .65 .6. 53.7 . 5v 49.1 58.1 .0246 .49 63-1 65.5 20.6 - 50 49.7 n8. 1 1 11.9 0198 20.2 . . . **.** .4V. 9.5 1 11.9 \_\_\_65.7 40 63,3 68.1 0150 .30 DL 4 63.9 .... 32 49.9 63.5 1.11.9. ... 66.2... 1011.9 .012Ť 54.2 66.5 • 26 64.3 49.9 68.7 .21 56.2 49.9 59.5 5 .. . 0 .14 1.07.9. ... .00.69 50.4 00.1 69.4 8.76 ļŀ 68.3 0069 .14 56.5 49.9 1,11.9 65.6 70.0 66.5 .0108 . 22 5i.4 09.9 1,111.9 68.2 50.1 0127 . 26 96,4 49.9 59.9 1:11.9 \_\_\_\_\_68.1 18 .0151 .30 ·30 \_ 1.11.9 67.9 ⊅t.6 , 65.9 50.1 69.8 • 40 54.4 55-1 49.9 •0199° 59.4 • 49 D11 - 4 64:3 .. ... t.5u.... 49.5 59 · 1 . 1007. 9 .... .0245 .0286 • 58 49.9 63.7 - 60 48.5 5R.6 1007.9 66 • 1 .... • 67 49.7 \_. 7.1 1207.9.... \_\_\_65.2\_\_\_ ...0335: . 62.7 48.3 57.8 • 75 49.7 63.0 • 80 47.8 c7•1 1007.9 Į, 87 49.7 1007.9.\_\_\_\_63.9 61.3 47.4 06.4 

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TABLE 38
FLOW PATE VENEUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 9-15-76

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CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL
PRESSURE. DATA ACQUIRED IN THE NORMAL FLOW DIRECTION
(S/N SIDE UPSTREAM) AFTER THE ADDITION OF 5.2 MG OF
SYNTHETIC CONTAMINANT AND AFTER 2 HIGH PRESSURE
(10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST
SPECIMEN (S/N 028) INLET PRESSURE = 1000 PSIA (NOMINAL).

1501 SECTION INCEL CONDITIONS	
格拉格特特特特特特特特特特特特特特特特特特特特特特特特特特特特特特特特特特特特	作計
•	4

PRESSURE (PŠĪA)	АУ Э (ЕМР (DEG• F)	AVG FLOW PATE (ACFM)	ARDSS DIFF• PRESS PRI4ARY (PSIU)	GR SS DIFF. PRESS SECTODAPY (PSIO)	AVG GRUŠS DIFF: PRESS (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)	
1011 • 9	07.1	• j42.	151.615	151.0.3	151,618	<b>~</b> 9∗000	151+618	
1011.9	26 <b>,</b> ∃	* 385	133,941	133, 41	133, 41	-0.000	133,942	
1011,9	75.7	. 1934	112,477	112,+77	112,477	-0.000	112,477	'
1011.9	25.6	4597	94,169	94,.59	94,169	-0.000	94,170	55
1011.9	∾5,೮	. 1245	75,283	76,493	76,390	<b>~0.000</b>	76,390	٠
1011,9	75,7	. 199	\$ <b>7</b> _947	55,5 1	58,244	-0.000	58,244	
1011.9	66.5	, "1 <sup>5</sup> "	42,122	42, C7	42,195	-0.000	42,105	
1011.9	66.3	. 12,	34,415	34,574	34,49	₩0.000 °	34,491	-
1011.9	56.9	- 11: 2	26.353	20.394	26,376	-0.000	26.379	
1007.9	77.~	69	16,435	12.5.7	16.491	=0 • 0 0 0	16,491	
1011.9	5d.3	لاه. ق∙	16.339	10.413	16,376	<b>~</b> 0.000	16.376	 
1011,9	\$6.5	.41 4	22.043	26.175	28.109	-0.000	28.110	"
1011.9	98 <b>-</b> [	. 127 -	33.953	34.161	34. 57	-0.000	34.057	
1011•9	67.9		41,949	42. 4.7	42.018	-0.000	42.018	1413
1007.9	57.7	. 1 <sup>99</sup>	<b>47.861</b>	59.195	58. 23	<b>~</b> 0.000 ~	58.023	j <sub>0</sub>
1007,9	66.7	. 245	75,285	75,546	75.415	-0.000	75,416	-
1007_9	°5,1	. 284	92,275	97,215	92,275	-0,000	92,276	-
1007.9	n <b>5</b> .2	335	111,340	111,346	111,046	-0.000	111.846	į
1007.9	· + • (·	•378	129,031	129,538	129,338	20.000	129,838	
1007.9	93 <b>.</b> 9	, 42u	15 ,355	15 ,355	150,355	-0.000	150,356	

IARE DIFF. PRESS = -1.64000E-04 + -1.2693.E-..2 (ACFM) + 2.48070E-01 (ACFM) #2 +

PAGE: 3. DATE: 9-15-76

FLOW H. TH VENSUS DIFFERENTIAL PRESSURE

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TEST SPECIAEN INLET CO NITIONS SEECUMEN (S/N UZO) INL

	PRESS	<u>URE</u>		IE				FLOW RATE	,	1	- 1-1-1 0 names or or took or or to product or
	*****		******	****	***	LITENS/	****	*****	۵۳ <sub>۰</sub> دری	GNZ	KG/SQ CM
	KG/SQ CM	PSIA	DEG* K	LEV. Q	DEG, F	IN	4CFA	SCFM	ĸ∂∖ӈӵ	LBS/HR	DIFFERENTIAL: PSAD
	71:144	1011:7	292.7	19.4	67.1	₹, ۲۰	a 10 6 st	2.967	5.724	12.620	10.6598 151.618
	71.144	1011:3	292.2	19.1	66.3	7	. 3H.,	2,648	5.415	11.496	9.4170 133.942
)	71.144	1011.5	?91,9	18.7	۰ .7	5° •7	. 334	2,321	4 <u>.</u> 570	10.374	7.9080
	71•144	4ء.1ء ( 1	291.5	13.6	b≤.5	7.9	٠,٤٥.	2.:14	3.965	8.742	6,6208 94,170
	71.144	1::11.9	291,6	13.5	65.5	44.4	. 24	1.71	3.367	7.422	5.3707 76.390
	71 <u>•</u> 144	1011,5	291,4	\B•/	55,7	34.6	• .1 <sup>96</sup>	1.372	5*[0]	5 <u>•</u> 956	4.0950 58.244
	71.144	1011,7	292,2	10.	66.2	<sup>J4</sup> +5	alsi	1.063	2,754	4+529	2.9603 42.105
	71:144	1011.7	292.3	19.4	66.5		127	.881	1.735	3 456	2.4249 34.491
	71.144	lu11.5	292	19.4	76.9	c •1	• 21, 2	.7:9	1:397	3•080.	.1.8546 26.379
	70.865	1.07.5	292.9	્વ . હ	67.0	13+h	. 469	.477	•939	2.069	1,1595 16,491
3.	71:144	1011.05	293.3	2 • 2	58.3	13.4	• 0.14	.474	<u>•934</u>	2•059	1.1514 <u>16.376</u>
	71,144	1'11.7	293,3	2_+1	5.80	21.2	• 1 <sup>3</sup>	.748	1.473	3,248	1,9763 28,110
	71:144	101129	293.2	2. •1	26+1	24.8	• 12/	.875	1.722	3.797	2.3945 34.057
ij	71,144	1011,5	293.1	10.8	67.9	5 و م	151	1.041	2.050	4,520	2.9542 42.018
	70.865	7401.A	292.3	19.8	67.3	9. د د	• 199	1.373	2:703	5.959	4,0795 58,023
	70 865	1907,9	392.1	12.3	06.7	412.	. ,24"	1.694	3,335	7,352	5.3022 75.416
	70 • 865	1.:07.7	292.1	19.	05.1	n • ∞	. 210	1.978	3.594	8.586	6.4876 92.276
	70.865	1 107.9	د <b>.</b> الاد	18.5	65.2	54.6	. 334	5 <b>*</b> 319	4 • ភិទ្ធភ	10,764	7,8636 111,846
	70 <u>.</u> 865	1007.9	291.3	14,1	ចុង ្	73,5	.0376	2,607	5,134	11,318	9.1285 129.838
ł	70 865	1607.ម *####	19 , c	17.7 *****	###### 63°3	٠4. ٠	1424	2,973	5 • 454	12,907	10,5711 150,356
	71,046	1010.5	292,3	19.8	66.5						
	.127	1,6	.5	• •	1,4	DEVIATIONS	s				

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TABLE 39
FLOW RATE VERSUS NIFFERENTIAL PRESSURE

PAGE: 1 DATE: 9-15-76

TEST UMPER 12

PART 296

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. DATA ACQUIRED IN THE NORMAL FLOW DIRECTION

(\$\int \text{SIDE} UPSTREAM) AFTER THE ADDITION OF 5.2 MG OF

SYNTHETIC CONTAMINANT AND AFTER 2 HIGH PRESSURE (10,000 PSIA NOMINAL) GN\_2 IMPACT CYCLES. TEST SPECIMEN (\$\int \text{OND} 028)

INLET PRESSURE = 415 PSIA (NOMINAL).

TEST \$\int \text{CIMEN INLET CONDITIONS}

ELOW TIFR CONDITIONS \*\*\*\*\*\*

	FLOWMETER ONE		****	你你你你好你你你你	F_0.89ETER T40 \$444&\$\$44&\$\$		•			
	FLOW RATE	(Lāīv) bkāpānga	TEMP (UEG+ F)	FLOW RATE (QCFM)	Pressure (PSI.4)	TEMP (DEG. F)	PRESSURE (PSIA)	TEMP FLOW RATE	•	
	<u>•</u> 50	51.4	7: .7	, •వ్∪	49.5	72.)	414.3	.71.4		
	<u>.</u> 40	50.4	7 6	•41)	+9+9	72.1	413.7	71.30490		
Ľ	<u>.</u> 30	ងូប•ស	7 -7	•30	43.1	72.2	413.7	71*4 +03691	UL	
	<u>•</u> 26	47.7	1.7	.26	4 +	25.2	413.0	71.4		
	<u>.</u> 21	à^•5	7.*8	.21	49.9	£.3	413.0	. 71-50247	-	
	<u>.14</u>	50.2	7 🛂	• 1 4	49 • 9	12.4	413	71.7 .0168.		
	<u>.14</u>	4à•à	71 + 1	•14	49.5	12.6	413.0	71.8	_	
	•,21	ο <b>γ.</b> 1	71+0	-51	49.7	72.6	412.4	71.80256		
	-Sé	20.1	Zi +b	. 25	49.7	72.4	412.4	.71.6		
	<u>.</u> 31	511.4	7 • •	.31	49,9	12,3	411.7	71.4		
<u>l</u>	<u>.</u> 40	₽안•≥	7, +3	•4∉	49.5	72.2	411.1.	71.2	 N	
	•49	50.2	7.52	, nu	49.1	71.9	410.4			
	,									

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PAGE: 2 DATE: 9-15-76

TABLE 39

TABLE 39

FLOV RATE VANGS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAM) AFTER THE ADDITION OF 5.2 MG OF SYNTHETIC CONTAMINANT AND AFTER 2 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST SPECIMEN (S/N 028) INLET PRESSURE = 415 PSIA (NOMINAL). TTOT UPRER 12

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PRESSUKE (PŜĨĄ)	AVG ፲EMP (ብርር• F)	FLUM FATE	SEORA PRIMARY (Cley)	GR LSS DIFF. PRESS SEC'N DARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF: PRESS (PSID)	NET DIFF. PRESS (PSID)
414.4	71.4	• i 693	259.46n	459,455	259.466	• 0 0 0	259,465
413 <u>.</u> /	/1:3	• 14 <sup>11</sup> +	174.24	174.24.	174.24.	• 6 0 0	174.239
413,7	(1.4	. 3-9	114.26	114.2~6	114.266	•000	114.265
4]3 <u>.</u> 0	(1.4	. 311	94. 11 <sup>54</sup>	9: 492	90.326	• 0 0 0	90.319
<b>41</b> 3 <u>∗</u> d	11.5	. 247	56, 12	66.247	66•149	-000	66.149
413 <u>•</u> a	11:7	. 168	4 .96%	41.235	41. 99	•000	41.099
413.0	11.9	2 (127	49 <b>,</b> 59.	44.715	4() <u>,</u> ñgd	.000	40,607
412 <u>.</u> 4	71.4	, 265	69,395	69,759	69,578	.000	69.577
412.4	(1,6	_u3 3	49 427	69,445	89 <b>.</b> 534	•000	89,533
411.1	(1.4	, 374	117,422	117:422	117.422	• 0 0 0	117,422
411.1	(1.2	. 469	175,187	374.157	175.187	.600	175,186
410 * 4	71**	.06 0	2-9.741	2-9,7"	259.781	•000	259.781

160E DIFF. r:F65 = -3.4:000E-J5 + -4.4400JE-04 (ACF4) + 1.50933E-01 (ACF.)\*\*Z + 0 (ACFM) ##3

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TABLE 39 FLOT A TE VENSUS MIFFENENTI & PRESSURE PAGE: 3 DATE: 9-15-76

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CONTAMINATED CONDITION - FLOW RATE VERSUS\_DIFFERENTIAL . . PRESSURE. DATA ACQUIRED IN THE NORMAL FLOW DIRECTION TEST DESCRIPTION (S/N SIDE UPSTREAM) AFTER THE ADDITION OF 5.2 MG OF SYNTHETIC CONTAMINANT AND AFTER 2 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES, TEST SPECIMEN (S/N 028) INLET PRESSURE = 415 PSIA NET DIFFERENTIAL PRESS 

TEST SPECIMEN INLET CO MITIONS

FLOW A.TE PARTOR AND TO A TURE PRESSURE KÁ/SQ CM GN2 LITTAS/ 3445 ¢F^ DIEFERENTIAL. \_ PSID. ScFm Ku/HR LUS/HR KG/SQ CM PS1. × ∑ivi JEG. C 016. F 11:5. N 18.2422 259.465 1.644 3.330 7,354 29.128 414.5 295. 21.5 71.4 6000 . 0.3 12.2502 \_\_\_\_174.239 1.375 2.707 5.967 413.1 295, 21.5 32.9 . 47 29.083 71.3 4,492 0.0337 .114.265. 2...35 71,4 · JAY 1.035 29.083 +13.1 21.9 6.40 295.1 6.3501. 90+319 1.714 3./79 .871 415. 21.9 71.4 . 311 29.037 292.1 crol 4.6507 66,149 ر 36 و ر 3.405 . 17.1 692 295.1 72. 71.3 19.5 29.037 413... 2,8895 41,099 928 .472 2.,47 71.7 17.4 · 154 29.037 413.0 295.7 ?2.1 .921 2,,31 2,8550 40.607 71.4 458 29.037 413. 295.3 22.1 13.2 . .147 4,8918 69,577 . . 2 " 0 3,134 4...2 .715 1.400 28,992 412.4 295,3 22.1 71." 1.596 6.2948 89.533 3.740 28.992 412.4 295.2 71.5 4.4 . 13. ' 962 2. . 117.422 8,2556 4.537 28,946 . 3/4 1.045 2.055 411.1 295.1 41.7 71.4 15.0 175.186 2.080 5.922 12.3168 28,900 295. 21.0 71.2 3.00 . 407 1.364 411.1 , ,,61 , 259,781 71. "7.3 1,6/1 3,290 7.254 18.2644 28,855 410.4 294. 61.1 \*\*\* \*\*\*\* 计特许条件 动外外外外体 \*\*\* 29:011 412.3 1+295 21.5 71,. 31 ., . ? JUVITIONS .061 . 1 4 1

PAGE: 1 DATE: 9-15-76

TEST NUMBER 12

TABLE 40

GONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAM) AFTER THE ADDITION OF 5.2 MG OF SYNTHETIC CONTAMINANT
AND AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT

PART 281

TEST DESCRIPTION CYCLES. TEST SPECIMEN (S/N 028) INLET PRESSURE = 1000 PSIA

(NOMINAL).

	***	***		CONDITIONS	***	TEST SPECIMEN INLET CONDITIONS			
ıf.	****	FLOWME!ER ONE	***	*****	FLOWMETER TWO	***			
ń	ELOW RATE	PRESSURE (PSTA)	TFMP (DEG_ F)	FLOW RATE (ACEM)	PRESSURE (PSIA)	TEMP (DEG. F)	PRESSURE	AVG TEMP (DEG F)	FLOW RATE (ACEM)
	•86	47.9	55 <u>•</u> 8	•91	47.6	61.6	1007.9	58.7	•0427
	• 76	50 <u>.</u> 1	55 <u>.</u> 2	•81	48.3	60,8	1007.9	58.0	•0385
	<u>•</u> 67	aû•1	54:9	.70	48.5	60.5	1007.9	57.7	• 0335
	<u>.</u> 58	>៎∩ • ឱ	55•0	.60	49.5	60.5	1007.9	57.7	.0295
h	<u>.</u> 49	<b>9</b> φ.4	55 <u>.</u> 4	• <b>5</b> 0	49,5	60.7	1007.9	58 <sub>+</sub> 0	.0246
	.40	• • 4	56 <u>•</u> 0	• 40	49,7	61.0	1007.9	58 <sub>1</sub> 5	•0já <u>@</u> "
	•30	⊅ų•1	56,5	•30	49.5	61.3	1007.9	58 <b>. 9</b>	-0147
	.26	42.7	57 <u>•</u> 0	• 25	49.3	61.6	1007.9	59.3	•0125
	•21	49.7	57 <u>•</u> 5	• 20	49.3	62•0	1007.9	59.8	±0101 _
	<u>.</u> 14	⊃u•4	58.6	•13	50•2	62.7	1007.9	60+6	•0067
ĺ	<u>. 1</u> 4	5 <b>0.</b> 4	60.1	,1 <sub>3</sub>	50+2	6346	1007.9	61,9	.0067
	<u>.</u> 21	49.9	60 <u>•</u> 3	•21	49.5	63,7	1007.9	62.0	0104
	<u>.</u> 25	49.7	60:1	• 25	49•3	63.8	1007.9	62:0	•0122
	<u>.31</u>	ង់សី <sup>*</sup> រ៉ូ	59 <u>•</u> 9	•30	49 <u>•</u> 5	63 <sub>4</sub> 7	1007.9	61,8	.0150
	<u>• 40</u>		59 <u>•</u> 1	• 40	49.5	63,4	1007.9	61 <u>.3</u>	.019B
	•49	20.5	58 <u>.</u> 1	• 50	49.3	63.0	1007.9	60•€	•0\$46
1	<u>.</u> 58	àû•Ï	57 <u>∗</u> 5	•60	48 <u>.</u> 9	62 <u>.</u> 5	1007.9	<b>60</b> •0	• 0530
	<u>•67</u>	49.9	56 <u>•</u> 8	•71	48•5	61.9	1007.9	59+3	•0337
	• <u>7</u> 6	àñ∓J	56.1	<u>•</u> 8Ì	48 <u>•</u> 3	61.3	1007.9	58 <u>.</u> 7	•0385
	<u>.87</u>	50.4	55 <u>.</u> 4	•9j	48.3	60.5	1007.9	57,9	<b>,</b> 0435

PAGE: 2 DATE: 9-15-76

(NOMINAL).

TABLE 40

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE

DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAM) AFTER THE ADDITION OF 5.2 MG OF SYNTHETIC CONTAMINANT
AND AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE TEST DESCRIPTIONCYCLES. TEST SPECIMEN (S/N 028) INLET PRESSURE = 1000 PSTA

TEST NUMBER 12

PART 28I

TEST SPECIMEN INLET CONDITIONS

PRESSUKE (PSTA)	AVG LEMP (DÊÇ. F)	AVG FLOW RATE (ACFM)	GROSS DIFF∳ PRESS PRĬMARY (PSID)	GROSS DIFF• PRESS SĒCONDARY (PSID)	AVG GROSS OIFF PRESS (PSID)	TARE DIFF• PRESS (PSID)	NET DIFF• PRESS (PSID)
1007.9	- 58.7	•0427	119.044	119•044	119•044	<b>~0.00</b> 0	119 <u>-</u> 044
1007.2	58 <u>.</u> 0	.0382	104.506	104.506	104.506	-0.000	104,506
1007:5	5 <u>7.</u> 7	• 0335	88.200	88.704	88.452	70.000	68 <u>•</u> 452
1007.9	57 <u>.</u> 7	.0295	74.543	74.798	74.670	-0.000	74.670
1007.9	58.0	.0246	59.232	59.627	59.429	<b>~0 • 0 0 0</b>	59.430
1007.7	58 <u>.</u> 5	.0198	44.863	45.089	44.976	-0.000	44.976
1007.9	58 <u>.</u> 9	.0147	31.172	31,283	31.558	-0.000	31.228
1007.9	59.3	.0125	25,719	25,756	25.738	-0.000	25,738
1007.9	59.8	.0101	19.686	19,665	19.675	-0.000	19,676
1007.7	60.6	.0067	12,028	12.040	12.034	-0.000	12.ó34
1001.7	<u>61.9</u>	.0067	11.912	12.040	11,976	-0.000	11.976
1007.9	ē\$*0	-0104	20.266	20.412	20.339	<b>~0 • 0 0 0</b>	20+339
1007.9	ęŝ∓o	•0155	24.849	25.009	24.929	•0•000	24.929 <sup></sup>
1007:9	õÍ∓B	•0150	31,984	32.147	32.066	<b>-0.000</b>	32,066
1007.9	<u>61.</u> 3	.0198	44 863	44,773	44.818	-0.000	44.8 <u>18</u>
1007.9	_ <del>6</del> 0•6	.0246	58,980	58,995	58.988	<b>♥</b> 0 • 0 0 Õ	58.988
1007.9	ĕ0°0	.0290	73,038	72.901	72,970	-0.000	72.976
1007.9	<b>25</b> •3	.0337	89,076	89.020	89.048	<b>~</b> 0.000	89.048
1007.9	5 <u>8</u> .7	0382	Ĩ04 <b>,</b> 190	104.190	104.190	-0.000	104.190
1007 <del>. y</del>	57 <u>.</u> 9	.0435	122,837	122.837	122,837	<b>₩0</b> .000	122.837

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PAGE: 3 DATE: 9-15-76

TABLE 40

FLOW RATE VERSUS DIFFERENTIAL PRESSURE
DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAM) AFTER THE ADDITION OF 5.2 MG OF SYNTHETIC CONTAMINANT AND AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT (NOMINAL).

NET DIFFERENTIAL PRESS

TEST NUMBER 12

TEST SPECIMEN INLET CONDITIONS

	***	***	***	***	***	*****	****	***	***	***	******	****
,	PRESSI	****	****	TEMPERATURE	*****	*****	FLOW RATE					
	KG/SG CM	PS1 <sub>A</sub>	DEG. K	DEG. C	DEG. F	LITERS/ MIN	ACFM	sç <u>F</u> м	<u>кё\н</u> й ёи5	ĞN2 LBŞ∕ḤR	KG/SO CH DIFFERENTI	A <u>L, PSI</u> D, :
	70.865	100725	588.0	14.8	58.7	84 <u>.</u> 7	.0427	2. <sup>99</sup> 2	2 <b>∙</b> 885	12.990	8,3696	119.044
	70.665	100729	287.6	14.4	ŞB <sub>▼0</sub>	75 <u>.</u> 8	°0385	2.677	Ş•Ş7ļ,	11.620	7,3475	104-506
	70 <u>.86</u> 5	1007.5	287.4	14.3	57.7	66.6	• 0335	2.352	4.632	10-211	6.2188	88.452
	70 <sub>2</sub> 865	1007.5	287.5	14.3	<b>57.</b> 7	58 <u>.</u> 6	.0295	2.068	4 <u>•</u> 074	8.979	5.2499	74.670
	70.865	1007.7	287.6	14.5	58.0	48 <u>.</u> 9	.0246	1.727	3 <u>.4</u> 00	7 <u>.</u> 496	4.1783	59.430
	70.865	1007.2	287.9	14.7	58,5	39•3	•01 <sup>98</sup>	1.387	2.730	6.019	3,1622	44.976
	70 <u>.86</u> 5	1007:2	288 <b>.</b> 1	14.9	58,9	39 <b>∙</b> 5	<u>•</u> 0147	1.032	2 <u>.</u> 034	4.480	2,1955	31.220
	70.865	1007.5	288 <b>.</b> 3	15 <b>.</b> 2	59,3	24 <u>.</u> 8	•0125	.874	1.721	3.795	1.8095	25 <b>.</b> 738
	70.865	1007.4	288.6	15 <u>.4</u>	59.8	20.0	•0101	•70g	1.394	3.072	1.3833	19,676
	70 <u>.86</u> 5	1007.2	289.1	15.9	60.6	13.2	0067	466	21!	5.022	.8461	12.034
	70.865	1007-8	285 • 8	16.5	<u>61.9</u>	13 <u>.</u> 2	.0067	<b>.</b> 465	•915	2.017	- <u>B</u> 420	11 <u>.</u> 276
	.70 <u>.86</u> 5	1007-8	289.8	16.7	62.0	. 20 <u>•</u> 4	.0104	. <b>,</b> 722	1.422	3-134	1.4300.	20.339
	70 <u>.86</u> 5	1007.3	588.8	16 <u>.6</u>	<u>6</u> 2.0	24 <u>.</u> 1	.0122	849	1,673	3 <u>.688</u>	1.7527	24. 929
	70.865	100 <u>7.5</u>	289.7	16.5	<b>€</b> 1•8	29.€	•0 <sub>1</sub> 50	1.046	5•0e <sup>7</sup>	4.543	2.2545	32.066
	70 <u>.86</u> 5	1007.X	289.4	16,3	61.3	39,0	•0198	1.377	2.711	5.977	3,1510	44,818
	70 <u>• 86</u> 5	1007:3	289.0	15.9	60.6	48.6	.0246	1.718	3•382	7.456	4.1473	58.288
	70.865	100758	288.7	15•5	<b>€0 • 0</b>	57 <u>•</u> 3	•0290	\$ • 0 \$ 3	3.984	8.783	5 <u>•</u> 1303	Ţ <b>2•</b> ŽŽŌ ,
	70.865	1007.5	588*3	15•\$	<b>59</b> •3	66.8	•0337	2.358	4.643	10±236	6• <u>2</u> 607_	89.048
	70.865	1007-8	288.0	14 <u>•</u> ₿	58.7	75 <u>.</u> 7	<u>•</u> 0382	2.673	5•॒263	11.603	7.3253	104 <u>-1</u> 90
	70 <u>+865</u>	1007.9	. 287 <u>•</u> 6	14•4 ******	57 • 9	86•4	<u>*</u> 0435	3.050	6.005	13:240	8• <u>636</u> 3	1224837
	70 • 865	1007.9	288.5	15.4	59.6							
	• 000		•7	•7	i.3	DEVIATIONS						

PAGE: 1 DATE: 9-15-76

### TABLE 41 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREA )

AFTER THE ADDITION OF 5.2 MG OF SYNTHETIC CONTAMINANT AND

AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT

CYCLES, TEST SPECIMEN (S/N 028) INLET PRESSURE = 415 PSIA (NOMINAL).

TEST NUMBER 12 PART 28J

FLOWMETER CONDITIONS

TEST SPECIMEN INLET CONDITIONS \*\*\* \*\*\*\*\*\*\*

							•		- ***	
1	****	FLOWNGIER ONE	****	***	FLOAMEIER TWO	****			•	
·	FLOW RATE	PRLABURE (PSIA)	TEMP (DEG. F)	FLOW RATE (ACEM)	PRESSURE (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	FLOW RATE (ACFM)	
	•5 <sup>9</sup>	၁့ပု • 4	69:1	•61	4 <sup>9</sup> •3	69.8	414.8	69.5	*0 <sup>7</sup> 18	
	<u>.</u> 50	<b>5</b> 0 • 8	69:1	•50	49.9	69.9	414•2	69•5	<u>•0606</u>	
	<u>.</u> 40	ភ្នំព័ • 4	64.S	• 40	49•9	70 • J	413.5	69.6	<u>•048</u> 7	
	•31	āñ•S	69•4	•31	49.9	70.0	413.5	69.8	.0374	
I	<u>•</u> 26	49.9	69.7	<b>+ 25</b>	49.5	7c.4	413.5	70 <u>•</u> 0	•0307	
	<u>.</u> 21	, sh*T	69.9	•20	49.9	70.6	413.5	70.2	.0250	
	•14	50.1	73:2	•13	49.9	74.8	413.5	70.5	•0165	
	<u>•</u> 14	49.9	7c+7	•13	49,5	71.2	413.5	70.9	•01 <u>6</u> 3	
	•s1	49.7	70 <u>.</u> 6	.21	49.3	71.2	413.5	70.9	.0251	
	• 26	24.5	75+6	• 25	49.9	71.2	413.5	70.9	•0309	
43	<u>.</u> 31	₽Ų.1	70.6	.31	49.5	71.3	412.9	70.9	.0371	
	.41	50.2	70 <u>.</u> 4	. 41	49.5	71.4	412.9	70.9	.0491	
	•50	5ù•1	7a <u>•</u> 3	+50	49.2	71.3	412.2	70.8	+0601	
	•60	ភិព៌∙ e	7 <u>u±</u> 4	• 60	49.3	71.3	411.6	70-8	<u>•</u> 0725	

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PAGE: 2 DATE: 9-15-76

#### TABLE 41 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 12 PART 28J

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAL.) AFTER THE ADDITION OF 5.2 MG OF SYNTHETIC CONTAMINANT AND AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST SPECIMEN (S/N 028) INLET PRESSURE - 415.PSIA (NOMINAL).

. - .

# TEST SPECIMEN INLET CONDITIONS

a	PRESSUKE (PŠĪA)	AVG (EMP (Dig. F)	AVG FLOW RATE (ACFM)	GROSS DIFF. PRESS PRIMARY (PSID)	GROSS DIFF. PRESS SECONDARY (PSID)	AVG GRUSS DIFE. PRESS (PSIQ)	TARE UIFF PRESS (PSID)	NET DIFF• PRESS (PSID)
•	414.0	69.5	•n718	266.831	266.d31	266.831	.001	266.830
	414.2	69 5	• 96 96	185.393	185.393	185+393	•000	185.392
	413.5	o9•6	•9487	129.838	129+838	129.838	•000	129•837
	413.55	69.8	• 9374	89.505	89.435	89 • 47 J	•000	89.469
a	413 <u>.</u> 5	10:0	-0347	68,853	69.233	69 - ( 43	-000	69•042
	413.5	10:2	• 0250	51.668	52.188	51.920	•000	51.927
	4 j. j. 5	/0.5	.0165	30,998	31., 72	31.035	-0.000	31.034
	413 <u>.</u> 5	10.9	.9163	30,650	3),899	30.774	-0,000	30,774
	413°2	10.9	.4251	52,798	53,135	52 <b>.</b> 96 <u>6</u>	•000	52,966
	413.5	/o <u>.</u> 9	.0309	69.103	69,549	69.325	•000	69,325 `
6	412.9	(0·9	• 9371	88.755	89.119	88.937	•000	88•936
	412.9	10.9	.0491	132.995	132,995	132.995	•000	132.994
•	412 <u>.</u> 2	10.8°	.0601	186.024	186.024	186•∪24	•000	186.023
_	411.6	10.8	• 9725	266.831	265.831	266.831	•001	266.830

TARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACEM) + 1.50933E-01 (ACEM) \*\* 2 +

0 (ACEM) ##3

PAGE: 3 DATE: 9-15-76

TABLE 41
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

LEZI MNW8EK 15

PART 28J

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTRELL) AFTER THE ADDITION OF 5.2 MG OF SYNTHETIC CONTAMINANT AND AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN<sub>2</sub> IMPACT CYCLES. TEST SPECIMEN (S/N 028) INLET PRESSURE = 415 PSIA (NOMINAL).

	***	***	***	TEST S	PECIMEN INL	ET CONDITIONS	**	****	****	****	NET DIFFERENT	IAL PRESS	
,	PRESS!	JRE *******	***	IEMPERATURE	***	****	****	FLOW RATE	***	****			
•	KĢ/SQ CM	_ P <u>5</u> 1, <sub>A</sub>	DEG. K	DEG. C	DEG. F	LITERS/ MIN	ACFM	SCFM	к <u>е</u> `нй ён5	GN2 LBS/HR	KG/SQ CM Dif <u>f</u> erențial	PSID :	
	29,165	414.0	294.0,	2,,8	69.5	57.5	• : <b>71</b> 8	2.030	3.990	8,810	18,7600	\$ <b>eĕ</b> • <del>6</del> 30	
	29:119	414.4	294•(	29.8	59.5	48.4	•უ6ერ	1.708	3•364	7.415	13.0344	185.392	
	29 <u>•</u> 073	413:5	294+1	2n•9	69,6	38•़8	+ L 487	1.371	2.700	5.952	9-1285	129.837	
	55.013	413.5	294.2	21.0	69.8	29.8	+1374	1.053	2:074	4.571	6.2903	89,469	٠.
*	29.073	413.5	294.3	21.1	70.0	24.5	.0397	.864	1.704	3,751	4.8541	69.042	
	55.013	413:5	294.4	21.2	70.2	19.9	• v25 u	.702	1*38†	3.046	3,6508	51.927	μ
	29.073	413.5	294.5	21.4	70.5	13.1	.v165	.463	•914	2.011	2,1819	31.034	:
	29.073	413.5	294.8	21.0	70.9	13,0	.0163	.457	•50 ř	1,986	2 <sub>-</sub> 1636	30.774	
	29.073	413,5	294.8	21.6	70.9	20,0	.0251	706	1.389	3,063	3,7239	52,966	
	55.013	413.5	294.8	21.0	70.9	24.5	•1309	866	1.709	3,761	4.8740	69,325	
·	29°05R	412.9	294.8	21.5	70.9	29.4	.3371	1.039	2.045	4.510	<u>6</u> <u>.</u> 2526	88,936	
	29:028	412.4	294.8	21.0	70.9	39_ა	•u <sup>49</sup> 1	1.377	2:14	5 <u>•</u> 979	9.3504	132-994	
	28.982	<u>412.4</u>	294.7	21.6	70.8	47.7	•06n1	1.684	3.315	7 <u>•</u> 310	13.0797	186.023	
	28.937	411.0 86682	294.7 *****	21.0 *****	70.8 *****	57 <u>.</u> 4	• 1725	5*0 <b>\$</b> 8	3•99€	8 <u>.</u> 801	18 <u>.</u> 7600	266.830	
	56.000	ئِيدِ 41	294•5	21.3	70.4								
	•038	•5	.3	.3	•5	DEVIATIONS							

PAGE · 1 DATE: 9-20-76

TABLE 42
FLOW RATE VENSUS DIFFERENTIAL PRESSURE
DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAM,
AFTER THE ADDITION OF 10.2 Mg OF SYNTHETIC CONTAMINANT AND AFTER
PART 28L

PART 28L

[EST DESCRIPTION TEST SPECIMEN (S/N 028) INLET PRESSURE = 1000 PSIA (NOMINAL).

TEST MUMBER IS

	*****	**	FLOWMETER	CONDITIONS	**	***	TEST SPEC	IMEN INLET CO	ONDITIONS	
	****	FLOWMETER UNE	****	****	FLOWMETER TWO	***			M.	
łs	FLOW RATE	PRESSURE (PSIA)	T¢mp (UE6: F)	FLUW RATE (ACEM)	PheSoure (P514)	ι <sup>€₩</sup> Ρ	PRESSURE (PSIA)	TAVG (DEG. F)	FLOWANGTE (ACEM)	. ,
	•86	50°5	64 • 7	<u>.</u> 9υ	41.9	59 <u>•</u> 8	1011+9	67.3	<u>*</u> 0429	
	.78	عہُ•ً≤	03 <u>*</u> 5	<u>*</u> hu	48.3	5d•2	1011.9	65 <u>. 8</u>	<u>•</u> 0384	
	•69	. ⊅û <u>•</u> 1	63±1	<u>.</u> 7u	48.5	67.6	i 011.9	65 <u>•</u> 4	∓ŏ33 <i>8</i>	
	<u>.60</u>	45.7	6 < <b>.</b> 4	<b>•</b> €•	4 <b>9</b> •5	57+6	1011+9	65 <u>•</u> 2	₹osáĬ	-
1	<u>•</u> 50	## <u>#</u> 2	62:5	<u>∗</u> 50	40.9	67 <u>•</u> 6	1v11+9	65 <u>•</u> 0	<u>•</u> 024 <u>6</u>	
	• <b>4</b> 0	Pv.5	62.3	. 40	44.9	b7 <b>.</b> 7	1011.9	65.3	•0155.	J
	•̃3ŝ	4× 5	63.5	• 3 ų·	49.3	68,3	1,111.9	65,9	•012\$	
	<u>.</u> 26	#5./	64.5	<u>.</u> 25	49.1	<b>లక</b> ్త	1011.9	66.7	0156	
	•\$1	D <u>v.</u> 4	65 <u>∗</u> 8	• 40	50.1	69 <u>.</u> 3	jųj1.9	67 <u>•</u> 5	40104,	
	<u>.14</u>	ລຄ•<	6 <b>3</b> <u>.</u> 7	•) ⊴	49 • 9	69 <u>*</u> 8	1011.9	67:8	<b>₹</b> 00€5	
ß	•14	47.4	68 % 0	٠١٠	49•5	7 <sub>11 •</sub> 7	1911•9	69.4	•00 <u>68</u> .	
	•35	ង់កឺ*ន	97:4	•2 <u>1</u>	49.9	71 - 0	<u>1</u> 011.9	64 <u>•4</u>	∓õjog5	d
	• <u>2</u> ?	añ∙T	67.5	• 50	49 • 9	/1:1	1011.9	69.3	•01′55	
	•32	añ-7	<del>6</del> 7 <u>.</u> 3	•31	49 ្ 5	71 • 0	j#11.9	69 <u>.</u> 1	±0 <u>1</u> 5 <u>3</u>	
	<u>•41</u>	4 <u>7.</u> 9	<b>55</b> €7	<u>*</u> 40	4 <sup>9</sup> •3	70.0	1,111.9	68.6	*0199	**
	• <u>•</u> •0	47.9	6⊎ <u>•</u> 7	•==	48.9	70+1	1011.9	67.9	.º0246	
Ú	<u>•60</u>	47.2	ចកិត្តប	•by	48 <u>.</u> 7	69 <u>₹</u> 6	1011.9	67.3	<b>∓</b> 0\$9 <u>3</u> .	
	•69	45*4	64 <u>+</u> 4	<u>•</u> 7∪	+8 <u>•</u> 3	69.1	1011+9	66 <u>∙</u> 8	<u>•</u> 033 <u>8</u>	4
	• 7 <u>8</u>	47.9	63 <b>.</b> 9	<u>•</u> 81	48 <u>•</u> 3	08 <u>4</u> 2	1907.9	66±0	•0386	
	±87	>y.4	53.€	•8 <sub>Ī</sub>	4 <sub>8±</sub> 3	67:6	1607.9	65,4	<u>•</u> 0435	

PAGE: 2 DATE: 9-20-76

TABLE 42 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAM, AFTER THE ADDITION OF 10.2 MG OF SYNTHETIC CONTAMINANT AND AFTER 20 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES.

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1007.9

U5.4

,,435

FART 28L TEST DESCRIPTIONTEST SPECIMEN (S/N 028) INLET PRESSURE = 1000 PSIA (NOMINAL). THOT HUMBER 12

ILST SPLEIMEN INLET CONLITIONS \*\*\*\*\*\*\*\*\* GRUSS DIFF: PRESS GRASS DIFF. PRESS NET DIFF PRESS (PSID) AVG GRUSS TARE ų۷G ق∀ير חודד + האבאָּב (אַבְּוֹנוֹן) PRESSURE (PSIA) PRĪN<sub>A</sub>KY (PŠIJ) DIFF. PRESS FLOW RATE SECUNDARY LEMP (PS(i)) (ULG. F) 158.971 158.971 158,971 158,971 1011.9 07.3 ·11429 -0.000 4,,384 133,088 133,680 133,688 133.088 1011.9 ರಿಶ.ಕ -0.000 9دون. 199.660 1,9,008 109.065 109.668 1011-7 05.4 -0.000 86,677 1011.9 ..291 66.441 86,913 86.670 -0.000 65.2 1011.7 .0246 06.682 57.102 66,044 -0.000 66.842 ن ۽ ون 48.516 65.3 0179 48,361 40,071 48.516 -0.000 1011.7 32,660 32,660 J2.666 1011.9 ວລຸ9 .0122 35.625 -0.000 TOŤI°Ă .3140 25,011 25,022 25.016 -0.000 25.017 06.7 .0144 1011.7 67.b 18,811 18,39) 18,051 -0.000 18.851 1011.9 10.909 10.909 0/.8 10,931 ly doc 0,59 -0.000 1011.9 10.700 10.029 10.764 10.765 59,4 . გიიც -0.000 19,177 19,110 09.4 19.043 19,110 1011.9 . ១1 ៤១ -0.000 69.3 .:125 25.596 25,539 25,535 1011.9 25,474 -0.000 1011.9 ô9•1 32.659 45,833 32.746 32.746 ·1123 -0.000 1011.9 . 1199 48.084 08∙6 48.129 45.(39 -0.000 48.084 1011<u>•</u>9 57.9 . 3246 66.557 60.066 66.621 66.622 -0.000 87.713 1011.9 51.3 .1543 87,564 87.8el -0,000 87.713 1011.9 .0338 149.660 109.668 109.665 56.8 -0.000 109.668 1007.9 66.v . 0386 134.952 134.952 134.952 134.952 -0.000

164, 128

164.025

[ARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACEM) + 2.48070E-01 (ACEM) #2 +

104.1126

0 (ACFM) ##3

164.028

-0.000

PAGE: 3 DATE: 9-20-76

FLOW HATE VERSUS DIFFCHENTIAL PRESSURE CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAM)

AFTER THE ADDITION OF 10.2 MG OF SYNTHETIC CONTAMINANT AND AFTER

20 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES.

PART 28L

TEST DESCRIPTIONEST SPECIMEN (S/N 028) INLET PRESSURE = 1000 PSIA (NOMINAL).

TEST WUMBER 12

	7 THE THE	am i la ini	 (5)11 020) 2201	10000000	
TES! SPEC	IMEN INLET CONDITIONS			NET DIFFERENTIAL	PRESS.

	***	*****	***	*****	****	***	***	******	****	***	****	6466446 <del>8</del> 66
a	PRESS	URL <del>-</del>	<b>ង</b>	LEMPERATURE	****	*****	*****	FLOW RATE	****	****	·	
v	KG/SG CM	P51 <sub>A</sub>	UEG. K	υ <b>Ε<u></u>6•</b> ሮ	<u>0Ε,Θ.</u> F	LITERS/	ACF™	SCEM	ĸ <u>ġ</u> \Ĥਔ ĈŊŞ	Γ <del>Β</del> 2/HK GNS	KG/SQ CM DIFFERENTIAL	PS10
	71.144	101123	295 <sup>‡</sup> 8	19.0	67.3	. 84 <u>•</u> @	•042 <sup>9</sup>	2.967	5.841	12.878	11-1768	158,271
	71.144	101j*;	\$92•∩	19•à	05.8	7,5 <u>.</u> 5	•1)3 <sup>84</sup>	2.667	5 <u>•</u> 254	11:579	2.3992	រ័33•ឝ៊ិ <u>ត</u> ិទ
	7 <u>1.144</u>	1011:7	291:1	18.5	<u>05.4</u>	66.0	•v339	2.352	4:234	10:211	7.7104	109.668
	71.144	ioij;	2 <sup>9</sup> 1 <u>•</u> 5	18.5	52.5	. 57 <u>.</u> 2	<u>•</u> 5291	2:019	3.975	8.765	6.0940 . ·	86.677
A	71.144	ĭoJ Ť∓ặ	2 <sup>9</sup> 1•5	18**	65:0	્ 48•ું	<u>•</u> √246	1:707	3,361	7.411	4.6995	66.942
	71.144	111177	291.7	18•2	65.3	<u>39.1</u>	•01 <sup>99</sup>	1:380	2:710	5.988	3.4110	48.516
	71.144	1011.3	292.0	18.0	<u>9</u> 5,9	29 <b>.</b> 9	.0152	1.054	2.070	4.577	\$•\$ <b>\$</b> ē\$	35 <b>-</b> 560
	71.144	1011.7	292.4	19.3	<u>6</u> 6.7	24.8	.0126	.875	1, 124	3.796	1.7588	25.017
	71.144	1011.7	595 <b>.</b> 9	19.	67,5	20.3	<u>•</u> 0194	•7 <u>1</u> 7	1.411	3,111	1.3254	18.851
	71.144	1011:5	293.9	19.9	<u>9</u> 7 <u>.</u> 8	13.4	•0069	474	<u>.</u> 934	2.059	• <u>7</u> 670	10.302
ţţ	71.144	īojī/ā	293.9	2(1.0	09.4	13°4	•00eg	•469	•92 <del>4</del>	2:037	<u>.</u> 756 <u>B</u>	10:(65
	71.144	1011•ă	294.0	20.5	<u>9</u> 9.4	20.5	0105	.723	1•#24	3,138	1,3436	19.110
	71,144	1011.7	293,9	20. !	69,3	<b>25</b> ِ د	.012 <sup>9</sup>	.892	1.752	3.870	1.7953	Š2° 232
	71:144	řájř=ž	593 <b>-</b> в	2.) • 5	99.1	29.9	•0153	1.055	2:07/	4.579	5°3053	32.746
	71:144	1011.7	293.5	د. ن2	68,6	±9•0	•0199	1.376	2.709	5 <u>.</u> 972	3.3807	48.084
	71-144	īāļíšā.	2 <sup>9</sup> 3 <u>.</u> 1	19.9	<u> </u>	48 <u>.</u> 1	<u>•</u> 0245	1.694	3.343	7.470	4.6840	66.922.
ij	71.144	TOJŤ•ś	292.8	19.0	67.3	د <u>.</u> 57	•0293	2,025	3.581	8.790	<u>6•</u> 1668	87./13
	71 <u>.</u> 144	1011.7	\$92.5	19.3	96.8	6 <u>6.3</u>	•033 <sub>H</sub>	2.340	4:20/	10:157	7.7104	109.668
	70.865	100(12	2 <sup>9</sup> 2 <u>•</u> 1	18 <u>.</u> 9	ភិទ្ <b>ំ</b> ពិ	75 <u>.</u> 5	<u>•</u> 03do	2.658	5,454	11:581	9.4881	134.252
	70.865 \$\$\$\$	155(\$\$	291.7	18.0 48484	05•4 ######	85-1	±0435	3:006	Þ <b>1</b> ₹Sú	13≛∪ <sup>5</sup> l	1ị•5323 .	1 <sub>64</sub> •ōśg -
	71:110	1011.5	292•6	19.5	97+1	•				•		· · ·
	• 020	2!	•1	• f	1,3	DEVIATIONS	>					



PAGE: 1 DATE: 9-20-76

TABLE 43
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAM)

AFTER THE ADDITION OF 10.2 MG OF SYNTHETIC CONTAMINANT AND AFTER

TEST DESCRIPTION

TEST SPECIMEN (S/N 028) INLET PRESSURE = 415 FSIA (NOMINAL).

TEST NUMBER 12

PART 28M

TEST SPECIMEN INLET CONSITIONS PLOWMETER CONDITIONS

«សុសុស្តីសុស្តីសុស្តីសុសសពល់លេខសុសសពល់សុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខសុសសពល់លេខ

	FLOWINGTER ONE	·		FLOWMETER TWO				,	
FLOW RATE	PHESSURE (PSIA)	ÎFMP (DEG <u>.</u> F)	FLOW RATE (ACEM)	PRESSURE (PSIA)	TEMP (DEG. 'F)	PRESSURE (PSIA)	AVG TEMP (DEG. E)	AVG FLOW RATE (ACFM)	
•50	⊅ <sub>0•4</sub>	74.7	•5 <sub>0</sub>	49.8	76.7	4,5,7	75.7	•06º8	
• 41	5y.4	74•7	• 40	50 • 0	76 <b>•7</b>	415.7	75.7	• 0469"	
•31	⊋ú <b>,</b> 4	75:0	•30	50.0	76.9	415,7	76.0	•0370	
.26	<b>50.1</b>	75 • 1	.25	49.6	77.3	415.7	76.0	.0309	
•21	÷0•S	75:3	-20	30:0	77•≀	415.7	76+2	•0250	٠,
.15	2• و⊄	75•9	•14	50.0	77.2	415.7	76.5	.0170 [	~
• 55	50.1,	75.9	•21	49.8	77.2	415.1	76.5	•0256	
. 26	2،,2	75•9	.25	50.0	77.2	415.1	76.5	.0310	
.31	49.9	75.7	•31	49.4	77.2	414.4	76.4	037.0	
•40	24.45	75•6	• 40	49.6	77.1	414.4	76.3	.0486	
<u>•</u> 45	⊃ <sub>6</sub> • 2	75•5	· + 45	49.4	76.9	413.8	76.2	• 0544	
<u>.</u> • 50	50.1	75•5	•50	49.2	76.9	413.1	. 76.2	0599	

PAGE: 2 DATE: 9-20-76

TABLE 43
FLOW RATE VERSUS DIFFERENTIAL PRESSURE
DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAM)
AFTER THE ADDITION OF 10.2 MG-OF SYNTHETIC CONTAMINANT-AND-AFTER
20 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES.
PART 28M

TEST DESCRIPTIONTEST SPECIMEN (S/N 028) INLET PRESSURE = 415 PSIA (NOMINAL).

TEST NUMBER 12

TEST SPECIMEN INLET CONDITIONS \*\*\*

	NET DÎFF• PRESS (PSID)	· TARE DIFF. PRESS (PSI <sub>D</sub> )	AVG GROSS DIFF: PRESS (PSID)	GRUSS DIFF. PRESS SECONDARY (PSID)	GROSS DIFF. PRESS PRIMARY (PSI <sub>D</sub> )	AVG FLOW RATE (ACFM)	AVO <u>lemp</u> (Deg• f)	PRESSURE (PSIA)
- 1	248 628	.000	248,628	248 678	248,628	.0608	75.7	415.7
	154.248	.000	154,248	154,244	154,248	.11489	75.7	415.
	94.590	.000	94.590	94.590	94.590	.0370	/6.v	415,7
	71,146	.000	71,147	71,232	71_962	,0309	70.0	415.7
	51,528	.000	51,528	51,662	51,395	.0250	76.2	415./
	29.793	• 0 0 0	29.793	29.942	29.685	·e170	76.5	415.7
1	53.069°	• 0 0 0	53.070	53.240	52.90v	. ,256	76•€	415.1
	71.492	•000	71.49Z	71.548	71.437	•0310	76.5	415•1
	95.221	• 0 0 0	95.222	97.222	95.222	.037.	16.4	414.4
	153,301	.000	153,301	153,301	193.301	.0486	76.3	414.4
	192,442	•000	192.442	192.442	192.442	. 544	16.2	413.5
	244.209	•000	244.209	244.219	244.209	• 1599	16.2	413.1
i								

LARE DIFF. PRESS = -3.4000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM)\*\*2 +

0 (ACFM) \*\*3

ORIGINALI PAGEI IS

PAGE: 3 DATE: 9-20-76

TABLE 43

FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE NORMAL FLOW DIRECTION (S/N SIDE UPSTREAM)

AFTER THE ADDITION OF 10, 2 MG OF SYNTHETIC CONTAMINANT AND AFTER

1 O HIGH PRESSURE (10,000 PSIA NOMINAL) CN2 IMPACT CYCLES.

PART 28M

TEST DESCRIPTIONEST SPECIMEN (S/N 028) INLET PRESSURE = 415 PSIA (NOMINAL).

TOST HUMBER 12

	****	****	***			ET CONNITIONS		***	***	***	NET DIFFERENT		
ı.	PRESSU		***	IE - ERATURE	***	***	*****	FLOW RATE	*****	***			
	KG/SQ CM-	bp j't	OEG. K	DEG. C	DEG. F	LITERS, M <sup>I</sup> N	\CF <sub>14</sub>	scf <sub>M</sub>	KĞ\HH GNS	GN2 LBS/HR	kg/ŜQ cm Dif <u>f</u> erentia <sub>l</sub> .	₽SĨ₽	
	29.229	41521	297.5	.24.3	75,7	48+1	• g6 j3	1.700	3.341	7.378	17.4803	248,628	
	29.229	415.1	297.4	24.3	75.7	3A.7	. 7489	1.368	2,694	5.940	10.8447	154.248	
	29.229	415.	297.6	24.4	76.6	E. 65	.0370	1.036	2.040	4.497	6+6503	94.590	
	29.229	415, [	297.6	24.5	76.0	24.5	.03]9	.864	1.701	3.749	5.0021	71.146	
Í	29.229	415.	297.7	24.5	76.2	19.8	• J25a	.700	1:379	3.639	3.6228	51.528	
	29.229	415.	297,9	24.7	76,5	13.5	•0170	.476	.93!	2.065	2.0946	29.793	.1
	29.183	415,1	297.9	24.7	76.5	20.2	. 1256	.714	1.405	3.100	3,7312	53.069	•
	29,183	415,1	297.9	24.7	76,5	24.5	.0310	865	1.703	3,755	5,0264	71,492	
	29,138	414.4	297.8	24.7	76.4	29.2	្ឋ37ត្	1.032	2.031	4,478	6 6947	95,221	
	29.13ä	414.4	291.8	24.6	76.3	38.3	.0486	1,353	2 665	5.875	10,7781	153,301	
Í'	29,092	413,8	7,795	۶4 <b>.</b> 5	76,2	42.9	.0544	1,514	2,981	6,571	13,5300	192,442	
	29.046	413 <u>. 1</u>	297.7 ****	24 <b>.</b> 5	76.2	47.2	.,,599	1.665	3 <u>•</u> 279	7.228	17.1696	244,209	ıì
	29.179	415.0	297.7	24.6	76.2								
	•051	• (	•1	•1	•2	DEVIATIONS	i						

FAGE: 1 DATE · 9-20-76-

TABLE 44

TABLE 44

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE REVERSE FLOW DIRECTION (S/N SIDE DOWN
STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE
ADDITION OF 5.3 MG OF SYNTHETIC CONTAMINANT AND 10 HIGH PRESSURE

PART 280R

TEST DESCRIPTION (S/N 028) INLET PRESSURE = 1000 PSIA(NOMINAL).

TEST NUMBER 12

	<b>មត់ទំ</b> ងនិតិស៊ីតស៊ីទីពី	*********	FLOWMETER	CONDITIONS	****	**		CIMEN INLET C		-
Į.	***	FLOWME LEK ONE	***	****	FLO*METER TYO		•		•	i
	FLOW RATE	Phessure (PSIA)	TEMP	FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG. F)	PRESSURE (PSI <sub>4</sub> )	AVG TEMP (DEG. F)	FLOW RATE .	٠.,
	.87	5v.1	75.5	•91	47.6	80.6	1017.2	78.0	•0426	
	.78	5,.1	74 • 4	• • 1	48•4	79•9	1.417.2	77•2	•0384	
	•69	5ï.1	73.0	•71	48.4	79+3	1417.2	76.6	.0339	
h	.60	30.5	73.5	.61	48.8	79.1	1017,2	76,3	.0294	-
	.50	50,4	73."	.50	49,5	79.1	1:17.2	76,3	.0246	~
	.41	50.4	73.6	. 4V	49.5	79.1	1/17.2	76,4	.0198	ξ,
	•31	50.2	74.2	.30	49,5	79.3	1.17.2	76.7	.0151	- •
	•\$6	50.1	74.5	, 26	49,5	79.5	1313.2	77.0	.0128	
	• 21	56.4	75.0	•20	49.9	73.5	1017.2	77.3	•0103	
ı	•14	36.42	75 • 7	•13	49+9	79.9	1,17.2	77+8	• ŏ Ō Ĝ B	
	-14	49.7	75•7	•13	49.2	·1 • 4	1017+2	78.5	•0067	
	•22	50.4	76.4	١خ.	49.9	80.3	1.117.2	78.4	•óîo5	- 0
	•26	44.7	76	• 20 •	49.2	19.8	1-17-2	78.2	•0127	
	•31	50.1	15.7	•31	49.3	* ( • <b>1</b>	1317.2	77.9	•0152	
	• <b>÷</b> ĩ´ ˙ ˙¯	5 <sub>0 • 1</sub>	74.7	• 4 U	49.2	79.6	1013.2	77.3	•0199	
jl	•50	49.9	73.0	•50	49.1	79.1	1013.2	76+5	.0246	
•	<b>.</b> \$9	5v.1	77.1	•6v	48 <sub>8</sub>	78.5	1,113,2	75.8	.0290	
	•69	2.14	7?•]	•70	40.5	77.9	1.13.2	75•0	•0339	-1
	•78	50•5	71.5	•81	48.4	7 <b>7</b> • 1	1413*2	74+1	• 0386	
	•87	49.4	7 •5	•91	47.5	76.3	1.09.2	73•4	• 0429'	į

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PAGE· 2 DATE: 9-20-76

#### TABLE 44

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. DATA ACQUIRED CONTITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE REVERSE FLOW DIRECTION (3/N SIDE DOWN
STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE
ADDITION OF 5.3 MG OF SYNTHETIC CONTAMINANT AND 10 HIGH PRESSURE
(10,000 PSIA NOMINAL) GN<sub>2</sub> IMPACT CYCLES. TEST SPECIMEN

[EST DESCRIPTION (S/N 028) INLET PRESSURE = 1000 PSIA (NOMINAL).

TEST HUNNER 12

PART SHOK

Test Specimen Intel Confitions

PRESSURE (PSJA)	∆V(- 1EMP (Ե⊑G, F)	₹₹Ŭ FLON R <sub>A</sub> T <sub>E</sub> (¬CFM)	ત્રસંગ્રેડડ DIFF• અસદકડ PAIM <sub>વ</sub> તેY (୭Տ10)	RM SS DIFF. PRESS SECOMBARY (PSIO)	AVG GRUSS DIFF• PRESS (PSIU)	TARE DIFF. PRESS (PSIn)	NET DÍFF• PRESS (PSID)	ł
1017,4	/8.	.,426	125.846	125.340	125.84t	-0.000	125.640	
1917.2	17.2	. 384	109.116	132.110	109.114	-0.000	109.110	
1017.4	10.6	. 339	45,564	92.096	92.033	-0.000	92.633	
1017.4	(0.3	• , 2 <sup>9</sup> 4	74.72%	7~.914	76.818 .	-0.000	76.818	
1017.2	70.3	. 246	60 <b>.97</b> 1	63.447	61.207	-0.000	61.209	
1017.2	<u> 1</u> 6.4	•11 <sup>7h</sup>	46,642	46.611	46.625	-0.000	46.627	1
1017.2	(6.7	*4121	33.084	33,296	33.19v	-0.000	33,190	
1013+2	17.	* , <sup>7</sup> Sg	و000 <sub>ج</sub> 7	; (.083	27.042	-0.000	27.042	
1017•≤	(7.B	.01.3	29.685	21,768	20.726	-0,000	20.727	
1017.2	17.6	• 4466	12,515	12,377	12,546	-0.000	12,546	
1017.2	/8 <sub>*</sub> \$	.0:67	12,341	12,520	12,431	-0.000	12,431	-
1017.4	18.4	•01 <sup>5</sup>	21.148	21.342	21.245	-0.000	21.245	3
1017.4	18.2	., 127	26.71,	20.911	26.811	-0.000	26.811	
1017.2	17.9	152	33,431	33.7 0	33,565	-0.000	33,566	
1013.2	17.3	•v199	46.816	46,927	46,871	-0.000	46,871	
1013.¢	/6_5	, 7246	60.721	01.131 -	60.456	-0,000	60.926	
1013.4	/5.a	*115Ac	د47.75	75.941	75.72c	-0.000	75 <u>.</u> 720	
1013 <u>∗</u> ∠	fb.	., 339	92,814	93,37#	93.473	-0.000	93.073	ı
1013.2	14-1	• 0336	119,373	117.373	110.379	-0.000	110.373	
1009.2	13,4	<b>.</b> n429	127.102	127.1,2	127,102	-0.000	127,103	1

PAGE: 3 DATE: 9-20-76

TABLE 44

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE REVERSE FLOW DIRECTION (S/N SIDE DOWN
STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE
ADDITION OF 5.3 MG OF SYNTHETIC CONTAMINANT AND 10 HICH PRESSURE
(10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST SPECIMEN

PART 280R

TEST DESCRIPTION(S/N 028) INLET PRESSURE = 1000 PSIA (NOMINAL).

TEST NUMBER 12

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DEVIATIONS

	***	TES! SPECIMEN INF		***	***	NET DIFFERENTIAL PRESS
ľ	PRESSURE	anannanananananananananananananananana	*********	FLO# KATE	****	
				1	CHO	KC 150 011

PRESSURE			340Tupla o. orecessoropopopopopopopopopo			FLO# RATE				****		
	"KG/SQ CM	PSIA	DEG. K	nEG. €	DEG. F	FIT: HS/	∴CF⁄4	SCFM	KĞ\HK PNS	Γ₹2\HK GN5	KG/SO CM DIFFERENTIAL	PSID 1
	71.514	1017.2	z:98.7	25.0	78 <sub>-4</sub> ·	82.8	• 1427	2- <sup>9</sup> 02	5.715	12.599	8.8474	125.840
	71.514	1011.2	294.2	25•ι	77.2	74.3	• 3 <sup>H</sup> 4	2.624	5.166	11•390	7,6712	10 <sup>9</sup> •110
	71.514	1017.2	247.9	74.8	76.5	65.6	• 339	8.316	4 <u>•</u> 560	10.052	6.5 <sub>12</sub> 7	92.633
ıί	71.514	1017.2	297.5	24.b	76.3	56.9	۰ ۲۰ ۲ <sup>۷</sup> ۹	<•00 <sup>9</sup>	3. <sup>9</sup> 5!	8.723	5•4 <sub>00</sub> 8	76.8 <sub>1</sub> 8
	71.514	1017.4	8 . 97م	74.6	76.3	47.7	. ,245	1 • 684	3.316	7.310	4.3034	61.20 <sup>9</sup>
	71.514	1017.2	297.9	24.1	76.4	34.4	• 1 <sup>9</sup> 13	1.356	2.671	5.888	3.2782	46.527
	71,514	1017.4	296.0	24.5	76,7	29.1	.2151	1.0≥9	2.020	4,467	2,3335	33°Ĭ <sub>8</sub> 0
	71,235	1013.6	298.2	25.	77.,	24.7	· (120	.871	1.715	3.781	1.9012	27 <b>.</b> 042
	71.514	1017+2	298.3	25.2	77.3	19.8	• (193	•730	1.379	3.040	1.4572	20.727
ŀ	71,514	1917.2	798.6	25.4	77.8	13.1	. g6 v	.463	•a15	2.011	.888.	ĩ2.546
	71,514	1017.2	299.0	24.9	78.5	12.9	. 1057	.456	. 69ÿ	1.982	.8740	12.431
	71.514	1017.4	. 69× · 9	25.8	78.4	≥,.3	.0105	.716	1.410	3.108	1.4937	21.245
	71.514	1017,2	298.5	5.7	78.2	24.4	127	.H62	1.698	3.744	1.8850	26.811
	71.514	1017.2	×98.7	د <b>.</b> 5	77.9	29.3	•4152	1.034	2,036	4.489	2,3599	33,566
	71.235	7+FI91	X98.3	25+1	/7.3	34.4	• 1199	1.355	2.668	5.883	3.2954	46.87 <u>1</u>
ì	71.235	1913.4	297.9	24.1	76.5	47.4	• 124 5	1.673	3.294	7.261	4.2835	60•926
	71.235	1013.4	~97.S	24.3	75.8	क्षाक्ष)	• 62 <sup>9</sup>	1.979	3:891	8.59 <sub>1</sub>	5.3236	75• <b>7</b> 20
	71.235	1013:4	297.,	23.4	75.6	65.6	• 9339	2.317	4 <u>•</u> ⊃63	10-059	6.5437	93.073 <sup>~ )</sup>
	71,235	1013.6	ه ه 96 خ	23.4	74.1	14.1	.4380	2.638	5.194	11.451	7.7600	110.373
	70 956	1109.4	290.2 ****	******	73.4 *****	សិ <b>ខ</b> ិត	. 1420	. 2,925	5 <u>.</u> 759	12,697	8,9362	127.103
	71,403	1015.0	298.0	24.9	76.7							-11 THJ



PAGE · 1 DATE: 9-20-76

#### TABLE 45

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. DATA ACQUIRED IN THE REVERSE FLOW DIRECTION (S/N SIDE DOWN FLOW HATE VERSUS DIFFERENTIAL PRESSURE STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE ADDITION OF 5.3 MG OF SYNTHETIC CONTAMINANT AND 10 HIGH PRESSURE

(10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST SPECIMEN TEST DESCRIPTION(S/N 028) INLET PRESSURE = 415 PSIA (NOMINAL).

TEST NUMBER 12 PART 28PK

FLOWMETER CONDITIONS TEST SPECIMEN INLET CONDITIONS FLOWNLIEK ONE FLOWNETER TWO TEMP (DEG. F) PRESSURE (PSIA) PRESSURE ELOW RATE PKF 220HF FLOV RATE (ACEM) T<sub>EMP</sub> TEMP (DFG. F) (PSIA) 79.6 •0709 415.5 •58 49.1 81.2 2006 70.9 • 50 415.5 79.6 • 0596 49.9 49-1 •50 74.9 •5u on•2 79.6 0484 •40 54.4 74.4 49.7 41.2 414.8 •41 **79.7** · 0368 .31 Du.2 79 . . . 44.9 .... 414.8 • 3 U .0312 .26 20.4 79:0 4.4 414.8 79.7 50 - 1 -20 49.9 79.7 .0253 .21 79.0 .21 49.5 R. . 4 414.2 414.2 79.9 .0164 .14 20.1 .13 49.9 84.5 79.2 50.2 414.2 79.9 .14 74.3 .13 សត្. ៦ .016+ 50.1 •0253 79.8 .21 ∌∿•1 79.5 49.7 86.5 414.2 .21 .0311 49.7 413.5 79.6 -26 78.8 . ~6 49.3 153.4 .0370 79.5 413.5 .31 50.1 73. 2 .31 49.5 96.3 .0489 412.9 79.3 .41 50.1 78 • 4 .41 49.3 -0.1 • 0599 44.9 79.1 •50 78.3 •50 46.9 0.00 412.2 .0690 •57 78 . 4 -55 .8.9 79.8 411.6 79.1 20.1

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PAGE: 2 DATE: 9-20-76

TABLE 45

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE REVERSE FLOW DIRECTION (S/N SIDE DOWN

STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE

ADDITION OF 5.3 MG OF SYNTHETIC CONTAMINANT AND 10 HIGH PRESSURE

(10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST SPECIMEN

PART PARK

TEST DESCRIPTION(S/N 028) INLET PRESSURE - 415 PSIA (NOMINAL).

TEST NUMBER 12

TEST SPECIMEN INLET COUNTITIONS

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3	NET DIFF• PRESS (PSID) .	TAPE DIFF• PRESS (PSID)	AVĢ ĢRUSS DIFF. PRESS (PSID)	UIFF. PRESS SECÖ√DARY (PS10)	AROSS DIFF: PRESS PRIMARY (PSID)	AVG FLOW RATE (ACHH)	1∨6  EMP   (D#G• F)	PRESSURE (PŠIA). —
	268,715	•001	288.716	288.716	288.716	•07:9	4.61	415.5
	196,545	.000	196.546	196.546	196.540	• , 596	49.6	415.5
	137.518	.000	137.519	137,519	137,519	• (* 484	(9.5	414.년
	93.034	•000	93.034	93,412	93.,57	. ევ68	19.7	414.5
	73•785	.000	73.78 <u>5</u>	73./57	73.814	.0312	19.7	414.0
.,	55.585	• 0 0 0	55.586	55.765	55.417	• ¢253	19+7	414.4
·	32,659	-0.000	32.659	32,775	32,543	•01 <sup>64</sup>	<u> (9.9</u>	414.6
	32,832	~0.000	35*433	32,493	32.775	•104	19.9	414.2
	56,560	.000	56.561	56.712	56.41 ป	. 253	ia*8	414.2
	73,377	.000	73.375	73,442	73,314	.0311	19.6	413.5
2.▼	94,274	.000	94.275	94,275	94,275	.0370	(9.5	413.5
jj	140,359	.000	140,360	140,360	140,360	. 3 <sup>489</sup>	(9.3	412.7
	199,702	.000	199.702	199,702	199,792	.0599	19.1	412,2
	271.354	•001	271.355	271.355	271.355	• 0590	(9 <u>.</u> 1	411.5

JARA DIFF. MRESS = -3.43000E-05 + -4.44000E-04 (ACF4) + 1.50933E-01 (ACFM) +2 +

0 (ACFM) ##3

PAGE: 3

DATE: 9-20-76

TABLE 45

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE REVERSE FLOW DIRECTION (S/N SIDE DOWN
STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE
ADDITION OF 5.3 MG OF SYNTHETIC CONTAMINANT AND 10 HIGH PRESSURE
PART 28PA 15PT DESCRIPTION(S/N 028) INLET FRESSURE - 415 PSIA (NOMINAL).

TEST NUMBER 12

	****	****	*******			el conditions		*****	***	***	NET DIFFERENT	
f.	PRESSU คระสะสะสะสะสะสะ		*****	IEMPERATURE	***	***	****	FLOW RATE	****	***		• • • •
	KG/SQ CM	PSIA	neg. K	DEG. C	DEG. F	LITERS/	ACFM	SCFM	ĸĠ`Ħĕ ĕiv5	LBS/HR GN2	KG/SQ CM DIFFERENTIAL	PSKO " 1
	2 <sup>9</sup> •210	415.5	299.5	26.4	79.6	55.7	• 1) 7119	1.967	3.87₹	8.539	20.2987	288.715
	2 <sup>9</sup> +210	415.5	299.6	26.+	79.6	46.8	*+15 <sup>9</sup> h	1.654	3.25?	7,182	13,8185	196 <u>.</u> 545
	29.165	414,8	გ99.ი	26.4	79.6	a+⊬E	• 444	1+342	2.642	5,824	9,6685	ī37•5 <u>î</u> 8
â	29.165	414,8	299.6	26.5	79.1	5u.6	• 1368	1.021	2:011	4•433	6,5409	93• <u>0</u> 34
•	29.165	414.0	299.7	26.5	79•7	24.5	. 312	•a66	1.705	3 <sub>•7</sub> 59	5,1876	73.785
	29,119	414.2	299.7	26,5	79.7	19*a	:253	699	1.376	3.033	3,9080	55 585
	29.119	414.4	299,8	26.6	79.9	12.9	.,164	.455	.895	1.974	2,2961	32,659
	29.114	414,2	299.8	26 <b>.</b> n	79.9	12.0	.3164	<b>,</b> 454	893	1.969	2.3083	35 635
	29,119	414.4	299.7	26.b	79.8	19.9	.0253	.701	1 • 38 i	3.044	3,9766	56,560
А	29.073	413.5	299.6	26.5	79.6	24.3	.v311	,859	1.690	3,727	5.1589	73.377
•	29.073	413.5	299.5	26.4	79.5	24.9	370	1.021	2:011	4.433	6,6281	94.274
	29.028	412.5	299.4	26+3	79.3	38.2	•4469	1.349	2,65/	5.857	9.8682	140•359 <sup>3</sup>
	28,982	412,6	299.3	26.2	79.1	46.8	. (1599	1.652	3 • 254	7:173	14.0404	199.702
	28.937 ####	411.6 ****	299.3	******	79.1 *****	53.8	• 069 <sub>0</sub>	1.898	3•ੁ73੪ੁ	8.240	19,0781	271.354
	29:106	414.4	299.6	26.4	79.6							<del>-</del>
4	•065	<u>. 5</u>	.1	•1	5.	DENIATIONS	;					

PAGE; 1

DATE: 9-20-76 ...

### TABLE 46

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE REVERSE FLOW DIRECTION (S/N SIDE DOWN
STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE
ADDITION OF 11.1 MG OF SYNTHETIC CONTAMINANT AND 20 HIGH PRESSURE
(10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST SPECIMEN.

TEST DESCRIPTION (S/N 028) INLET PRESSURE = 1000 PSIA (NOMINAL).

TEST NUMBER 12

PART 28RR

Ç	****	***		CONDITIONS	**	****	TEST SPE	CIMEN INLET CO	ONDITIONS
ŧ	******	FLOWMETER ONE	***	***	FLOWNETER TWO		- w	a see a seeme assessed	1)
	FLOW RATE	PRLSSURE (PSI4)	TĘMP (nEG• F)	FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	TEMP (DEG. F)	FLOW RATE
	<u>•</u> 87	49.9	72.6	•91	47.6	76.7	1013•Ž	74.6	•0427
	•78	50.1	71 • 4	•A1	48 • 1	75.9	101 <b>3</b> •8	73+6	+0385
ţ	•69	ລິບ•4	7n+5	•70	48.9	75•1	1009.2	72.8	•0343
	•60	54.5	7 •1	•60	49-1	74 <b>-</b> B	1109+2	72.5	•0295
	•50	5 <sub>0•1</sub>	70-1	•50	49•1	74.7	1009•2	72.4	10246
	.41	5v.1	7, .3	.40	49,3	74.7	1.09.2	72.5	1020.
	<u>•</u> 31	01.0	76.9	•30	50 • 4	75•}	1009.2	73.0	•0154
	• 26	49.7	71.3	. 25	49.3	75.2	1009.2	73.3	.0127
•	<u>.</u> 21	49.9	71 - 7	.20	49.7	75.5	1009.2	73.6	+0103:
	.14	49.9	72.4	.13	49.7	75.8	1009.2	74.1	.8500.
	<u>•</u> 14	49.5	73•7	•13	49.3	76•4	1009-2	75•1	• 006B
	•22	⊅γ.4	73.5	•21	50.2	76.4	1009+2	75.0	-0107
	.26	49.9	73.3	5د .	49.5	76.4	1009.2	74.9	.0127
	•31	àn°1	73.0	.30	49.7	75.4	1009.2	74.7	.0152
ř	. <sup>41</sup>	p0.5	72.3	.40	49,5	76_1	1005,3	74,2	0200
	.50	50.1	71.5	.50	49.1	75.7	1005.3	73.6	.0247
	•59	49.9	75.40	• 4 ઇ	48,7	75.1	1005.3	72.9	•0293
	.69	⊅v.1	64.9	.73	48.7	74.6	1005.3	72,3	.0341
	.78	49.9	69.2	.91	46.1	74.0	1005.3	71.6	.0386 T
	.87	50.1	64.6	•91	47,9	73.2	1001.3	70.9	., 0435

PAGE: 2 DATE: 9-20-76

TABLE 46

#### FLOW RATE VERSUS DIFFFRENTIAL PRESSURE

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE REVERSE FLOW DIRECTION (S/N SIDE DOWN
STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE
ADDITION OF 11.1 MG OF SYNTHETIC CONTAMINANT AND 20 HIGH PRESSURE

(10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST\_SPECIMEN\_ TEST\_DUSCRIPTION(S/N 028) INLET PRESSURE = 1000 PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* PROSS GR SS DIFF. PRESS AVG GROSS DIFF. PRESS TARE DIFF. PRESS NET дVG , V15 DIFF. PRESS DIFF PRESS SECONDARY PRESSURE TEMP FLOW RATE PRIMARY (PS10) (PSID) (PSID) (PSID) (PSID) (PSIA) (0±G. F) (iCFM) 226.007 226. 107 -0.000 74.6 . 427 226.007 225.307 1013.2 190.969 190.969 -0.000 73.6 . 385 1911,969 191,969 1013.2 158.773 158,773 ...343 158,773 -0.000 1009.2 12.8 158,773 125.630 125.629 125,629 125.629 -0.000 1009.2 12.5 . . 275 95,643 95.642 95.642 95.642 -0.000 1009.4 72.4 . 1246 70.896 70.896 -0.000 1009-2 12.5 1056. 70.771 71.622 48,387 48.387 1009.4 73.0 .0154 48 479 48.295 -0.000 36.931 36,877 36,944 36.93( -0.000 /3.3 .. 127 1009.2 27,858 57,888 27.857 27.627 -0.000 1009.4 13.6 .01.3 15.973 15,973 15,934 16.. 11 1009.4 14.1 . ពួក២៦ -0.000 15.886 15.954 15.886 1009.2 15.818 -0.000 8d000 15.1 29,128 29.211 29.126 75.0 29.045 1009.2 -0137 -0.000 36,873 36,872 36,944 **~0.000** 36,761 1009.2 14.9 .0127 47.881 47.881 1009.2 .. 152 47.783 47.979 -0.000 14.7 70.205 70.300 70.205 -0.000 74.2 70.02) 1005.4 .0200 96,274 96,274 96,274 96.274 -0.000 1005,3 13.6 . 1247 125.314 125.314 125.314 125.314 -0.000 12.9 .4293 1005.3 158.142 158.141 15%.141 150.141 -0.000 د.1005ء 12.3 . (,341 193.495 193,494 193.494 -0.000 193.494 1005.3 11.6 0.386 233,898 233,898 و.1001 10.9 .0435 233.890 233,898 -0.000

IARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM)\*\*2 +

0 (ACFM) ##3

PAGE: 3

DATE. 9-20-76\_

### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TABLE 46

CONTAMINATED CONDITION = FLOW\_RATE\_VERSUS DIFFERENTIAL PRESSURE.

DATA ACQUIRED IN THE REVERSE FLOW DIRECTION (S/N SIDE DOWN
STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE
ADDITION OF 11.1 MG OF SYNTHETIC CONTAMINANT AND 20 HIGH PRESSURE

(10,000 PSIA NOMINAL). GN2 IMPACT CYCLES. TEST SPECIMEN

TEST DESCRIPTION(S/N 028) INLET PRESSURE = 1000 PSIA (NOMINAL).

TEST NUMBER 12

PART 28RK

TEST SPECIMEN INLET CONDITIONS NET DIFFERENTIAL, PRESS.

#	PRESS!			TF	***	***	***	FLOW RATE	***	****		
к	ē∕šo cM	PSIA	DEG. K	7)EG. C	DEG. F	LITERS/ MIN	ACFM	SCFM -	К₫ЛНН— ВиЅ	E8>\HK	KG/SQ CM	РЅІД
	71.235	1013.2	\$96.8	7.وح	74.6	82.6	427	2.915	5 <u>•</u> 740	12.656	15.8899	226.007
	71.235	1013.2	296.3	23 • 1	73.6	74.6	· 385	2.633	5 <u>•</u> 18∳	11.429	13,4265	190-366
	70.956	1009+4	8•55ج	55.1	72.8	რრ∙4	4,343	2.346	4.619	10.184	11.1629	158.773
	70.956	1009+4	295.6	55.9	72.5	57 • 1	· 2 <sup>9</sup> 5	2.017	3.972	8.756	8.8356	125.630
	70.956	100 <sup>9</sup> :4	295.6	22.4	72.4	47.7	•9246	1.683	3.315	7.307	6,7243	95.643
	70.956	1009+4	295.7	22.5	72.5	39.0	•0201	1.376	2.709	5,971	4,9845	70.896
	70.956	1009.4	295.9	8,55	73.0	29.8	.0154	1.051	2 <u>.</u> 07ŏ	4.563	3.4020	~48 <u>~38</u> 7
	70.956	1009.2	296.1	58°8	73.3	24.5	.5127	.864	1.700	3.749	2,5965	36_337
	70.956	1009.2	296.3	23.)	73,6	20.0	.0103	.705	1 • 38ž	3.062	7,9586	27 <u>-8</u> 56
	70.956	1009.2	296.6	23.4	74.1	13.1	•1, g6B	.464	<u>•</u> 913	2.013	T-1230	~~ 15 <u>~9</u> 73
	70.956	1009.4	297.1	23.9	75.1	13•1	•005A	•462	•910	2.006	1.1169	<u>1</u> 5•886
	70.956	1009,4	297.0	23. <sup>9</sup>	75.n	2,1.6	.0107	.726	1,430	3,152	2.0479	59 <b>-</b> i 58
	70,956	1009,2	297.0	23,8	74.9	24.4	127	. <sup>86</sup> 1	1 696	3,739	12,5924	36-873
	70.956	1009.4	296.9	23.7	74.7	29.2	.0152	1.033	2 • 034	4.484	3,3664	47-881
	70±677	1005.3	296.6	23.4	74.2	38.4	•4200	1.357	2.671	5 <u>6</u> 89	4.9359	10.502
	70-677	1005.3	296.3	23.1	73,6	47.5	·1247	1.677	3.305	7.279	6,7687	96-\$? <del>\</del>
	70.677	1005.3	295.9	22.7	72.9	56•4	•J293	1.992	3.922	8.647	· -8-8104 · -	125.314
	70.677	1005.3	2 <sup>9</sup> 5•5	42.4	72.3	65.8	•0341	2.323	4 <u>•</u> 575	10.086	11.1185	128.145
	70.677	1002.3	295.2	27.0	71.6	74.5	•.j386	2.632	5 <u>•</u> 183	11:427	13.5040	~ 193 <del>.49</del> 5
	70.398 ****	1001.3	, 294.B ####	21.6	7 <sub>0</sub> .9	83.7	• 1435	2.956	5 <u>.</u> 820	í2•832 °	16.4447	533 <u>*8</u> 88
	70.886	100 <u>8.</u> ⊄	296.1	23.0	?3.4			-				
	.154	2,4	,5	.5	1.0	DEVIATIONS	ŝ					



PACE: 1 DATE: 9-20-76

FI OW RATE VEHSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. DATA ACQUIRED IN THE REVERSE SLOW DIRECTION (S/N SIDE DOWN STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE ADDITION OF 11.1 MG OF SYNTHETIC CONTAMINANT AND 20 HIGH PRESSURE (10,000 PSIA NOMINAL). CN2\_IMPACT.CYCLES.\_\_TEST\_SPECIMEN\_\_\_\_\_\_
TEST\_DESCRIPTION (S/N 028) INLET PRESSURE = 415 PSIA(NOMINAL).

TEST NUMBER 12

PART 28SK

TEST SPECIMEN INLET CONDITIONS FLOWMETER CONDITIONS <sup>我</sup>在我们的现在我们的现在分词的现在分词的现在分词 "我们的一个人,我们们们的一个人,我们们们的一个人,我们们们的一个人,我们们们的一个人,我们们们的一个人,我们们 FLOWMETER THO FLOWNEJER ONE \*\*\*\*\* AVG FLOW RAJE AVG

TEMP PRESSURE TEMP PRESSURE (PSI<sub>A</sub>) PPESSURE TEMP FLOW RATE FLOW RATE (PSIA) (ACFM) (DEG. F) (ACFM) (ACEM) (PSIA) (DEG. F) (DEG . F) 419.5 78.5 78-9 ·0487 75.0 50.1 •41 50.6 • 40 418.H 78.5 .0427 79. • 36 50.1 50.4 78<u>•</u>1 .36 78.6 <u>•0368</u> 418.8 79-1 7.3 • 1 50.1 • 31 ⊅u•6 •30 **.**0313 415.8 7877 79.2 .26 ១៤.4 78.2 .26 50.1 78,9 0247 418.8 49 9 79.4 71.3 .20 .21 **ບ**ບ 1 .0165 79.1 418.8 .13 79.6 **υ.1** 78.6 50.1 .14 79.4 , 5164 418.8 79.9 .14 ĵ0.l 78.9 .13 50.1 .024B 779.5 ,21 49.5 80.0 418.2 49.9 7K.9 .21 418.2 79.5 .0304 .26 49,7 .25 80.0 Þv.l 78.9 417.5 79 • 4 49.7 80.0 •31 50.1 79.8 •31 4,7.5 79.4 .0418 • 35 49.5 80.0 50.1 78.8 • 35 79.2 .0483 416.9 49.3 79.8 ⊃0.1 78.7 .41 •41

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PAGE: 2 DATE: 9-20-76

TABLE 47

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. DATA ACQUIRED IN THE REVERSE SLOW DIRECTION (S/N SIDE DOWN FLUM RATE VERSUS DIFFERENTI L PRESSURE STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE ADDITION OF 11.1 MG OF SYNTHETIC CONTAMINANT AND 20 HIGH PRESSURE

(10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST SPECIMEN TEST OFSCRIPTION(S/N 028) INLET PRESSURE = 415 PSIA (NOMINAL). PART 28SR TEST NUMBER 12 TEST SPECIMEN INLET COMPLITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* OIFF PRESS aRnSS AVG GRUSS NET TARE "DIFF." PRESS VG AVG DIFF. PRESS DIFF. PRESS DIFF. PRESS SECONDARY PRESSURE TEMP FLOW RATE PRIMIRY (PSID) (PSID) (PSIU) (PSID) (PSIA) (ULG. F) (ACFM) (PSIU) 249.575 249.575 249.575 49,575 .000 . 487 419.5 18.5 188.023 188.023 135.177 .000 198,425 418.8 18.5 .427 142.253 142,254 142.254 .000 . ,368 18.6 142,254 418.8 107.532 107.532 1.7.532 .000 1 7.532 8.7 . .313 418.6 74.634 74.634 .000 74.7 4 74.565 418.8 78.9 ...247 42.120 42.254 42.121 -0.000 41.937 418.0 79.1 .0165 41,918 41,918 -0.000 42. 11 19.4 . 154 41.755 418.9 75,483 75,483 75.315 75.051 .000 418.2 19.5 .1:248 103.744 103,744 103.744 .000 153.744 418.2 4.5 .0304 141.306 141,347 141.307 .000 141,307 417.0 19.4 . . 367 180.447 180.447 180.447 · ;418 180.447 417.5 19.4 .000 245.472 245.471 245.472 245,472 •000 19.2 . 483 416.9 0 (ACFM) ##3 TARE DIFF. PRESS = -3.4 1000E-05 + -4.44000E-04 (ACF/) + 1.50933E-01 (ACF/) #2 +

PAGE: 3

DATE: 9-20-76

TABLE 47

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED IN THE REVERSE SLOW DIRECTION (S/N SIDE DOWN

FLOW RATE VERSUS OFFERENTIAL PRESSURE STREAM) AFTER COMPLETION OF THE FORWARD FLOW TESTS AND AFTER THE ADDITION OF 11.1 Mg OF SYNTHETIC CONTAMINANT AND 20 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST SPECIMEN

PART 285R

TEST DESCRIPTIO(8/N 028) INLET PRESSURE = 415 PSIA (NOMINAL).

TEST NUMBER 12

	\$\$UR <u>C</u> *********	****	TEMPERATURE	****	*****	*****	FLOW RATE	***	***		
KĢ∕SQ CM	АІга	ora	oeg, c	DEG. F	LITERS/ "In	ACFM	scFm	<u>ぺ</u> ੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑੑ	GN2 LBS/HR * *	KG/SQ CM	PSĮD
29,493	419.5	299.	25.8	76.5	38.7	. 437	1.367	2.692	5.935	17.5469	249.575
29.447	418.8	299.0	25.9	75.5	33.9	. 427	1.199	2 <b>.</b> 360	5,-204	13.2193	188,053
29.447	418.8	299.1	25.9	78,6	29.2	368	1.032	5 • 033	4.481	10-0014	142,253
29.447	416.8	299.1	26.	78.7	24.B	• ,313	.877	1.720	3.805	7.5602	<u>10</u> 7,532,
29.447	41g.8	299.2	26. /	78.9	19.6	247	.693	1.364	3.007	57.2473	74,634
29,447	4] ៦ ៦	299.3	26,2	79,1	13,1	.0165	.462	.910	2,006	2,9614	42,120
29.447	418.8	299.5	26.3	79.4	13.0	··1164	.459	±904	1•992	2.9471	41.918
2 <sup>9</sup> :4 <sup>0</sup> 2	418.2	2 <sup>99</sup> .5	6.4م	79,5	19.6	.4548	•6 <sup>9</sup> 4	1.365	3.012 ·	\$.3070 °	75,483
29.402	418.2	299.5	26.4	79.5	24.0	.0304	.849	1.672	3.685	~7 <del>,</del> 2939	103,744
29.356	417.5	299.5	26.3	79.4	29 • 0	.3367	1.024	2.010	4.445	9.9348	141.306
29.356	417.5	299.5	26.3	79.4	33•0	•0418	1.166	2:295	5.061	12:6867	180.447
2 <sup>9</sup> ,311	416.7	29 <b>9.</b> 4	4****	79 <b>.</b> 2	38+1	••)4 <sup>13</sup> 3	1.347	5 <sup>‡</sup> 62 <sup>4</sup>	5:848		Z45,471
29:41?	410-4	299.3	26+1	79.1							
<u>•</u> 043	:0	• 5	• 2	•3	DEVIATIONS						
									٠.	— A see	
								•		. پريستند ۽ پيدستان سان	



TABLE 48
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

DATE: 8-31-76----

PAGE: 1

TEST NUMBER 5

PART 250R

TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTAIL PRESSURE. FLOW IN REVERSE DIRECTION. TEST SPECIMEN (S/N 025) INLET PRESSURE = 415 PSIA NOMINAL.

TEST SPECIMEN INLET CONDITIONS

我你你我看你你你你你你你你你你你你你你你你你你你你你你你你你你你你你你你你你	PLOWPETER CONDITIONS	
	*******************************	****

•	***	FLOWMLIER ONE	***	****	FLOWMETER TWO	***	-		
	FLOW RATE	PRESSURE (PSTA)	TEMP (DEG• F)	FLOW RATE (ACFM)	PRESSURE (PSÌA)	TEMP (DEG. F) _	PRESSURE (PSIA)	AVG TEMP (DEG. E)	FLOW RATE (ACEN)
	<u>.</u> 54	ងុម្ភ-6	84 • 4	•55	49.9	85.3	415.6	.84.8.	. 0656
	<u>.</u> 50	∍v.2	84.3	.50	49.5	85.3	414.9	84,8	.0601
l)	<u>•</u> 41	## · 7	94+2	.41	49.1	85 <b>.3</b>	414.9	84.7	.0485
,	•31	±¼.9	84+1	•31	49.5	85.2	414.3	84.7	0370
	<u>.</u> 26	ង់កំ*ខ	84 • 1	.26	50.2	85.2	<u> 414.3</u>	84 <sub>9</sub> 6	•0314
	<u>.</u> 21	20.2	84:1	.21	50 <b>•0</b>	85.2	414.3	. 8 <u>4.7</u>	-0252
	.13	5 <sub>7.2</sub>	84+3	.13	50.0	85.4	414.9	84.8	0157
	.10	ಶಿಕ್ಕಿದ	84.5	• 09	50.0	85.5	414.9	85.0.	.0114
	<u>•</u> 10	50.l	84.5	• 1. 9	49.9	<b>₫5•</b> 4	<del>4</del> 15.6	84.9	+0114-
•	.13	50.4	84.5	.13	50.2	85.5	415.6	85+0	0159
	<u>.</u> 21	56*1	84 • 4	•21	49.9	85∙5	415.6	84.9	·0251 1
	•26	49.9	84 <u>•</u> 2	•26	49,5	85,5	414.9	84.8	
	•31	44.9	84+1	•31	49.5	85•4	414.3	8,4.7	•0371
	.40	50.1	83.9	-4¢	49.5	85+2	414.3	84.5	
	49	#¥.7	83.6	• <b>5</b> 0	48.9	85•1	413.7	84.3	• 0593
	<u>.</u> 54	49.7	83.8	,55	48.7	85.√	413.0	84,4	.0647

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TABLE 48
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 8-31-76

TFST NUMBER 5	PART 750R	ĮEST DESCRIPŢION	CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. FLOW IN REVERSE DIRECTION. TEST SPECIMEN (S/N 025) INLET PRESSURE = 415 PSIA NOMINAL.
TEST SPECIMEN INLET CONDITIONS			de A de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la company de la compa
*****************			A . D. STEEL BATE I.

	•	•					
PRESSURE (PŠÍAI	AVG LEMP (DEG. F)	AVG FLOW RATE (ACFM)	GROSS DIFF: PRESS PRIMARY (PSID)	GROSS DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF PRESS (PSID)	NET DIFF. PRESS (PSID)
415.0	<b>⊍4</b> •8	, 4656	347.299	3 <sub>0</sub> 7,299	307.299	.001	307,299
414.9	<b>84</b> • 8	.0601	245,671	245,671	245.671	•000	245,670
414.9	84.7	. 465	169.821	169.821	169.82]	•000	169.820
ڊ.414	84 <u>•</u> 7	.03/1	115.777	115.777	115.777	•000	115.777
414,3	54.6	.,314	92.143	93,022	92.603	•000	92.602
414.3	<b>84</b> •7	. 1252	69.452	70.267	69 • <b>8</b> 6 0	•000	69.859
414.7	114.8	.0157	40.520	40.837	40.678	-0.000	40 <u>.</u> 678
414.9	85•t	• 1114	28,642	28.753	28.697	-0.000	28,697
415.0	04.9	. 114	28.526	28,695	58*617	-0.000	28.610
415.0	85∙#	.(,159	40.925	41.183	41.054	-0.000	41,053
415,9	84±9	.0251	70.202	74.899	70.550	000	70.550
414.7	8.4.€	.0310	91.211	92.074	91.643	•000	91.642
414.2	84.7	.0371	117.041	117.041	117.041	•000	117.041
414.5	^ 4 <b>.</b> 5	.04-3	170.769	179.769	170.769	.000	170,768
413.4	<b>04.</b> 3	. 4593	242.827	242.827	242.82!	•000	242,826
4]3• <u></u> ÿ	84.4	•0647	300.346	300.346	300.346	•001	300.346

TARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACEM) + 1.50933E-01 (ACEM) \*2 +

0 (ACFM) ##3

PAGE: 8-31-76

#### TABLE 48 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5

PART 250R

TEST SPECIMEN INLET CONDITIONS

TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. FLOW-IN REVERSE DIRECTION. TEST SPECIMEN (S/N 025) INLET PRESSURE = 415 PSIA NOMINAL.

NET DIFFERENTIAL! PRESS PRESSURE TEMPERATURE FLOW RATE \*\*\*\* \*\*\*\*\*\* \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* d GN2 ĢNŽ KG/SQ CM LITERS/ KG/SQ CM PSIA UEG. K υEG. C DEG. F MIN ĸĞŹĦŖ LBS/HR .... DIFFERENTIAL **ACFM** . \_ SCFM PSID\_ 29.219 415.0 3,,2,5 29.4 54.8 .0656 3.550 7.826 51.0 1.803 21.6053 307.299 29.174 414.7 302.5 29.3 245-670 84.8 46.7 .0601 1.650 3.249 7.163 17,2723 29,174 302.5 414.9 29.3 84.7 37.7 . 11485 1.333 2.624 5.786 11.9395 169.820 29.128 414.5 302.4 29.3 84.7 28.7 .0370 1.015 1.995 4.404 8.1399 115,777 29.128 414.2 302.4 29.2 84.6 24.4 . 3314 .861 1.695 3.737 92,602 6.5106 29,128 302.4 414.2 29.3 84.7 19.5 . 0252 .690 1.359 2.996 69.859 4.9116 29.174 302.5 414.9 29.4 2.8599 84.8 12.2 .0157 .432 <u>.8</u>50 1.875 40,678 29.174 372.6 414,7 29.4 85.3 8.9 . 0114 .314 <u>•61</u>2 1.364 2.0176 28,697 29.219 3,2.6 29.4 415.0 84.9 ყ•9 .313 -619 1.358 ev114 2.0115 28,610 29.219 415.0 312.6 29.4 85.0 12.4 .0159 .436 <u>.859</u> 1.894 2,8863 41.053 29.219 415.0 3,2.6 29.4 70.550 84.9 19.5 .0251 690 1.355 2.995 4.9601 29.174 414.7 3:2.5 29.4 64.8 24.1 .0310 .850 1.674 3.691 6.4431 91,642 29.128 414.5 3:2.5 29.3 84.7 28.8 .0371 1.017 2.004 4.416 8.2288 117.041 29.128 3:2.3 414.5 29.2 84.5 37.5 .0483 1.324 5.747 2.60% 12-0062 170.768 29.083 413.1 302.2 29.1 84.3 46.0 .0593 1.624 3.198 7.051 17.0724 242,826 29.037 413.5 302.3 29.1 84.4 50.1 . (:647 1.769 3.484 7.681 300.346 21.1164 \*\*\* \*\*\* \*\*\* 29.157 414.1 3-2.5 29.3 84.7 .042 • 0 • 1 · i .2 DEVIATIONS

PAGE: 1 DATÉ: 8-31-76

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5

FLOWMETER CONDITIONS

PART 25ER

TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE, FLOW IN REVERSE DIRECTION, TEST SPECIMEN (S/N-025) INLET PRESSURE = 1000 PSIA NOMINAL.

TEST SPECIMEN INLET CONDITIONS

"	****	FLOWMLTER ONE	***	### <b>#####</b> ##	FLOWMETER TWO	****			4 page 4 had	J
	FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG: F)	FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	TEMP (DEG. F)	FLOW RATE (ACFM)	
	•84	49.7	66.3	•90	47.8	71.5	1000.0	68.9	.0423	_
	•76	50.2	65+8	•81	48.5	71 • 1	1904.0	68+4	.0387	
ı	•67	, pr.5	65•5	•71	48.7	70.5	1000.0	68 <u>*</u> 0	•0340	
	•59	49.9	65.6	•61	48.7	70.5	1000+0	68 <u>•</u> 1	•0294-	_
	•49	50.1	65.8	•51	49.3	70.6	1000.0	68,2	•0248	Į.
	•40	50°5	66•3	•41	49.7	70.9	1000.0	68 <u>.6</u>	.0203.	
	•30	50.1	67.0	•30	49.9	71.3	1000.0	69,1	.0152	-
	•26	⊅0.1	67.5	•26	49.9	71.5	1000.0	69.5	•012 <u>8</u>	
5	<u>.</u> 21	49 • <u>7</u>	68 <u>•</u> ∙	•51	49,5	71.8	1000.0	69.9	•0103	
	<u>.</u> 13	49.7	69•2	•13	49.7	72.5	1000.0	70,9	• 0065	_
	•13	50.1	7:0 • 3	•13	49.9	73.2	1000.0	71.7	.0065	.il
	•55	49.9	7 - 13	•22	49•5	73.2	1000.0	71.7	.0108	
	•27	49.9	70.0	•27	49.7	73•1	1000.0	71.6	•0134	F.
	•31	49.9	69+9	•31	49.5	73•2	1000.0	71.5	.0155	
;	<b>+40</b>	50.1	69•3	•41	49.5	72+9	1/00.0	71+1	• 0203.	
	•49	49.7	6848	•5)	48.9	72.6	1000.0	70.7	7450•	-
	<b>∙</b> 58	<b>⊅0</b> •6	68+0	•61	49.5	72•2	1000.0	70.1	• 029B	. 4
	•67	26.1	67 • 4	•71	48.7	71.8	1000.0	69.6	.0342	
	•76	50.1	66•8	•81	48•3	71.2	1000.0	69.0	.0386	_
	•B5	50.2	66±0	•91	48.3	70•5	1000.0	68.3	.0434	

ų

TABLE 49
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 8-31-76

TEST SPECIMEN INLET CONDITIONS

TEST SPECIMEN INLET CONDITIONS

	AVG	AVG	GROSS DIFF. PRESS	GRASS DIFF. PRESS	illo enere		
PRESSUME (PSIA)	TEMP (DEG. F)	FLOW RATE (ACFM)	PRIMARY (PSID)	SECONDARY (PSID)	AVG GROSS DIFF PRESS	DIFF. PRESS	DIFF. PRESS
1000.0	68.9				(PSID)	(PSID)	(PSID)
•		• 9423	140.007	140.007	140.007	-0.000	140.007
1004.0	68.4	.9387	125.469	125,469	125.469	-0.000	125,469
1000.0	68.0	.0340	107,455	107.455	107.455	÷0.000	- 107.455
1000.0	ō8.1	•4294	88.734	89.756	89.245	-0.000	89.246
1000.v	68.2	• 0248	72.031	72,690	72.360	000.0∓	72.361
1000.0	68 <b>.</b> 6	.02n3	56,638	57.520	57.079	0000.00	57.079
1000-ń	69.1	•0152	41,138	41,356	41.247	-0.000	41.247
1000.0	69.5	•0128	33,953	34.099	34.026	=0.000 · ·	34,026
1000.0	69.9	.01/3	26,421	26.457	26.439	<b>⇔0.000</b> -	267439
1000.0	70.9	.0065	15,702	15.687	15.694	-0.000	15.694
1000.0	71.7	.0065	15,818	15,915	15.867	-0:000	Í5.867
1000.0	71.7	.0108	27,580	27.720	27.650	-0.000	27.650
1000.9	71.6	.n134	35,575	35.768	35.672	-0.000	35,672
1000.0	71.5	• 1 <b>1</b> 55	42,239	42.394	42,316	-0.000	42.317
1000-0	71.1	.0203	56,764	57 <b>.</b> 520	57.142	÷0.000 ····	57,142
1000.0	70.7	.0247	72,031	72.690	72,360	=0.000	72,361
1000.0	70.1	.0298	90.078	91.020	90.549	+0.000 ··· ···	90.549
1000.0	69.6	.0342	107.455	107.455	107.455	#0.00σ =	107.455
1000.0	59.0	-0386	124.837	124.837	124.837	=0:000	
1000.0	68.3	• n434	144,748	144.748	144.748		124,837
		• • • •		174170	**** ( 45	<b>-0.000</b> ~	1444748

JARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM)\*\*2 +

O (ACFM)\*\*

PAGE: 3 DATE: 8=31-76

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5

PART 25ER

TEST DESCRIPTION

CLEAN CONDITION — FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. FLOW IN REVERSE
DIRECTION. TEST-SPECIMEN (S/N 025) INLETPRESSURE = 1000 PSIA NOMINAL.

# TEST SPECIMEN INLET CONDITIONS

TNET DIPPERENTIAL PRESS

PRESS	URE ########	***	TEMPERATURE	***	***	****	FLOW RATE	***	*****		
kg∕sg cm	PSIA	DEG. K	DEG. C	DEĢ. F	LITERS/ MIN	AÇFM	SCFM	ĸ <u>ĕ</u> `Hĸ ĕńs	- GN2	DIFFERENTIAL	PSID
70.307	1000.0	293.7	20.5	68.9	81.7	•9423	2.884	5.678	12:518	9.8435	140.007
70 <u>•</u> 586	1004.0	293.4	20.2	68.4	75.0	.0387	2.649	5.216	114499	8.8214	125-469
70.307	1000.0	293,2	20.0	68.0	65•8	.0340	2.324	4.576	104088	7.5548	107.455
70.307	1000.0	293.2	0.05	68.1	56.9	.0294	2.008	3.954	8 • 717	6.2746	89,246
70.307	1000.0	293.3	20.1	68.2	47•9	•n248	1.693	3•333	7.348	5+0875	72.361
70.307	1000.0	293.5	20.3	68.6	39•2	.0203	1.384	2.724	6,006	4.0131	57.079
70.307	1000.0	293.8	20.6	69.1	29.3	•0152	1,033	2.034	4.485	2.9000	41.247
70.307	1000.0	294.0	20.8	69.5	24 • 8	.0128	.874	1.722	3,795	2,3923	34,026
70.307	1000.9	294.2	21.1	69,9	19•9	.0103	.701	1*387	34044	1,8589	26,439
70.307	1000 . u	294.7	21.6	70.9	12.4	.0065	•439	• 865	1 <u>.</u> 906	1.1034	15,694
70.307	1000.0	295.2	22.1	71.7	12.4	•1065	.438	<u>.</u> 863	1.902	1.1155	15,867
70.367	1000-0	295.2	22.1	71.7	20 <u>•</u> 7	•0108	. 732	1,441	3,176	1.9440	27,650
70:307	1000.0	295,1	22.0	71.6	25.7	-0134	•907	1.787	3,939,	2-5080	351672
70 <u>•</u> 307	1000.0	295.1	22.0	71.5	29 <u>•</u> 8	•0155	1.051	2.070	4.563	2-9752	42,317
70.307	1000°ñ	294.9	21.7	71.1	39.0	•0503	1.378	2.713	5,981	4.0175	57.142
70.307	1000•0	294.7	21.5	70.7	47,5	•n247	1.678	3.303	7•282	5 <u>•</u> 0875	72,361
70,307	1000.0	294.3	21.2	70.1	57 <u>•</u> 3	.0298	2.025	3•38₽	8.792	6.3663	90.549
70,307	1000.0	294.0	20.9	69.6	66•0	.0342	2,330	4.589	10:116	7.5548	107-455
70,307	1000.6	293.7	20.5	69.0	74.5	•0386	2.633	5 <u>•</u> 184	11.428	8.7769	124,837
70.307 #####	1000.0	293.3	20.1	E.86	84 <u>•</u> 0	•0434	2.965	5 <u>•</u> 838	12.870	10-1768	144.748
18ĕ•01	100055	294•1	21.0	69.7			•			<u> </u>	······································
•026	<u>*</u> 4	•6	•6	1.2	DEVIATIONS	S			- ***		

			TEST UNIVEE	5-25 PART		TEST DESCRIPTION	(S/N-02 <del>5) INLET -</del> PI DATA OBTAINED AFTI	SURE. TEST SI RESSURE - 1000 ER REVERSE FLO	PECIMEN D PSIA NOMINAL. DW DATA RUN.
***	***	****	FLOW! ETER	~ONDITIONS	***	104454644664	1EST 5PE ############	CIMEN INLET C	##############
****	FL *******	OWNLTER ONE	4444444	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	FLOWMETER TWO	)		. 120	
LOW F	ATÉ M)	PRESSURE (PSIA)	TemP (DEG• F)	FLOW RATE (40FM)	PRESSURE (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG, F)	AVG FLOW RATE (ACFM)
- 86		49.7	<u>69.8</u>		4 <u>7</u> • 8	73.3	1000.0	71.6	•0432:
.78		54	69.2.	81	48.7	72:4	1000.0	70•8	• 0395·
<u>. 69</u>		49.9			48.5	.72• -	1000.0	70-6	.0344
<u>• 60</u>		49.9	69.2		48.7	71.5	1900.n	70.4	.0297
51		5(.1	69.2	•51	49.3	71.5	1 04-0	70+4	•0250
42		<u>5.2</u>	69.3	.41	49.9	72.3	1900.0	<u>70∙8</u>	.0207
32	<b>.</b> .	50.1	69.8	. 31	49.9	73.2	1/100.0	71.5	.0155'
. 27		D4	7-,4	, 26	50.2	74.3	1000.0	72.4	.0132
-55		55	71.0	.21	50.0	74.5	1000.0	72,7	.0106
15		49.9	71.6	.14	49.7	75,2	1:00.0	73,4	.0071
•15		49.9	73.2	• • 13	49.9	77.9	1000.0	75.6	.0070
. 23		49.9	73.7	.22	49.7	77.9	1100.0	75,6	.0114
.26		51.2	73+1	• 25	50•A	77.7	1:00.0	<u> 75.4</u>	•0129·
•32	· ×	49.9	7748	· <u>3</u> ]	49.5	77.4	1:00.0	75-1	.015B
-42	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	49.9	72.2	•41	49.5	77•1	1.00.0	74+6	-0206
•50		ÞJ•1	71.6		49.3	75.7	1^00-0	<u>74∙2</u>	•0250
<u>•</u> 60	-	5. 44_	_7 :9	61	49.5	76.2	1 '00.0	73.6	-0301
69		51.4	7C:1		49.3	75.5	1:00.0	72.7	•0350
.78		50.6	. 69+4	.81	48.9	74.7	1000.0	72.0	•ó396·
.87		50 <u>.1</u>	68.9	•91	48.1	74.0	1000.0	71.5	+0436·

PAGE: 2

DATE: 8-31-76---

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST UMBER 5-25 PART 2541 TEST DESCRIPTION

DATA OBTAINED AFTER REVERSE FLOW DATA RUN.

TEST SPECIMEN INLET COMPLITIONS

1"

11

PRESSURE (PSIA)	7 (0 € € € € € € € € € € € € € € € € € €	VG . FLOW RATE ( CFM)	ĢR∩SS DĬFŕ• PRFŠS -PRIM RY - (PŠĬŌ)	GR SS DIFF. PRESS SECONDARY (PSID)	ĀVĞ GKOSS DIFF. PRESS (PSII')	TARĒ DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)	
1000.0	···71.6·	. 7432	101.766	101,766	101.766	-0.000	101.766	F 2
1000.0	70.8	.4395	90.202 "	91°vS0	90,611	-0,000	90,611	
1000.0	70.6	.ċ344	75,768	76.4ª2	76.125	-0.000	76,126	
1000.4	75.4		62,777	63,525	63,151	-0.000	63,151	4 ;
1094.0	70.4	.0259	51,374	52,147	51.760 1	-0.000	51.761	
1000.0	70.9	, 1217	40 616	- 40.722	40,669	-0.000	40,669	
1000.0	71.5	, u155 ° -	29,202	29,213	29,207	-0.000	29,208	
1000.0	72.4	. 132	24,219	24.221	24.219	<b>→0.000</b>	24.220	******
1000.0	/2.7	.01 6	18.773	18.934	18,843	-0.000	18,803	
1000.0	73.4	· 1071	11.994	11,972	11.983	-0.000	11.983	
1000.0	75.6	.0076	11.994	1229	12. 11	-0.000	12.011	
1000.0	75.6	114	20.511	54.666	20.588	-0.000	20.589	
1000.y	75.4	189	23.698	23,8'8	23.758	=0.000	23.758	
1000.0	75.1	.71587 77	30.071	31,189	30.130	-0.000	30.130	<del></del>
1000.0	- "74.6"	.0276	40.79	40,953	40.871	-0.000	40.872	******
1000.0	74.2	.0251	50.998	51.831	51.414	-0.000	51,415	ti 1
1000.0	73.6	.03e1	64,1129	64,473	64,251	-0,000	64,251	
1000.Ú	72.7	้ กู้กลัธิง	77.26?	77,747	77.504	-0,000	77,504	
1000,0	/2.	กลัยรั	90,324	91,020	90,472	-0,000	90,672	
1000.0	71.5	436	113,662	1 (3,662	103,662	-0.000	103,662	<del></del>

TANE DIFF. F ESS = -1.64000E-04 + -1.28930E-02 (ACFM) + 7.48070E-01 (ACFM)\*\*2 +

					-						PAGE: 3 DATE: 8-31-76	
					FLOW BATE	TABLE 50 VERSUS DIF	ÉFRÉNÍÍAL I	PRESSURÉ "				
			TES	 IT 'U' RER 5-2		ayan diti bana a		F we have been	DIFFERENTI - (S/N 025) -	al pressure. Inlet-pressu	V RATE VERSUS . TEST SPECIMEN JRE-= 1000-PSIA- EVERSE FLOW DATA	NGMINAL;
	***	****	***	TEST SP	ECIMEN INLE	T CONDITION	S ~ ********		****	****	NET OIFFERENT	
	PRES!	SURE *******	្រ និង្គិបស់ទីទីងបំទំង	EMPER TURE	តីទំនំជន់នគន	************	****	FLOW KATE	2422244	****	The state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the s	
.,	- _к <u>е/50_см</u> _	 PSI-	DEG. K		DEG. F	Tite?sy i	<u>.cfm</u>	<u>sçfm</u>	KG/HR	GNS LRS/HR	KG/SO CM DIFFERENTIAL	PSID
	70 <u>•</u> 307	1000 . 4	295.1	22.	71.6	.82.9	. 432	2.929	5.767	12.714	7.1549	161.766
	70.307	1000 •••	294.7	21.5	70.8	. 75:9	.: 395	2.681	. 5.280	11.639	6.3706	90,611
	70.307	1000	294.6	21.5	70.6	66.2	• '344	2,336	4.600	<u> </u>	5.3522	76,126
	70 <u>•</u> 307	1000.	294.5	21.3	70.4	57 <u>•</u> 2	•1°297	2.019	3.976	8 • 7 6 5	4+4400	63,151
	70 <u>•</u> 586	1004. /	294.5	21.3	70.4	48.4	<u>. 4 25/1</u>	1.708	3.364	7.416	3.6391	51.761
1:	70.307	1000 22	294.7	21.6	7,a.s	39.7	•0207	1.403	2.763	6.092	2.8593	40.669
	70.307	1000.	295.1	21.9	71.5	29.8	.0155	1.054	2.076	4.576	2.0535	29.208
	70.307	1000.0	295.4	22,4	72.4	25.4	.0132	.896	1.765	3.890	1.7028	24,220
	70.307	1000.0	295.8	55.6	72.7	20.3	.0106	.717	1.412	3.112	1,3220	i8.803
	70.307	1000.4	296.2	23,7	73,4	13.5	•0071	.478	•942	2•176	.8425	<u> 11.983'</u>
	70,307	1000.0	297.4	24,2_	75,6	13.4	.0070	<u>. 474</u>	<u>•934</u>	2.058	.8445	ī2.011
l,	70.307	1000	297.4	24.2	75.6	21.7	. 114	.767	1,511	3.331	1,4475	20.589
	70,307	1000.4	297,3	24.1	75.4	24.7	- 129	.871	1.714	3.779	1,6704	23,758
	70,307	1000.4	. 297.1	<u>24 - r</u>	75.1	30.2	•0158	1.066	2.100	4.630	2.1184	30.130
	70.307	1000.	296.8	73.7	74.6	39•3	•0206	1.388	2.734	6•à27	2.8736	40.672
	70 <u>.307</u>	1000.	_296.6	23.4	74.2	47.7	<u> </u>	1.685	3.317	7.314	3,6148	Śì.415
-	70.307	1000	296.3	23.1	73.6	57 • 7	• 1311	2.037	4 • + 11	8 • 8 4 2	4.5173	64.251
.L-	70.307	1000+.	295.8	55.4	72.7	67+1	• J35g	2.370	4.667	10.289	5.4491	77.504
	70.307	100000	295.4	55.5	72.:	76-0	•6396	2,682	5.282	11-644	6.3749	90.672
	70.307 #####	1000 · · · · · · · · · · · · · · · · · ·	295.1	21.9 \$\$\$\$\$\$	71.5	83.8	•=436	2,958	5.824	12+841	7•2882	103-662
.1-	70.321	1000.2	295.9	27.6	72.7	·	······································	<del></del>				<del></del>

DEVIATIONS

						DA DA	GE: 1 ATE: 9-15-76	
			SI OM DAT	TABLE 51	RENTIAL PRESSURE	CLEAN CONDITION - I	LOW RATE VERSUS	DIFFERENTIAL PRESSUR
			FCOW RM	E AÉKSOS DILLE	WENTER PRESSONE	DATA ACQUIRED WITH	FLOW IN THE REV	ERSE (S/N SIDE DOWNST ) INLET PRESSURE =
		TEST NUMBE	R 12 PART	288 <u>Ř</u>	ŢEST_DĘŚCRIPŢION_	415 PSTA (NOMINAL),		, 11111 1111000111
444444444	****	FLOWMETER	CONDITIONS	************	***	TEST SPE	CIMEN: INLET C	ONDITIONS.
٠,	FLOWMETER ONE		• •	FLOWMETER TWO	,	, , , ,	71.	· · · · · · · · · · · · · · · · · · ·
****	*****	****	***	****	***		AVG	AVG.
(VČEM) FOM BYTE	(ŠŽÍV) bkřžžnuř	TEMP (DEG + F)	FLOW RATE (ACEM)	PRESSURE (PS[A)	TEMP (DEG. F)	PRESSURE (PSIA)	TEMP. (DEG. E)	FLOW RATE (ACEN)
60		77 - 0	-60	48.9	78,1	419.5	77.5	.070 <u>6</u> :
50	bų 4	77.0	•50	49.5	78.6	<u> </u>	77.5	•0599'
41	49.5	77.1	•41	48.7	78.1	418.8	77.6	0483:
<u>.</u> 31	24.2	77.3	•30	49.9	78.2	418.8	77 <u>.8</u>	0386.
26	52.4	77-3	.25	.50.1	78.3	418.8	77.8	.0308
21	49.9	77 <u>•</u> 5	.20	49.5	78.4	418.8	77.9	, <u>, , , , , , , , , , , , , , , , , , </u>
14	49.7	77 • 7	<del></del>	49.3	78.5	418.8	78.1	•0jé <u>3</u> :
14	49.5	.78 <u>a</u>	.13	49.3	78.6	418.8	78.3	
. 22	54,1	78:1	.21	49,7	78+7	418.8		-05ej
.26	<u>5,</u> ,2		.25		78.6	418.2	78.4:	0305
32	<u>⇒,4</u>	78:3	.31	49.9	78.6	418+2	78.4	0374
<u>•</u> 41		79±3	.40	49.5	78.7	<u> </u>	78.5	-048 <u>6</u> :
<u>.</u> 50	5₫.6	78+3	.54	49.9	78.6	417.5	78 <sub>2</sub> 5'	*•••••
260	<u> </u>	78-4	-60	49.5	78,7	416.9	78 <u>+</u> 5:	•0.455:
						<u> </u>		
								· · · · · · · · · · · · · · · · · · ·
	·····				, , , , , , , , , , , , , , , , , , ,	-		1
	<del> </del>							

PAGE: 2 DATE: 9-15-76

TABLE 51

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. DATA ACQUIRED WITH FLOW IN THE REVERSE (S/N SIDE DOWNSTREAM)
DIRECTION. TEST SPECIMEN (S/N 028) INLET FRESSURE =
415 PSIA (NOMINAL).

TEST NUMBER 12

TEST DESCRIPTION PART 28BR

TEST SPECIMEN INLET CONDITIONS

PRESSURE	AVG TEMP	AVG FLOW RATE	DIFF. PRESS	GROSS DIFF. PRESS SECONDARY	AVG GRUSS DIEF. PRESS	TARE:	NET PRESS
(PŠIA)	(DÊG. F)	(ACFM)	(PŽID)	(pSID)	(bàiồ)	(PŠĻĎ)	(Psto)
419.5	77.5	•07.6	268,199	268,199	268.199	•001	268-198
419,5	17.5	• 11549	200,334	201.334	200.334	•000	500 • 333′
418.8	77.6	<b>- ₁4</b> ₿3	144,779	144.779 ,	144.779	•000	144,778
418.8	77.8	• ù369	101,850	101.450	101.850	•000	101.850
418.8	77.8	8, 80.	80,972	81.964	81.468	•000	B1.467
418.8	?7.9	. 247	62,532	63,341	62.936	•000	62,936
418.6	78+1	.0163	38,991	39.800	39,395	=0.000	3953941
418.8	78,3	. 163	38,865	39.627	39.246	<b>40.000</b>	39°, 246:
418.0	78.4	261	66,715	67,444	67.080	.000	67,079
418.2	78.4	• 03 '5	79,903	81.017	80,466	.000	80.460
418.2	18.4	•r374	104.060	104.060	104.060	•000	104,059
417.5	(8,5	. 486	145.726	145.726	145.726	•000	145,725
417.5	78.5	•0600	199,071	199.071	199.071	•000	199.070
416.9	78.5	• . 722	287,453	287.453	287.453	•001	287.453

TARE DIFF, TRESS = -3,40000E-05 + -4,44000E-04 (ACFM) + 1,50933E-01 (ACFM) +2 +-0 (ACFM)\*\*\*3

PAGE: DATE: 9-15-76 TABLE 51 CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED WITH FLOW IN THE REVERSE (S/N SIDE DOWNSTREAM) DIRECTION. TEST SPECIMEN (S/N 028) INLET PRESSURE = 415 PSIA (NOMINAL). TEST DESCRIPTION TEST\_NUMBER 12 PART 2888 NET DIFFERENTIAL! PRESS' FLOW RATE IEMPERATURE PRESSURE \*\*\*\* \*\*\*\* KB/SQ CM DIFFERENTIAL LITERS/ GNZ KĞZHK PSID: DEG. F MIN .CFM SCFM LBS/HR DEG. C KG/SQ CM PSIA DEG. K 3.909 258:198 8.618 18.8562 .0706 1.985 29,493 419.5 298.5 25.3 77.5 56.2 200.333 1.687 3.321 7.322 14.0846 599 29.493 419.5 298.4 25.3 77.5 47.8 144,778 1.357 2.671 5,889 10.1789 418.0 298.5 25.3 77.6 38.4 483 29.447 101.850 298.6 77.8 29.3 · 369 1.035 2.039 4.495 7.1607 418.0 25.4 29.447 ·5.7277 866 1.704 3,757 81.467 -415.0 298.6 25.5 77.8 24.5 . v308 29.447 692 1.363 3.004 4,4248 62,935 . 247 418.0 298.7 25.5 77.9 19.6 29.447 39.394 457 .90v 1.985 2.7697 418.0 78.1 12.9 · 163 298.8 25.6 29.447 898 1.980 2.7592 39,245 456 29.447 416.5 298.9 25.7 78.3 12.9 . 163 731 1.439 3,173 67.079 .1261 -4.7161 29.447 416.0 298.9 25.8 78.4 20.7 1.679 853 5,6569 80.460 29.402 410.6 298.9 25.8 78.4 24.1 .0305 3.702 298.9 25.8 78.4 29.1 .,374 1.047 2.062 4.547 7.3161 104.059 29.402 413.4 417.5 299. 25.8 78.5 38.5 ...486 1.358 2.674 5.896 10-2455 145.725: 29.356 7.276 199.070 29.356 417.5 299.0 25.8 78.5 47.5 -1600 1.676 3 30 U 13.9960 287:453. 29,311 2722 2.016 3.970 8.752 20-2099 299. 25.8 78.5 57.1 \*\*\*\* \*\*\* \*\*\* \*\*\* \*\*\* 78.1 29.425 418.5 298.8 25.6 042 . 0 . 2 . 2 .3 DEVIATIONS

							GE: 1 TE: 9-15-76	
			FLOV RAT	TABLE 52 E VELSUS OIFFE	RENTIAL PRESSURE	DATA ACQUIRED WITH	FLOW IN THE REVE	DIFFERENTIAL PRESSUR RSE (S/N SIDE DOWNST
		TEST UMBI	ER 12 PART	PRAK	TEST DESCRIPTION	DIRECTION. TEST SP 1000 PSIA (NOMINAL)		INLET PRESSURE
			R CONDITIONS			TEST SPE	CIMEN INLET C	ONDITIONS
	7.7		**********			пискинаван		
****	FLOWNELEH ONF	****	****	FLOV'METER TWO	<u> </u>		AVG	AVG
LOW RATE	PRESSURE	T (ህP (ህርዓል E)	FLOW R.TE	PRESSUR.	TEMP (DEG. E)	PRESSURE (OSIA)	TEMP (DEG. E)	FLOW RATE (AÇEM)
86	50 <u>c</u>	72,	9.1	48,0	77.3	1007.9	74.7	.0430
<u> </u>	49.9	71.	.81	48 6	76.3	1 07.9	73_6	0385:
69	De.1	71.8	.7,		75.9	1 07.9	73,3	.03A1
	50.2	75		<u>94.1</u>	75.7	1.04.0	73_2	.0297
<u>.50</u>	49.7	718			75.7	1.104.0	73,3	0246
<u></u>	99.9	73.1		19.2	75.8	1::07.9	73.4	<u> </u>
<u>.31</u>	311.4	71.5	36	49.9	76.0	1.04.0	73_8	<u>•0158</u> .
.26	49.9	70.	.25	49.5	16.2	1 04-0	74-1	-012 <u>7</u>
- · -21	bu.l	7241	.2	49.7	76.4	1904-0	74.5	_0103
.14	90-1	73•3	.13	49.7	76.8	1.04.0	75.0	*0065
.14	911.6	74+)	.13	<u> </u>	77.1	1/04.0	75.6	•0069 <sup>(</sup>
.22	5,,2	73.9	•21	49.9	77.0	1004.0	75.5	,010 <u>7</u> .
26	50.4	73.7	. 25	49.9	77	1 04.0	75.3	0127
.31	5 L 4	73.2	.31	49.9	76.8	1 04.0	75.0	,0155
<u>-40</u>	5 ( <u>2</u>	75.5		49.7	76.5	1.04.0	74-6	0,195,
49	56.6	7a.	.49	49.3	75.2	1 04.0	74.1	0245
59	b; 4	71.1	65.	49.2	75.7	1 00.0	73.4	<u>.0296</u>
69	B( .]	. 7	.70	48.8	75.1	1_00_0	72.7	<u>n343</u>
•77	5, 1	65.5		<u> </u>	74.4	1 00.0	71.9	•0388 •
.87	37.2	65+3	1.0	48.2	73.4	1_00.0	70 <u>•</u> 9	0437

PAGE: 2 DATE: 9-15-76

TABLE 52

FLOW PATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. DATA ACQUIRED WITH FLOW IN THE REVERSE (S/N SIDE DOWNSTREAM) DIRECTION. TEST SPECIMEN (S/N 028) INLET PRESSURE = 1000 PSIA (NOMINAL).

0 (ACFM)##3

T ST ULBER 12 PART 28AR TEST DESCRIPTION

<u>Test</u>	PAFI YMEN	INLET	COBITI	. JV2
***	*****	计设计符件公司	***	***

PRESSURF	4 V G	VG ELON RAJE	DIFF. FRESS	UIFF. PRESS SECONDARY	AVG GRUSS DIFF. PRESS (PSIQ)	TARE DIFF. PRESS	NET' OTEF. PRESS
TPSTAT	(ÞĒĢ. F)	(. Crh)	(עַנַּבּק)	(PSID)	์ ได้เร็ส <u>)</u>	(PSID)	(FSID)
1007.5	14.7	.0409	127,654	12.,394	120,684	<b>-0.000</b>	120,684
1007.7	/3 <u>•</u> 6	385	1.6.164	1 6.154	106.164	-0.000	106,164
1007.5	(3,3	. 341	89,914	91,544	90.775	~0.000	90.779
1004.0	5.61	. 2 <sup>4</sup> 7	70.879	77.755	77.317.	#0.000	77.317
1004 <u>.</u> ų	73.3	. 246	62,615	63,236	62.925	<b>→0.000</b>	62.925
1007.5	13.4	. 197	48,949	49,978	49,464	<b>~0.000</b>	49,464
1004.0	(3+8	.<152	J6.943	37.668	37.307	-0.000	37,307
1004.0	(4.1	-147	30.19.	31,936	30+563	-0.000	30.563.
1004.0	14.5	.01 3	24.567	24.521	24.594	<b>™0±000</b>	24.594
1004.0	/5°.	* tet roð	15.872	15.915	15.895	=0.000	15.896
1004.0	/5 <u>.</u> 6	. 11: 69	16.165	16.259	16.212	<b>~0.00</b> 0	16•sis
1004.0	15.5	.01 7	25,32:	25,481	25.401	<b>~0.00</b> 0	25.401
1004.0	15.3	• :127	30.19/	33.879	30,534	=0 <u>=</u> 000	30,535:
1004.0	15.(	. 155	37.447	36.244	37.845	<b>~</b> 0.000	37.845
1004.0	(4.6	. 159	49.574	5 .294	49.934	-0.000	49.934
1004.0	<u>[4</u> :1	. 245	62.615	63,551	63, 183	<b>~0.000</b>	63,083
Ĭ 0 0 0 • 0	13.4	• 5A¢	77.119	78,387	77.753	-0.000	77,759
j000°a	12.7	. 1343	94,713	92,947	91.810	<b>=0.00</b>	91.810
1000.0	4T•a	. 368	1:6.795	1, 6,795	106.795	#0.000	106,796
1000.0	10.9	. 0437	123.249	123,2,9	123.209	-0.000	153.510

THRE DIFF. PRESS = -1.64000E-04 + -1.2693JE-02 (ACFM) + 2.48070E-01 (ACFM)##2 +

PAGE: 3 DATE: 9-15-76 TABLE 52 CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED WITH FLOW IN THE REVERSE (S/N SIDE DOWNSTRE DIRECTION. TEST SPECIMEN (S/N 028) INLET PRESSURE = TEST DESCRIPTION 1000 PSIA (NOMINAL). TEST NUMBER 12 PART 28AR NET DIFFERENTIALI PRESS: TEST SPECIMEN INLET CONDITIONS **你我看你我我我我我我我我我我我我我我我我我我我我我我我我我我我我我我的我的我们的我们的人,我们我们的我们的我们的我们的我我的我的我的,我们我们我们的我们的人们的人们的人** PRESSURE (FNPERATURE FLOW RATE \*\*\*\* \*\*\*\* \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* KG/SQ: CMI DIFFERENTIALI ĸ<u>ĕ</u>∖₩Ĥ LITERS/ PS LOI KB/SQ CM PSIA **ACFM** SCFM LB5/HR DEG. K JEG. C DEG. F MIN 120-684 2.922 5.753 12:683 8-485n 1007.× 74.7 82.7 0430 70.865 296.9 23.7 56167 15.391 7,4641 106-164 1007.9 296.3 23.1 <u> 4385</u> 2.624 70.865 73.6 74.3 4,571 90.779 1007.4 10:077 6.3824 701865 73.3 65.7 <u> 1341</u> 2.321 296.1 23.0 3,968 77:317: 57 - 1 8.749 5-4359 296.0 22.9 73.2 .0297 2.015 70,586 1004 • 9 <u> 6246</u> 1.667 3.282 7.236 62: 925! <u>4-4241</u> 70:586 1004.0 296. 22.9 73.3 47.2 3,4777 0197 2.642 5.824 4014641 70.865 1007.4 296.7 23.0 38\_0 1.342 37,307 70:586 296.4 2:031 2::6230 1004-9 23.2 73.8 29.2 1.031 4.477 30.2563 70.586 296.6 23.4 74.1 24.4 27لىي .862 1-698 9-742 2.148B 1004.4 19.8 1,377 9-037 1.7291 24.594 23.6 0103 700 70,586 1004... 296\_8 74.5 23.9 <u> 1915 - ا</u> 111176 15.8961 70:586 1004.0 297.1 75.0 <u>13.</u>} 464 3-015 924 2.033 1,1398 16.342 75.6 13.3 -0069 .468 70:586 297.4 24.2 1004-6 1:420 1004-0 3-130 1.7859 25 401 70.586 297.3 75.5 20.4 0107 **,721** <del>24 \$</del> 1.688 35,595 857 70<u>±586</u> 1004.4 297,2 24.1 75.3 24.3 <u>...127</u> 3.720 <u>2.1468</u> 17.845 4.542 2-6608 704586 نىي<u>4004</u> 297.4 23.4 75.6 29.6 -0155 1.046 بهوميع 2,656 491934 70.586 596\*8 23.7 18.2 <u>199س</u> 1.349 9.055 3.5307 بعيوند 3,275 4.4852 <u> 586 ۽ 70</u> 1004.3 <u> 296.5</u> 23.4 74.1 47.1 <u> 1245</u> 1.663 7.221 63: 088. 73.4 56.7 <u>• 0296</u> 3.946 8-69n 774753. 70.307 1000-0 296.2 23.4 2.002 5-4666 705307 295.8 4,574 22.6 72.7 2,323 10.084 <u> 6-4549</u> <u>-91-810-</u> 100040 هيخم 343 نام <del>70<u>;3</u>07</del> 5,180 14.420 <u> 1067338</u> 71.9 . 038E 2,631 <u>7\_5085:</u> 1406+6 295.3 22.2 74.5 5,839 70:307 294.8 70.9 123, 230. 21.6 84-0 0437 2.966 12.874 8-6625 1000-0 \*\*\*\* \*\*\* \*\*\*\* \*\*\* \*\*\* 70.586 1004.9 296.4 23.3 73.9 •115 1.9 .5 ,5 .9 DEVIATIONS

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PARŤ ∌B

PAGE: 1 DATE: 7/23/76

CLEAN CONDITION-FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. BEFORE PROOF TEST.
TEST DFSCRIPTION TEST SPECIMEN (S/N 023) INLET PRESSURE = 415 FSIA (NOMIBAL)

TEST HULBER 6

ŢĘSŤ SPĘĆIMEN INCEŤ ČONDĨŤŤONS

			•	****	Fi Odwitter Two	***	***	FLOW- TEP ONE	*******
5	ĂVĠ Flow Rāțe (ăcpa)	ÄVG TEMP (neg. F)	PRFSSUŘÉ (PSÍŽ)	TEMP (DEG. F)	PRESSURE.	FLOW RITE (ACFH)	ŤcMP (Ngć. F)	PRESSURE	FLOW RATE (ACFM)
	,0567	á3. ő	<b>∳</b> ž1•n	-4,5	49.9	.42	~ޕ5	50.4	.47
	• ຄື5ຂັ7	Ŕ3∗Ī	4āī.ă	97.6	Ã8.9	• 45	8 +6	49.7	• 45
	.0476	e3• ī	421.2	33.6	49.9	• 4.:	83.6	5n . 4	.40
	.0425	ล์3•โ	451.5	93.7	ទំព•∽	• 35	¤ •€	8 و 115	•36
 	.0368	ēj.ž	42ī.ž	93.7	50.2	.31	22.6	<b>50.6</b>	•31
"	, 0306	ěã,ž	42ĭ.2	Դৰ•ুβ	49.Q	,56	R>+6	p. • 5	•26
	.0249	83.2	451.5	83.7	50.3	.51	95.÷7	50.4	•51
••	,0188	คือ, อึ	4ēĭ.≅	43 <b>.</b> 8	Šn.4	. 75	વકે.ક	50.6	.16
-	.0132	ĀŠ.Š	4žī.ž	83.8	5.1	•11	ષર્ગ 🛪 છ	5. *S	•12
• -	,0133	ล์ช์.4	4žĩ.á	43.9	50.4	.11	89.R	50.4	•12
,	. 0189	ė3.3	421.a	43.9	49.9	• <sup>11</sup> 6	8 <b>⊅</b> +7	5. •1	.16
- 1	.ñžšī	83.ž	45ĩ.ñ	rd.9	49.9	.51	8=+6	50.1	.21
<del>-</del> -	.0306	á3 <b>,</b> 1	421.2	ค์รั <sub>ง</sub> ส	49.3	. 76	85.5	49.7	.26
	.0961	63.1	4žī.ž	73.B	49.9	•31	95.3	50.1	•31
	.0419	ēġ.ō	āī.ă	83.7	:9 <b>.</b> 5	•35	92.3	16.1	<b>.</b> 36
<b>_</b>	,0475	83,0	420.5	93.7	49.3	.40	92.3	49.9	•4ព
- ,	. 6526	ñž.9	419.9	A3.6	49.7	• 44	A +3	49.9	•44
- 1	• 0565	ěž.9	419.9	9	49.7	• 48	82.4	49,9	<b>.</b> 48

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7/23/76

CLEAN CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE. BEFORE PROOF PRESSURE TEST TEST HUMBER 6 PART 58 TEST DESCRIPTION TEST SPECIMEN (S/N 023) INLET PRESSURE = 415 PSIA (NOMINAL) TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\* ł: 3R-55 \_gRnSs TVG GROSS ΔVG T€MP TVG FLOW RATE DIFE. PRESS DIFF. PRESS SECONDARY DIFF. PRESS DIFF. PRESS PRESSURE (PSIA) (DEG. F) (ACFM) (PSiD) (PSiD) (PSID) (PSID) 421.8 299.869 83... . 6567 299.869 299.869 299.869 . .āoò .òoô \_\_\_\_258\_203\_\_\_ ∾3•1 421.2 • 15 -7 258.203 258.203 258.203 421.4 .6476 213.380 213,395 213,380 \_ .213.360\_ 83.1 .00ô \_ ĭ6ō.5ŠŽ. 421.2 83. ī • 3425 191.553 181.553 180,553 •000 146.146 421.2 83.0 .0368 146.147 146.147 146.14 .000 421.2 83.2 .0306 115 844 115.844 115.844 .000 115'-844. 421.2 Á9.271 .3.2 .0249 88.899 39.645 89,272 .000 421.2 .5188 64.322 . 64.673... 83.3 65.024 64.673 .000 421.4 A3.3 ·; 132 44.76-44.57 44.631 -ò.òoo ÃÃ, 630 421.8 83.4 .1133 43 210 42.945 43.078 -0.000 ¥3.077 63.629 421.8 93.3 . 189 63.321 64.077 63.699 ەًە و 87.906 87.916 421.4 83.2 . 251 87.429 88.382 .000 EDO.EII 421.2 ĨĨ3,003 113.003 .000 87.1 <u>.0306</u> 113.103 144.252 421.2 144.253 144,253 .000 93.1 44.253 . 361 Ĩ76.76š 421.6 83.6 .0419 176,765 176.765 176,765 ..000 214.958 214 959 214,959 420.5 83.0 . 4475 214.959 • QQQ 252.246 252.208 419.9 R2.9 .1521 252.266 252.200 .000 419.9 82.9 .1565 299.869 299.8/9 299,849 .000 292.869 PARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM) +2 +

PAGE: 3 DATE: 7/23/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION-FLOW RATE VERBUS DIFFERENTIAL

PRESSURE BEFORE PROOF PRESSURE TEST.

TEST DESCRIPTION TEST SPECIMEN (S/N 023) INLET PRESSURE = 415 PSIA (NOMINAL) TEST NUMBER 6 PART 58

	***	***	***			ET CONDITIONS			***	***	ŅĘŤ DIĘFĖŘĖNŤ	TĂĽI PRESS
Ŀ	PRESSŲ ė̀#ė́########			TFMPERITURE	***	***	*******	FLOW RATE	***	**********		
	KG/SQ CM	PSIA	DEG. K	DEG. C	DEG. F	LITERS/ Min	CFM	·SCFM	KĞ∕HĞ ĞNS	CAS/HR	KG/SQ ČM DIFFERENTIAL	PSID
	ž9,658	421,8	311.5	28.3	83.0	45 <b>.</b> 1	.456 <b>7</b>	1.588	3.127	6.894	21.0829	299° 869
	29.612	421.2	3 1.5	29.4	83.1	41.6	527	1.474	2.962	6.398	18.1534	250,203
	29.612	421.2	301.5	54.4	83.1	37.5	· 0476	1,330	2.6jē	5• <b>7</b> 72	15.0021	213, 380
ì,	ž9,612	421.2	361.6	2P.4	83.1	33.4	.^425	i.ia9	2,341	<b>5.</b> 161	12,6941	160.552
	29.612	421.4	3 1.6	20.4	83.2	28.9	.^368	1.028	2.025	4.464	10.2751	1466 146
	29.612	421.4	-01.6	29.5	84.2	24.0	.0=06	.855	1.684	á•712	8.1446	115'-844
	29.612	421,2	301.6	28,5	83.8	19.5	. 24°9	.696	1.371	3.ñžž	6,2764	89',271
	ž9,612	421.2	361.7	29.5	83.3	14.6	•1188	•525	1.034	ž.ž79	4.5476	64,673
	ā9.612	421.2	3'1.7	24.5	83.3	15.0	•4132	.369	•727	ī•6ñ3	3,1378	44.630
ı	ž9,658	421.8	3ñ1.7	-8.6	83.4	ī ā.1	•อมีจร	.iñī	.731	1.615	3.0286	43.077
	29,658	421,6	341.7	28,5	83 <b>.</b> 3	14.8	.n[89	.53n	1.044	2•30Ž	4,4785	63,699
	29,658	421.6	3 1.6	28.5	83.2	19.7	• ^25 î	.Toz	1.303	3 • ñ 4 8	6.ĪĖnĀ	87.906
	59,612	421.2	3.11E	nR•4	83.1	54.n	.0306	<b>.</b> 857	i.68?	3.718	7.9449	113.003
	ž9,612	421,2	3/1,5	2a.4	83.1	28.5	<u>.</u> 136]	1.010	1.989	4.386	10.1419	144.252
	ž9,612	421.2	3 1.5	E, AS	eà.A	3ž.9	. 419	ī.ī7ī	2.3ñ6	5.185	12.4278	176.764
ŧ	₹9 <b>.</b> 567	420.5	301.5	∌ŕ•3	83.ñ	37.4	•0475	1.326	2.6 <u>1</u> 1	5.756	15.1131	214.758
	29 <b>.</b> 521	419.9	301.5	Ē, PŜ	82.9	4 n . B	.0\$2c	1.449	2.853	6.291	17.7318	252,205
	29.521	419• <sup>9</sup> ****	3 1.5 *****	E.PS BRŠBRB	62.9	44.5	• 4565	1.575	3.102	6.839	21.0829	299,869
	29 <b>.</b> 610	421,6	361,6	28.4	83.1							
	.025	٤.	•1	•1	•1	DEVÍATIONS	3				Will Brown for the	

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 7/23/76

TEST NUMBER 6 PART SA

CLEAN CONDITION-PLOW RATE VERSUS DIFFERENTIAL
PRESSURE. BEFORE PROOF PRESSURE TEST
TEST DESCRIPTION TEST SPECIMEN (5/N 023) INLET PRESSURE = 1000 PSIA (NOMINAL)

	***	***	FLOWMETER *******	R CONDITIONS	****	****	ŤESŤ SPE *******	CIMEN ÎNLET C	ONÖTTTONS:
<b>{</b> ,	***	FLOWMETER ONF	*****	****	FLOWMETER TWO	***	•	. W	
	FLOW RATE	PRESSUPE (PSIA)	TEMP (DEG• F)	FLOW RITE (/CFM)	PRESSURE.	TEMP (DEG. F)	PRESSURE (PSIX)	ÄVG TEMP (DEG. F)	AVG. FLOW BATE (ACFM)
	.83	49.5	₹. ñ÷	.90	47.4	μ <b>λ.2</b>	. 1c11.9	77.2	.0414
	.75	20.5	73•6	.81	ă8.Š	79 <b>.7</b>	i^īī.9	76.6	.0381
	.66	59.1	73•4	,70	48.7	79 <b>.</b> i	i-ō7.9	76.2	.0335
i	.58	49.0	77.3	•67	%8.7	7A.9	1.07.9	76.1	.0288
	.49	49,9	73.8	.50	ă8,9	79.1	înō7.9	76.4	.0241
	.39	49,9	₹Ã.	,40	49.3	-19.4	1~07.9	77.0 -	.0194
	.31	៦0 ឺន	7Å.3	.31	49.9	79.9	1007.9	77,6	, ô152 <sup>-</sup>
	• 25	49.9	76 • Ř	<b>,</b> ⊼5	49.5	B#.6	1007.9	78.5 ~	.0125
	.21	50.1	77•4	oś.	79,9	я <b>д,</b> 9	ĩ c õ 7 . 9	79.0	.õīôž
þ	.14	50.2	77.8	. į 3	50 <b>.</b> 1	81.3	inoř.9	79,5	.0067
	.14	51.1	79∙5	.13	49.9	82.3	ĩ~ô <b>7.</b> 9	ลีถ้•ฺจิ	.0067' y
	•22	50.1	7° • 3	.51	49.9	₽ġ.a	īcīi.9	éō.è	.0106
	.25	59.1	70.1	.25	49.9	ครั. เ	ĭ^īī.9	80.6	.0125
	.31	50.1	78•6	.71	<b>49.9</b>	Ro∎1	ī^ñ7,9	ēñ.4	.0152
	<b>.</b> 40	50.1	<del>7</del> 9 • 8	.40	49.5	9 <b>1.</b> 9	Ĭ~Ö <b>Ť.</b> 9	éō₊ō	.0190
ľ	. 49	54.2	77•2	•\$)	49.5	AŢ.5	ī^ñ <b>7.</b> 9	79.3	.0247
	.58	50.1	76.	•60	/9·Ī	P1.1	ī^őŤ.9	76.7	.0291
	,67	49.9	75.7	, 70	48.5	80.6	1007.9	78,1 <sup>-1</sup>	.0334
	,75	5, 2	74.9	481	48.5	79.9	ĩ·ò7.9	77.4	40381
	.84	49.9	74.2	.91	47.9	79.2	Ĩnñ7.9	76.7	.0424

l.

## TABLE 54

PAGE: 2 DATE: 7/23/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE BEFORE PROOF PRESSURE TEST.

TEST NUMBER 6 PART SA TEST DESCRIPTION TEST S

TEST SPECIMEN (S/N 023) INLET PRESSURE = 1000 FSIA (NOMINAL)

TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*\* dRnSS GRASS TEMP äVG DIFF PRESS JĀVG GROSS. DĪFF. PRESS NET DIFE. PRESS PRESSURE FLOW RATE DIFF, PRESS PRIMARY SECOMOARY DIFF. PRESS (PSIA) (PSID) (DEG. F) (. CFM) (PSID) (P51n) (PSID) 1011.9 77.2 161 4n3 161.4n3 .0414 161.403. . . 161.40<u>3</u> -0.000 76.6 1011.2 • 3381 145.345 145,365 145.355 #Ö. 000 1007.9 76.2 •0315 124.472 124.472 ĪŽĀ.ĀŽŽ 124.472 -0.000 1007.9 76. î \_ô28B 104]902 ĩãt.90Z 104.902 104.902 **#0.000** 1007.7 76.4 . 7241 84.294 85,015 84,655 -0.00ô 1007.9 .0194 77.0 66.283 67.023 66.653 -0.000 1007.9 77.6 .ñī52 55,142 50.925 Šα.534 ŠÕ.Š39 -0.00à 1007.9 78.5 .6125 41 867 41.635 4ï.Ťšī 41.751 -0.000. 1007.9 79.0 .0102 33.494 33.229 33.356 -0.000 1007.9 79.4 <u>. ñ</u> ń 67 21.655 žī šiī 21.4-6 21.530 -0.000 1007.9 50.9 21.468 .op67 21.4.6 21,437 21.437 1011.9 B0 . 8 .0176 34,975 34,839 34.907 -0.000 1011.9 40.6 .6125 ĨŽ. 177 . ž. 679 41.98ï Z2.079 \_\_\_0\_000\_\_\_ 1007.9 \_5i\_94ž 80.4 .ñï52 56\_642 51,241 50.942 1007.9 30 a g . 198 67.847 67.448 68,286 67.847 -0.000 1007.9 79.3 .0247 86.505 87.225 86.865 -5.000 1007.9 78.7 . ō291 Ĭ06.164 106.164 106.164 106-164 -Q.000 1007.9 78.ī . 334 124.788 124.738 124.786 124,788 **-**0.000 1007.9 77.4 .0781 145.621 145.621 ..145.621 .000.000 145.621 1007,9 76.7 .6424 166,769 166,769 166.769

IARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM) +2 +

Ô (ĀĈĒM)♣43

PAGE: 3 DATE: 7/23/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION-FLOW RATE VERSUS DIFFERENTIAL

TEST NUMBER 6 TEST DESCRÍPTION PART ŠA

THE CONTRACT THE LANGE CONTRACTOR

PRESSURE, BEFORE PROOF PRESSURE TEST TEST SPECIMEN (S/N 023) INLET PRESSURE = 1000 PSIA (NOMINAL)

ľ	PRESSU			TEMPER TURE		9696995394 FI COMPTITOR		FLOW RATE		********		*
KG/SG		PSIA	DEG, K	DEG. C	DEG. F	LITERS/ MIN	ACFM	scŕM	ĸã∕Hϗ	GŃŻ LasyHR	KG/SQ ČM DIFFERENTIÄL	PSID
Ť1.	144	1:11:9	298,3	28.1	7Ť.2	8 <u>7</u> •1	• 1414	2.812	5 <b>.</b> 537	12.206	11.3478	161.203
<b>71.</b>	144	1011.9	597.9	÷4.8	76.6	74.7	.138i	2.589	5.098	ĨĨ• <u>ż</u> 4Ō	10.2160	145,305
70.	865	1007.9	297.7	24.6	76.2	65.3	.0335	2.269	4.467	9.848	8,7513	124,472
70.	865	1107.9	297.6	24.5	76.1	55.8	• 280	1.952	3.643	6.472	7.3753	104,902
<b>70.</b>	865	1007.9	597.8	24.7	76.4	46•4	• * 241	1.634	3.718	7.594	5.9518	84,655
<b>70.</b>	865	1007,9	298.2	25.0	77.0	37.4	.0194	1.315	2,590	5.710	4,6862	66,653
70.	865	1107.5	298.5	25.4	77.6	36°t	.1152	1.125	2.nî9	4.451	3,5529	50.534
<b>7</b> 0.	865	1007.9	399,0	35.B	78.5	23.7	• 1 <b>1</b> 25	.842	1.658	3.655	2,9354	41.751
Ť٥.	865	1007.9	299.3	26,1	79.4	19.3	•0īe2	,688	1 • 354	2.986	2.3452	33,356
70.	865	1007.9	299.6	26.4	79.5	j2.6	• >067	<b>.</b> 453	.892	j.966	1.5138	21.531
<b>70.</b>	865	1007.5	300.3	27.2	8ń.9	12.5	. 2067	• 45ñ	.886	î•954	1.5 <sub>0</sub> 72	21.237
<del>7</del> 1.	.144	1011.9	300.3	27.1	86.8	25.1	.vinA	.7i4	1-466	3.799	2.4542	34.908
<b>71</b> .	144	1011.9	300.2	27.1	85.6	24.0	.0ĭ25	. B46	1.667	3.674	2.9585	42.079
70.	.865	1007.5	300.0	24.9	81.4	29•0	.ŋĬ52	1.024	2.016	4.445	3.5816	50.942
<b>7</b> 0.	.865	1407.9	299.8	≈6 <b>.</b> 6	8ñ.n	37•8	•nī98	1.330	2.612	š.774	4.7761	67.047
ľ 70.	,865	1007.9	299.5	26.3	79.3	47,3	. 24Ť	1.661	3.271	7.211	6,1673	86, 865
žn•	865	1007.9	299 • 1	26.4	78,7	56.3	• -291	1.965	3.869	8.529	7.4641	166.164
<u>.</u> 70	865	1007.9	298.8	<sub>7</sub> 5•6	78 <b>.</b> ī	64.8	• `334	>• <i>5</i> 57	4 • 4 4 5	9.799	8.7735	124.788
Ťο.	865	1407,9	298.4	25,2	77,4	74.7	ī8ėn.	ź.574	5.068	<b>11.17</b> 3	10,2382	145,621
	.865 ****	1 '07. <sup>9</sup>	298 <b>.</b> r	24.H *****	76.7 *****	83.5	. 0424	5.868	5.647	ī2.449	11.7251	166.770
<b>70.</b>	921	1008.	298.0	25.8	78.4							
	.089	1.3	• B	• <b>8</b>	1.4	DEVIATIONS	S					

PAGE: 1 DATE: '9-8-76

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL FRESSURE DATA ACQUIRED AFTER 10-HIGH PRESSURE-

(10,000 PSIA NOMINAL) CN2 IMPACT CYCLES: FLOW IN REVERSE DIRECTION. TEST SPECIMEN (S/N 023)

INLET PRESSURE = 415 PSIA NOMINAL.

#### TABLE 55 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST HUMBER 5

FLOW ETER CONDITIONS

PART 23DR

TEST DESCRIPTION

DATA OBTAINED AFTER PROOF TEST. TEST SPECIMEN INLET CONDITIONS. \*\*\*

FLOWMETER ONE FLOWMETER TWO \*\*\*\*\*\*\*\* \*\*\*\*\*\* \_AVG PRESSURE FLOW RATE FLOW RATE PRESSURE TEMP FLOW HATE PRESSURE TÈMP (DEG. F) (PSIA) (PSIÁ) (DEG. F) (PSIA) (ACFM) (DEG. F) (ACFM) 418.8 90.2 .0624 44.9 .54 48.9 94.9 .52 69.5 418.2 .0598 90.0 .50 50.2 89.3 .51 49.5 96.7 418.2 89.9 .0496 49.7 .41 2.00 89.2 .42 90.7 ,0369 90.4 417.5 89.7 .31 DV.4 .31 50.0 89.0 417.5 89.6 ·0315 90.4 .26 20.4 88.8 .20 50.0 .21 417,5 89.6 .0254 .21 2..4 88.8 50.0 90.4 .0174 69.7 .15 20.2 88.8 .14 50.0 90.5 417,5 89.7 +0175 20.4 .14 50.2 90.5 417.5 . 15 89.0 416.9 89.5 .0272 .23 .23 49.9 90.4 2...2 B8.7 .0315 416.9 .26 51 .4 88.4 .26 50.0 90.2 .0369 416.2 89.1 .31 49.9 88.2 .31 49.5 90.0 88.9 .0480 コリ・エ .40 49.5 89.7 415.6 • 40 88 • 1 88.8 .0600 .51 49.3 39.5 415.6 -50 2002 88•0 88.8\_\_\_\_ .0633 .52 Su.1 88.2 .54 49.1 39.5

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PAGE: 2 DATE: 9-8-76

TABLE 55
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION TEST NUMBER 5 PART 23DR

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW IN REVERSE DIRECTION. TEST SPECIMEN (S/N.023) INLET PRESSURE = 415 PSIA NOMINAL. DATA OBTAINED AFTER PROOF PRESSURE TEST.

TEST SPECIMEN INLET CONDITIONS \*\*\*\*\* GRASS DIFF. PRESS SECONDARY GROSS DIFF. PRESS AVG GROSS DIFF. PRESS NET DIFF. PRESS TARE AVG AVG PRESSURE DIFF. PRESS TEMP FLOW RATE PRIMARY (PS10) (PSID) (PSID) (PSID) (PSTA) (DÊĠ. F) (ACFM) (pSIU) .001 418.0 291.076 291.076 291.075 40.2 .0624 291,076 261.684 261.684 .000 261.683. 418.4 261.684 90.0 .,598 188.046 188,045 .000 188.045 418.4 59.9 . 0496 188.046 125.153 125.153 417.5 89.7 . 369 125,153 125.153 .000 102.398 102,398 ÕOÕ. 102.397 417.5 .4315 102,398 89.6 •00ŏ 78.296 79.011 78.653 78.653. 417.5 59.6 ·#254 .000 417.5 50,918 51.515 51.216 51.216 89.7 . 174 •000 50.793 51,515 51.154 51.153 417.5 89.7 .:175 84-280 .000 416.7 89.5 . 4272 83,862 84.700 84.281 102.081 416.9 89.3 .6315 102.082 102.082 102.082 .00ò 125.785 416.4 59.1 . 369 125.785 125.785 125.785 •000 180.776 180.777 .000 415.0 dB.9 .0480 180.777 180.777 266.424 •00ô 415.0 266.424 266.424 266.424 48.8 .0640 308.774 308.774 .001 308.774 414.7 08.8 .1633 308.774

IARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM) +\*2 +

0 (ACFM) \*\*3

PAGE: DATE:

TABLE 55 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5

PART 23UR

TEST DESCRIPTION .

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE (10,000 PSTA NOMINAL) GN2 IMPACT CYCLES. FLOW IN REVERSE DIRECTION. TEST SPECIMEN (S/N 023) INLET PRESSURE = 415 PSTA NOMINAL. DATA OBTAINED AFTER PROOF PRESSURE TEST.

NET DIFFERENTIAL! PRESS

TEST SPECIMEN INLET CONDITIONS

	PRESSU		*****	LEMPERATURE	***	****	****	FLOW RATE	****	#########		
	Kē∕ēơ ċu	bàta	DEG. K	DEG. C	DEG. F	LTTERS/ MIN	ACFM _	SCFM	™ K₫\Ĥĸ gns	ĞNZLBŞ/HR	KG/SQ-CM DIFFERENŢIAL	PŠĬĎ
	29.44!	410.5	305.5	32.4	90.2	48_5	•0624	1,713	3.374	7.436	20.4646	291 . 075:
	29.402	419.4	3.)5.4	32.2	90.0	46 • 4	. บ59ห	1,640	3°530	7 <u>.</u> 120	18.3982	261,683
4	29•405	41ق•خ	3,05.3	32.2	89.9	38.5	•v496	1,361	2.679	5.906	13-2209	188,045
·	29,356	417.5	3,5.2	32.1	89.7	28.6	• 0369	1.011	1.991	4.390	8,7991	125, 153.
	29.356	417.5	305.2	32.0	89.6	24.5	.0315	.864	1.701	3.749	7.1993	102,397
	29,356	417,5	305.2	32•	89.6	19•7	•0254	•696	1.371	3.023	5-5298	78,653
	29 • 356	417.5	305.2	32.0	89.7	13.5	•0174	•476	•93≝	2.067	3-6008	51,216
	29.356	417.5	305.2	32.1	89.7	13•5	.0175	•4 <u>78</u>	<u>•941</u>	2-075	3.5964	51,153.
þ	29.310	416.9	305.1	32	89.5	21.1	•u272	•744	1.465	3.229	5,9255	84.280
	29,310	410.7	305.0	31.8	89.3	24.4	.J315	.861	1.695	3.740	_7.177.0	102-081
	29.265	410.4	364.9	31.7	89.1	28.6	.0369	1.009	1.987	4.381	6,8435	125,785
	29.219	415.0	304.8	31.6	ģ8 <b>.</b> 9	37.1	•048p _	1.311	2,581	5,689	12.7098	180,776
	29.214	415.5	304.7	31.5	88,8	46-4	•0600	1,638	3.555	7:109	18,7315	266.424
	29.174 #####	414.9 #####	304• <b>7</b>	31.6	8.88 ****	48 <u>•</u> 9	• <u></u> ∉633	1,727	3.400	7.495	21 <u>*</u> 7089	<u>, 308.774</u>
I	29 <u>•</u> 323	417.1	3(5.1	31.9	89.5						-	
	€063	۰,۶	.2	•2	•4	DEVIAJIONŠ		-			<u> </u>	· J

TABLE 56 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5 PART 23ER

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 UTGH FRESSURE (10,000-FSTA NOMINAL) CN2 DEFACT CYCLES. FLOW IN REVERSE DIRECTION. TEST SPECIMEN (S/N 023) INLET PRESSURE = 1000 PSIA NOMINAL. DATA

FLOWMETER CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* OBTAINED AFTER PROOF PRESSURE TEST SPECIMEN INLET CONDITIONS.

lį.	•				•		· · · · · · · · · · · · · · · · · · ·		•	
	****	FLOWNEJEK ONE	***	******	FLOWMETER TWO					i
	FLOW RAIL	(FSTA)	TEMP (DEG. F)	FLOW RATE (ACÉM)	PRESSURE (PSIA)	TEMP	PRESSURE'	AVG TEMP (DEG. F)	FLOW RATE (ACFM)	"
	•85	⊅(.°İ	83.2	•91	47.9	87.8	1904.0	85.5	.0430	_
	<u>.</u> 77	ο <b>γ•1</b>	15 S	-81	48.3	86 <b>.9</b>	1004.0	. 84 <u>.5</u>	•0387	
	<u>•</u> 68	Dv • 6	81 •2	•71	49.1	86 • 0	1004.0	8 <u>3•6</u>	•0345	
	•59	⊃v • 4	80 • 9	-61	49.3	85.6	1004.0	83.3	•0297	
	•ુ5ն	50.1	81:1	•50	49.3	85 <sub>±</sub> 7	1004.0	83.4	•0248r	<u>.</u>
	•40	> v • 1	81 <u>.</u> 5	• 4 l	49.5	85 28	1004.0	83.6	.0200	
	<u>.</u> 31	50•2	85-0	•31	49.9	86 <u>.</u> 2	1"07.9	84.1	.0154	
	<u>.</u> 26	D , . 4	82.5	• 56	50.0	86 • 2	1004.0	84.4	·0159·	
	• 22	50.1	82 <u>•</u> 9	•21	49.9	მ <b>ნ</b> ენ	1 :04.0	84.7	.0106:	
	<u>•</u> 15	aå•J	83•4	•14	49•9	86 <u>.</u> 7	1004.0	85.1	• 0074	, .
	<u>.</u> 15	5.75	84•2	•14	50 <u>•</u> 0	87•3	1004.0	85 <u>.B</u>	.0074	1
	•53	49.7	84•2	•22	49.5	87.3	1004.0	85.8	•0112	
	•26	49.9	84 <u>±</u> 2	• 26	49.5	87 <u>.</u> 3	1)04.0	85.8	.0130	
	<u>.</u> 31	45°ā	84 . 1	•3j	49 <u>•</u> 3	87 <u>.</u> 2	1004.0	85.6	.0153	
	• <u>4</u> 0	a1•J	83 <u>•</u> 4	•40	4 <u>9</u> _5	86.9	1:04.0	85.1	.0200	
	•=0	1.00	82.7	•51	49 • 3	86 <u>.</u> 5	1404.0	84.6	• 0250	_
	• 59	÷1.4	81 • 9	•60	49+3	86•0	1004.0	84.0	-0296	·)
	•66	2. vc	81.2	+70	48•9	85.6	1304.0	83•4	.0338	
	•76	>6.1	8.0+5	•81	48•3	₽5•0	1,04+0	82.8	•0384	
	•8}	2,00	80,0	.gl	48.3	84.4	1004.0	85*5	.0436	

PAGE: 2... DATE: 9-8-76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5 PART >3ER

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL
PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE
(10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW
(10,000 PSIA NOMINAL) TEST SPECIMEN (S/N\_023)
INLET PRESSURE - 1000 PSIA NOMINAL. DATA
OBTAINED AFTER PROOF PRESSURE TEST.

I E S Ţ	SPECIMEN	INFEL	CONDITIONS
***	***	***	***

PRESSURE TPSTAT	AVG LEMP (DEG. F)	AVG FLOW RATE (ACHM)	GROSS DIFF: PRESS PRIMARY (PSID)	GROSS DIFF. PRESS SECONDARY (PSID)	AVG ĞRÖĞĞ DIFF PREŞS (PŞID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)	
1004.0	85.5	.0437	143,168	143.168	143.168	-0.000	143.168	
1004.0	84.5	. )387	126.733	126.733	126.733	-0.000	126,734	
1004. ջ	43 <u>.</u> 6	.0345	110.615	110.615	110,615	-0.000	110,615	
1004.0	43.3	.0297	92,63,	93.233	92.931	-0.000	92,932	
1004.0	d3.4	•0248	75,023	75,534	75.279	~õoóo	75.279	_;
1004.0	<b>83.</b> 6	.0200	59,522	60.048	59.785	-0.000	59.785.	
1007.9	84.1	. 1154	45 <b>,</b> 136	45.)94	45.165	→0.000	45.165	
1004•ပ္	74.4	.0129	37.082	37.265	37 <b>-</b> 173	-0.000	37.174	_
1004.0	44.7	.0196	29.665	29.787	29.726	-0.000	29,121	
1004.0	85•1	.0074	20.337	20.380	50•32 <u>8</u>	-0.000	20•359	
1004.0	<b>5.8</b>	•0074	20.395	20.551	20.473	#0.000	20.474	 ĭ
1004.0	∺5 <u>•</u> 8	.0112	31,635	31.856	31.746	-0.000	31.746	
1004.9	95.8	.0130	37,314	37.553 "	37.933	-0.000	37,433.	
1004.0	రవ∙6	.0153	44.440	44.703	44.571	-0.000	44.572.	-
1004.V	15.1	00200	58,895	59,416	59.156	→0.000	59.156	-
1004.4	d4∙6	.0250	75.645	76.166	75.906	-0.000	75.906	
1004.0	84.0	.0296	92.023	92.917	92.470	-0.000	92.470	<sub>(I</sub>
1004.0	33 <b>.</b> 4	.ŋ338	109.983	109.903	109.983	-0.000	109.983.	
1004.0	32.8	.0384	126.733	126.733	126.733	-0.000	126•73∳	_
1004.0	85 <b>•</b> 5	.0436	146.012	146.012	146.012	-0.000	146,012	
				*				

| ARE DIFF. PRESS = -1.64000E-04 + -1.2693UE-02 (ACFM) + 2.48070E-01 (ACFM) + 2

PAGE: 3 DATE: 9-8-76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW [15,1 DESCRIPTION IN REVERSE DIRECTION. TEST SPECIMEN (S/N 023) INLET PRESSURE - 1000 PSIA NOMINAL, DATA

TEST NUMBER 5

PART ZER

OBTAINED AFTER PROOF PRESSURE TEST

μ	***	*****	***	TEST S ********	PECIMEN INL	ÈT CONDITIONS	*****	-		TER PROOF PE	RESSURE TEST.	
•		PKESSURE		1EMPERATURE		FLOW RATE		FLOW RATE	ង់និងស៊ីនិងមិន្តីមិននិងគឺនិនិងជី <b>ទីនិនិ</b> ង		w 45	
	KG/SQ CM	PSLA	ĎĒĠ• K	DĒG∙ Ç	ĢEG. F	LITERS/ MIN	4ÇEM	<u>scem</u> _	KG\HĶ GNS	GN2	KE/SQ CM DIFFERENTIAL!	PSID.
	70.585	1004.0	3,02.9	29.7	85.5	80.8	.0430	2.854	5.620	12.389	10.0657	143.168
	70.585	1004.0	302.3	29.1	84.5	72 <u>•8</u>	•0387	2.572	5.064	11.164	8.9103	126.734
ŧį	70 <u>•</u> 586	1004.4	301.5	28. [	₿3•6	<u>6</u> 5 <u>•</u> ∩	•1345	2.295	_ 4 <u>.</u> 515	9.961	7.7770	110.615
•	70.585	1004+1	301.6	28.5	83.3	56 <u>•</u> 0	• 0297	1.977	3.893	8.583	6.5337	92.932
	70.586	1004.0	301.7	28.6	83.4	46 <u>•</u> 7	<u>•</u> J248	1,651	3.250	7 <u>•166</u>	5.2926	75.279
	70.560	1004.4	301,9	28.7	83.6	37 <u>.8</u>	<u>•</u> 0200	1.335	<b>5</b> •65₽	5.793	4.2033	59,785
	70.865	1007.9	302.1	28.9	¥4.1	29.1	<u>.</u> 0154	1.029	5.056	4.467	3.1754	45-165
	70 • 555	1004.	302.2	29.1	84.4	24.4	•0129	•8 <u>6</u> 1	1.695	3.737	2.6136	37,174
ı	70.586	1004.0	302.4	٤9.3	84.7	19•9	.0106	.704	1.38/	3.057	2.0900	29,727
	70.566	1004.9	302.7	29,5	85.1	13.9	.0074	•490	•964	2.126	1.4314	20.359
	70 • 566	1004.0	303.0	29.9	85.8	13 <u>.9</u>	•0074	.491	•96!	2 <u>•131</u>	1.4394	20.474
	70.586	1,004.6	303.0	29.9	85∙8	21.0	•01j\$	.742	1.461	3.221	2.2320	31.746
	70.586	1004.4	303.0	ž9.9	85.8	24 <u>•</u> 3	<u>.</u> 6130	.860	1.093	3.733	2.6318	37,433.
	70.555	1004 • 0	302.9	29∙8	გ2∙6	28 <u>.</u> 7	<u>•</u> 6153	1.014	1.999	<u>4.400</u>	3.1337	44,572
ľ	70.585	1004.0	302.7	29•5	85.1	37 <u>•</u> 5	•0200	1.325	2.610	5.753	4+1591	59,156
•	70.585	1004:0	302.4	29•2	84.6	47 <u>•</u> 0	•11250	1.661	3.271	7 <u>•</u> 211_	5.3367	75-906
	70.585	1004.5	302.0	28.9	84.0	55 <u>∙</u> ₿	<u>•</u> J296	1.969	3.87/	8.547	6.5013	92.470
	70 • 585	1004.0	301.7	28.0	83.4	63 <u>•</u> 7	<u>•</u> :338	2.248	4.42!	9.760	7.7326	109-983
	70.586	1004.	301.4	28.2	85*8	72 <u>.</u> 5	•.)384	2.560	5•041	11:114	8.9103	126,734
	70.585	1004.1	301.0	27.9 *****	62.2 *****	82 <u>*</u> 5	.0436	2.914	5.73/	12.649	10.2657	146-012.
	70.600	1004.4	302.2	29.1	<b>54.3</b>			MT 800 - 40-5		,		
	• 026	• 4	•5	•5	•9	DEVIATIONS	i			14 PLBS 1888		*** ***********************************

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST YUMPER 5

PART 23H

TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE .(10,000 PSIA NOMINAL) GN2.IMPACT CYCLES. TEST .SPECIMEN (S/N 023) INLET PRESSURE = 415 PSIA

PAGE: 1 DATE: 9-8-75

NOMINAL. TEST SPECIMEN INLET CONDITIONS

					FLOWNE	LEK CONDITIONS		
***	***	**	**	***	***	***	**	****
•				•	•	•	•	• • •

	*****	1110 H31_MnUJ1 **********	***	*****	FLOwMETER TWO	*****		am n =		
	FLOW RATE	(tatv) bysaanks	TEMP (DEG: F)	FLOW RATE (ACEM)	PRESSURE (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	FEON RATE (ACEM)	· · · · ·
	<u>•</u> 88	44 <u>*</u> 9	78.9	•91	47.9	81 <u>.3</u>	412.4	80.1	*1059	·
	.78	59.2	. 79•1	•81	48.5	<sup>4</sup> 1 • 3	411+7	8ô•̂\$	• 0955	•
4	.70	56.5	79 <u>.</u> 3	•71	4b • 9	#1 <u>•</u> 5	411.1	80.4	.0850	
•	•01	54.4	79•3	•61	49.3	·1•4	411.1	80 <u>•</u> 3	•0736	
	•51	24.1	79.3	•50	49.1	\$1.5	411.1	80+4	•0606 _	. 1
	.42	ಎಳ್.೭	79•5	.41	49.9	81.7	411.1	80.6	.0504	*** *
	, <u>3</u> 2	ಏ್.∠	79.7	•31	49.9	31.8	411.1	80.8	.0380	
	. 47	50.4	79.9	.26	50.0	b1•9	411.1	80 <b>-</b> â	.0326	
Į.	.22	၁၇ . 4	∂€•1	,2ļ	50.2	<b>82</b> •0	411.1	81.0	.0260	
٠.	•15	ع. يود	80 <u>•</u> 3	•14	50.0	82.1	411.1	81.2	.0173	<del>-</del>
	·15	ລດ•1	8,,.8	•1 <del>4</del>	49.9	82 <u>•</u> 5	411.7	81.6	.0172	U
	.23	44.9	81.9	•55	49.9	કે <b>ટ</b> •ે6	411.1	81.7	.0269	
	.∠8	20 el	86.+8	•26	49.9	12.5	411+1	8 <u>1</u> • <u>7</u>	-0328	
	•32	59.1	8.,•8	•31	49.7	82.6	411+1	81.7	•0387	
í	•42	+5*5	8 , , 6	-41	49.3	H2.5	411.1	81.5	• 0500	
	.51	٤., د	8 ,•3	•51	49 <u>.</u> 5	82.4	410.4	81.4	•0620	<del></del>
	<u>•</u> 61	عاود	80:2	•ei	49.3	<b>~2•</b> 2	410.4	8 <b>1</b> ∙5	0740	ŋ
	<u>• 79</u>	عوود	80.1	•71	48 <u>.</u> 9	+ 2 • 0	409.8	81.0	.0849	
	•79	2.+1	8426	-81	48 <u>∗</u> 3	81 <u>.</u> 8	409•1	80.9	•0962	
	·81	47.9	8.4 <u>•</u> .0	•91	47.9	3 <b>1.</b> 7	408.5	80.9	•1063.	

PAGE: 2 DATE: 9-8-76

TABLE 57
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

H

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE TEST SPECIMEN (S/N 023) INLET PRESSURE 415 PSIA NOMINAL.

TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\* GHOSS DIFF PRESS GROSS NET DIFF PRESS (PSID) AVG ΑVG DIFF. PRESS AVG GROSS TTARE DIFF. PRESS DIFF. PRESS **PKF220kF** SECONDARY (PSID) TEMP PRĪMARY FLOW RATE (PSID) (PSIA) (DeG. F) (ACHM) (PSID) 153.386 153.386 \$002 153.385 412.4 •1059 153,386 **ジリ・1** 411.1 50.2 .0955 129,999 129,999 129,999 .001 129,997 108.424 108.824 1081823. 411+1 ~u•4 • 0850 108.824 001 88,913 BB.741 411.1 88,569 .001 88.740 თე.3 .0736 68,687 68,465 68,464 411.4 011.4 .06"B 68.244 .000 52.955 411.1 .05 14 52,713 53, 2, 1 52,957 .000 υυ.6 411.1 **\*0.8** .0340 37.758 38.,13 37,885 .000 37.884 31,396 31,332 31,330 411.1 31.268 .000 81.6 . 1346 81.0 411.1 .026. 23.852 23,932 23.892 .000 23,891 14.871 14.943 14.907 411.1 41.5 . 1/3 -000 14.906 411.5 .. 172 14.813 14.943 14.875 61.6 .000 T4-877 411.1 24.779 24.9 7 24.843 **61.7** . 1269 .000 ` 24 **.**842` . 328 .000 411.1 31.798 31.678 31.677 01.7 31,558 38,877 38,781 411.1 . 387 38,685 61.7 .000 38.779 411.1 ,1.5 .0560 52,58s 53,2,1 52...94 .000 52.893 416.4 d1.4 .0620 70.368 76,899 70.634 .001 70.632 41,,4 81.2 .0744 89,424 90.178 89.801 .001 89.799 409.0 109,140 .0849 109,140 109,140 .001 109, 139" 51.0 •001 130.946 469.1 130.947 130.947 r (1 • 9 -0962 130.941 448.0 er.9 .1063 155,543 155,283 155,283 155,281 .002

LARE WIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E=01 1ACFM) + 2 +

0\_4YCEM1##3

PAGE: 3 DATE: 9-8-76

TABLE 57
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5

PART 23H

TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE YERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. TEST . SPECIMEN (S/N 023) INLET PRESSURE = 415 PSIA

į,	***	**	***	TEST S	NOMINAL.		NET DIFFERENTIAL PRESS						
,	PRESSURL TORE			***	****	*****	FLOW RATE	*****	*****	# 3 TH # 1			
	KG/SU CM	ЬŽIV	חבפ• ע	ŋĒĠ. C	DEG. F	LIT=RS/ MIN	,CFM	SCFM	ĸĞ\HŘ GuS	GN2	KG/SQ CM DIFFERENTIAL	PSID	, <sup>"</sup>
	28,991	414.4	299.1	26.7	b. •1	82.6	•14÷9	2.916	5 <u>.</u> 74¢	12,658	10.7840	153.385	•
	28.940	411./	360.0	26.4	84.5	74.3	. (955	2.624	5 <u>.</u> 16/	11.391	9,1397	129,997	_
Ь	28.90v	411:1	360.0	26.9	80.4	66.0	0460.	2.332	4,591	10:121	7,6510	108-853	
r	28.9(0	411.1	300.6	26.9	dn.3	57.2	736	2.019	3.975	8.763	6,2390	88./40	
	26.900	411.1	306.1	26.9	81, 4	47.2	•#69B	1.668	3.289	7.240	4.8135	68.161	IJ
	58. Ann	411.1	300.2	27.0	₽ <b>6</b> •6	39.1	. 1,5/14	1.381	\$• <u>1</u> 17	5.994	3.7231	52,955	
	28.90v	411.1	300.2	27.1	80.8	29.5	.0386	1.041	2.049	4.518	2,6635	37,884	
	29.900	411.1	300.3	27.2	80.9	25.3	326	.895	1.761	3.883	5.5058	31.330	
rı.	28.900	411:1	300.4	27.4	81.0	2ŏ•1	.026J	.711	1.401	3,088	1,6797	23,891.	
ŗ	28 <sub>2</sub> 900	411.1	300.5	27.3	81.2	13,4	, 173	.475	• 935	2.061	1.0480	14,906	
	28.946	411.1	360.7	27.6	81.0	13.4	. 172	.473	.931	2.052	1.0459	14.877	¥
	28.900	411.1	300.8	27.0	81.7	50°8	. 259	.735	1.44!	3,189	1.7465	24.542	
	28,900	411.1	306.8	27 •0	81.7	25.4	. 32H	.897	1.765	3,892	2.2271	31,677	
	28.900	411:1	3րե.Ց	27."	81.7	29.9	•µ387	1.058	2•∪84	4,591	2.7265	38.779	
	26,900	411,1	300.7	27.5	ģ1.5	38.7	•្ ឧទីបព	1,368	2.694	5,939	3,7187	52-893	
ι	28,855	4i .4	300.6	27.4	<b>¤1.</b> 4	48.9	62.	1.694	3•33₽	7.355	4.9659	70 <u>-632</u> .	
	28.855	41.4-+	300.0	27.3	61.2	57.3	.0740	2.023	3.984	B <u>.</u> 782	6.3135	89.799	¥
	58 80 y	409,3	300.4	27.2	81.3	65.6	.0849	2,317	4*264	10.060	7.6732	109.139	
	28.764	409.1	366.3	27.4	80.9	74.2	.4962	2,622	۶•16۶	11.383	9.2064	130.946	
	28./  \ 4####	40°*⊐ «អង្អិទ	3:);; • 3 *****	27.1	69 *****	d2 <u>•</u> 0	F901.	2.895	5.701	12.568	10.9173	155•281	
	Sp - 884	410.8	300.4	27.4	ã1 <b>∙</b> 0					*** **** **** ****	<u> </u>		
	<u>.</u> 042	.0	.2	٠.	. 4	DEVIATIONS	\$						_

PAGE: 1 DATE: 9-8-76

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL
PRESSURE DATA ACQUIRED AFTER 10 HICH PRESSURE
(10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW
IN REVERSE DIRECTION. TEST SPECIMEN (S/N 023)
INLET PRESSURE = 1000 PSIA NOMINAL.

TEST NUMBER 5

ţ

PART 23F

FLOWMETER CONDITIONS

FLOWMETER CONDITIONS	• • •		TEST SPECIMEN INLET CONDITIONS
<b>特种性经验性结婚性特殊性的证明的证明的证明的证明的证明的证明的证明的证明的证明的证明的证明的证明的证明的</b>	****		****
		•	·

	FLOWN: TER ONE			*******	FLOWMETER TWO		-			
	FLOW RATE	PRESSURE (PSIA)	T⊭MP (DEG• F)	FLOW RATE (ACFM)	PRESSURE.	TEMP	PRESSURE (PSIA)	TEMP (DEG. F)	FLOW RATE (ACFM)	. j
	•87	>v•1	77•7	• 90	47.9	82•7	1005.3	80.2	•0432	
	<u>•</u> 79	49.5	76+8	•82	47.8	81+8	1,05.3	79•3	. 0388	
1	• 69	20.1	76•8	•71	48.5	81.6	1405.3	79•2	•03*3	
	<b>.</b> 6ŋ	49.7	7A+9	•61	48.7	81.6	1 .05.3	79.2	.0296	_
	•51	49.9	77•3	•5)	48.9	81.7	1005.3	79.5	•0250	1
	.42	pv*3	77.9	.41	49.9	92.	1705.3	79.9	.0206	
	•35	⊅ນຸ•5	78 <u>•</u> 6	.30	50.1	82.4	1005.3	80.5	.0155	_
	.27	49.9	79.3	.26	49.5	82.8	1005.3	81.0	.0130	_
	•55	⊅v.3	79•9	•21	49.9	43.1	1,105.3	81.5	.0108	
	•14	50.1	84•6	•13	49.9	83.5	1,405.3	82•0	• 0069'	-
	-14	>0.1	81 • 6	•13	49.9	93.9	1:05.3	82.8	•0069	1
	•55	49.9	8) •5	•21	49.7	84 • •;	1^05.3	82.7	+0106	
	<u>•</u> 27	49.9	81+3	•26	49.5	84•"	1005.3	82.6	.0131	
	•35	49.7	81 • 1	•31	49.3	84.1	1::05+3	82.6	.0156	
	.42	49.5	8r • 4	-41	48.9	83.8	1001.3	82.1	.0203	_
	•51	49.9	79:5	•51	49•l	<b>93.</b> 5	1 101.3	81,5	.0251	_
	<b>.</b> 6ŋ	50.3	78+7	•60	49.1	82.9	1701.3	80.8	• 0298	J
	•69	44.7	77.9	•71	48.3	82+4	1:01:3	80 • 1	• 0343	
	<u>.</u> 78	20-3	77 <u>•</u> 1	•81	48•5	81.9	1001+3		•0392	-
	•B7	20.1	76.3	•91	48.1	n1.1	1601.3	78:7	.0437	

TABLE 58
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION

PAGE: 2 \_\_\_\_\_ DATE: 9-8-76

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW IN REVERSE DIRECTION. TEST SPECIMEN (S/N 023) INLET PRESSURE = 1000 PSIA NOMINAL.

TEST SPECIMEN INLET CONDITIONS

IARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM)\*\*2-7

PART 23F

TEST NUMBER 5

	*********	жилиниканпика		****	<b>4 4</b>		
PRESSUME (PSIA)	AVG 1EMP (DEG. F)	AVG FLOW RATE ("CFM)	GRASS DIFF• PRESS PRIMARY (PSIU)	GROSS DIFF. PRESST SECONDARY (PSID)	ÁVG GROSS DIFF• PREŜS (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)
1005.3	80.Ž	.0432	50.498	5ì.i99 " "	57.849	-0.000	50.849
1005.3	19.3	.1368	44,961	44.879	44.920	-0.000	44.920
1005.3	79.2	.0343	38,53	38,628	38.579	-0.000	38.579
1005.3	79.2	.1296	32.099	32.1º2	32.140	-0.000	32.140
1005.3	79.5	.0250	26.073	26.093	26.083	-0.000	26.083
1005.3	79.9	.0206	20.453	20.475	20•46 <u>4</u>	-0.000	20-464
1005.3	80.5	• 0155	14.659	14.695	14.677	-0.000	14-677
1005.5	ძ1•0	.0130	11.994	12.010	12.002	-0.00ā.	12.002
1005.3	81.5	•0108	9,676	9.669	9.672	-0.000	9.673
1005-3	H2.0	• 0 0 6 9	5,852	5.847	5.849	-0.000	5.850
1005.3	52•8	• 0 1 6 9	5.852	5.847	5.849	-0.000	5.850
1005.3	82.7	•01=6	9,444	9,497	9,471	-0.000	9.471
1005.3	82∙6	.4131	12,167	12.238	12,503.	-0.000	12.203.
1005.3	<b>83∙</b> 6	•6156	14.833	14.924	14.87 <u>8</u>	0.000	14.879
1001.3	42.1	.0203	20,105	20.3n3	20.204	-0.000	20,204
1001.3	81.5	.6251	26.247	26.387 * * *	. 56°313	-0.000	26.314
1001.3	~o.8	•029a	32,215	32.412	32.313	-0.000	32.313.
1001.5	H0+1	.0343	38,414	38.628	38,521		38.521
1001.3	79.4	.0392	45,193	45,195	45.194	-0.000	45+194
1001.3	78.7	.0437	51.373	52.148	51.760	-0.000	51.760

PAGE: 3 \_ DATE: 9-8-76

TABLE 58
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL
PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE
(10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW
IN REVERSE DIRECTION. TEST SPECIMEN (S/N 023)
INLET PRESSURE = 1000 PSIA NOMINAL.

NET DIFFERENTIAL PRESS

TEST UMBER 5 PART 23F

TEST SPECIMEN INLET CONDITIONS

U 4444	***	***	TESI SPECIMEN INLEI CONDITIONS								ななな事をものなる事ををををををなる。 MC1 D1とことには「する」、これにあっ		
•	PRESS	JRF +++++++	TEMPERATURE			FLOW RATE					* * ** *******************************		
K <u>G</u> /§	5Q CM	PSIμ	DEG• K	p <b>EG</b> ∙ C	DEĞ∗ F	Liteps/ Hin			KĞ\HĞ QNS	GNZ '	KG75Q CM DIFFERENTIAL	PSID	
7	0•677	1,)05+3	299.9	26+8	83.2	82•0	• 6432	2.897	5.704	12.574	3.5750	50.849	
	j •677	1005.3	299.5	26.3	79.3	73.7	• '388	2.6nB	5.135	į1•322	3-1582	44.920	
7 (	677	1005.3	299.4	25+2	79.2	64.8	•#343	2.303	4.535	9.999	2.7124	38.579	
7(	677	1005.4	299.4	26.2	79.2	55.9	. 296	1.990	3.918	8 • 639	2.2597	32,140	
76	677	1,05,3	299.6	26.4	79.5	46.9	• 4525	1.678	3•303	7.282	1.8338	26.083	
7(	0 • 677	1005+3	299.8	26.0	79.9	38•5	• 0206	1.381	2:720	5•996	1-4388	20.464	
7(	0.677	1405,3	300.1	26,9	80.5	28.7	.0155	1.041	2.050	4,519	1,0319	14,677	
76	677	1005.3	300.4	27.2	81.0	24.0	.013	.874	1.721	3.794	.8438	15-005	
70	.677	1vn5.3	304.7	27.5	81.5	19.9	1118	.725	1,42?	3.146	-6800	9,673	
70	0.677	1005.3	301.0	27.8	82.0	12.5	•1069	•461	•909	2.003	•4113	5,850	
76	0.677	1005.3	361.4	28.2	82.8	12.5	-1069	.461	•907	2.101	.4113	5. <u>8</u> 60	
7(	0.677	1005.3	301.4	28.2	82.7	19.4	•0100	.708	1•393	3.072	.6659	9,471	
7(	677	1005.3	301.3	28.1	82.6	24.1	• 1131	<b>.</b> 877	1.72?	3.807	.856 <sub>0</sub>	12.203	
7	0.677	1)05.3	301.3	28.1	85.6	29 • 0	• 0156	1 • 044	2:055	4+530	1.0461	14,879	
7 (	o•398	1001.3	301.0	27.8	82.1	37.6	• )203	1.352	2.663	5.870	1.4205	20.204	
70	0.398	1001.3	300.7	27.5	81.5	46.9	. '251	1,675	3,297	7.270	1.8500	26,314	
76	) <b>•39</b> 8	1)01.3	300.3	27.1	8.98	55.7	. 298	1.986	3.911	8.622	2+2719	32,313	
7	0,398	1,01.0	299.9	26.7	87.1	64.6	•/1343	2,292	4.5],2	9.948	2.7083	38,521	
70	ი•398	1001-3	299.5	26.4	79.4	74.2	• "392	2.623	5-164	11.385	3,1775	45.19 <del>4</del>	
7	0 • 398 #####	1001+3	2 <sup>99</sup> •1	26•) ****	78•7	83•0	• <sub>0</sub> 437	2.927	5•764	12.707	3.6391	51.760	
7	<sub>0•</sub> 593	1904-1	300.3	27•1	80.8			• •		page of the halfs of the	·		
	•117	1.1	•7	•7	1.2	DEVIATION	s						

PAGE: 1 DATE: 9-8-76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST HUMBER S

FLOWNETER CONDITIONS

PART 231R

TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED-AFTER-10-HIGH-PRESSURE-(10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW IN REVERSE DIRECTION.-TEST SPECIMEN-(5/N-023)-INLET PRESSURE = 415 PSIA NOMINAL.

TEST SPECIMEN INLET CONDITIONS

t 1		•			•	•	,, , ,,,,			
'n	***	FLOOMETEK ONE	化存收器外部收拾的数分	****	FLOWNETER TWO	) · ‹ · · · · · · · · · · · · · · · · · ·			AVG_	)
	FLUM RATE (ACEM)	(ちかてい) しゃこうついから	TựmP (DEG• F)	FLOW RATE (aCFH)	PRESSURE (PSI4)	TEMP (UFG. F)	PRESSURE	AVG TEMP (DEG. F)	FLOW RATE (ACEM)	: 
	•83	೨೪ ಕಿರ	83•4	• Rō	48.3	e-4 • 8	416.2	84.1	.1003.	
	•18	~. a £	83.2	• # 1	48.3	. 4•8	415.6	84 • 0	•0942	
	•69	ລົ•1	32.9	•71	48.7	84 <b>•</b> 7	415.6	83∙8	•0831	
•	• 56.	D . 4	82.5	•60	49.3	04•3	414.3	83.4	•0726	
	14.	47.9	8-54	√5 ي	49•1	⁴4•1	414.3	83.2	• 06 05	-d
	•42	⊃£.∠	42.2	.41	49.9	4.3	414.3	83.2	•0497	<del>-</del> -
	1 ك ۽	ءڙ ۽ <	62 <u>.</u> 2	.30	49,9	54 • l	414.3	83.2	.0372	
	:2!	21.5	82+2	• 30	49.9	~4.7	414.3	83 <u>•</u> 2	•0317	_
!	• 52	50.0	82 • 2	.20	49.9	4•2	414.3	83.2	• 0254	-
	•14	>0,€	82•4	•13	50 - 4	<b>64•3</b>	414.3	83 <u>*</u> 3	•0168	
	-14	54	82.5	•13	56.•2	-4 • 4	414.3	83.4	•0168	IJ
	<u>.</u> 21	54 • J	88.42	•50	49.9	n4.3	414.3	83.4	•0253	_
	.41	o1	B2 • 3	٠26	49.9	44.3	414.3	83 <u>•</u> 3	•0321	_
	•32	74.1	82*5	-31	49.7	64.2	414.3	83.2	•0376	
ı	•41	Dt .1	82.0	.41	49.5	114 - 4	413.7	83.0	•0494	
	•51	44.6	н•14	•51	49•1	M3•9	413.5	82.8	•0606	<u>.</u> .
	450	51	81.7	•60	48.9	#3+6	413.1	82.7	-0717	
	•69	۵، ۱۱	ძე • 7	•71	48.7	ხ3•5	412•4	82.6	•0837	
	• 7 is	45.6	ø) • 7	•#1	48•3	63+4	411.7	82•5'	• 0 <u>948</u>	
	• \$3	20.1	B2.1	.87	48.3	<b>83.</b> 4	411.7	82.7	<u>.101</u>	

PAGE: 2 DATE: 9-8-76

TABLE 59 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5 PART 231R TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10-HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW IN REVERSE DIRECTION. TEST SPECIMEN (5/N-023)—INLET PRESSURE = 415 PSIA NOMINAL.

РЯ <u>С</u> ЗЗИК <u>Е</u> (PŠIA)	AVG IEMP (DEG• F)	AVG FLOW RATE (ACFM)	GROSS DIFF• PRESS PRIMARY (PSID)	GRASS UIFF. PRESS T SECONDARY (PSID)	DIEŁ PREŚZ DIEŁ PREŚZ (PŚID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)
416.6	₩ <b>4</b> •1	.10:3	283,912	283,912	283.912	-001	583 <sup>°</sup> 811
415.0	٥4 <u>•</u> 0	.9942	241,878	241.878	241.878	001	241_877
415.6	6 <u>.</u> 3	.0831	190,995	196.995	190.995	.001	190-994
414.3	<b>33</b> ₄4	.0726	153,792	153,702	153.702	001	153,701
414.3	63.2	•06 •5	117.989	117.989	117.989	•000	
414.5	p3.2	.0497	89.993	97,178	90.085	•000	~ ····90 <u>•</u> 084·
414.3	83.2	.0372	62,697	62 <b>.</b> 998	62:847	.000	65°846.
414+3	n3 <u>*</u> 2	• .312	51.419	51.936	51.678	•000	51.67 <u>6</u>
د ، 414	,3 <b>.</b> 2	• 0254	39,940	40.687	40.014	•000 -	40.012
414.3	h3•3	•.:168	24.818	24.850	24.834	•000	24.832
414.5	73.4	•,:168	24.7.12	24.859	24.776		24.774
414+3	d3 <u>.</u> 4	• 1253	39.998	40.260	40 - 129	•000 * ***	40-128
414.3	<b>83•</b> 3	321	52.797	53,517	53,157		53,156
414.5	#3 <u>*</u> 2	.,13/6	64.199	64,578	64.389	•000	- 64 <u>-</u> 38 <u>7</u>
413.1	d3.0	.0494	89,993	90.410	90.402	• 0 0 0	90,400
u <b>. د 4</b> 1	62 <u>.</u> 8	•0606	119,886	119.886	119.886	•000	114°88¥
413.0	۶2 <u>.</u> 7	.0717	153.076	153.070	153.070	.001	123 <u>*</u> 06å
412.4	92 <u>.</u> 6	.0837	195,1)4	195,1 4	195.104	.001	182 <u>*</u> 103
411./	აგ∙2 2	•0948	249,779	249,779	~249.779	<u>•001</u>	249,778
411.	82.7	.1014	300.346	300.346	300.345	.001	300.345

1ARE DIFF, PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM) \*\*2"

STATE SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO SOOF TO

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PAGE: 3 DATE: 9-8-76

TABLE 59
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TCST LUMBER 5

PART 231H

TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW IN REVERSE DIRECTION. TEST SPECIMEN (5/N-023) INLET PRESSURE = 415 PSIA NOMINAL.

	TEST SPECIMEN INLET CONDITIONS									INLET PRESSURE = 415 PSIA NOMINAL.  NET DIFFERENTIAL  ***********************************				
ł	PHE534	aparantan pri	******	EMPEKATURE   \$444444	****	FLOW RATE					T. P. W. Married and Special additional property of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the se	1		
	ка́/50 см	<b>بارد</b> اء	WLG. K	}ĔĠ• (	UEĢ• F	LITERS/ Min	a <b>Ç</b> Fh	SCFM	кё́\нй Ри́ѕ	r₽₹\HK GNS _	DIFFERENTIAL	PSĮD		
	54•762	Hais	3n2 • 1	28+9	84.1	78•,4	•10:3	2.767	5.445	12.013	19.9609	283.911		
	74•517	710.0	302.,	28.7	d4 + +)	/3.5	. 942	2.596	5 <u>*</u> 11¢	11 <u>.</u> 269	17.0056	241.877		
ŀ	59.517	+1⊃ •′o	362:1	28.0	83.8	64+9	. 831	2•2 <sup>9</sup> 1	4.511	9.944	13.4282	190,994		
•	29.168	4]4+3	3 1.7	25.5	83.4	36.5	• ,720	1.996	3+3Å	8 <u>.</u> 665	10.8062	153,701		
	29.123	41443	3.11.0	28.4	83.2	47.1	. •126.37	1-664	3.27/	7:225	6.2954	117.988		
	29:128	स रिन् + व	31.0	28.4	3.2	1.86	• 497	1.366	š∙ė́8Ä	5.928	6.3335	90.08-		
	29.126	41462	3,1.6	28.4	03.2	28,9	. 13/2	1.022	2.013	4.437	4.4185	62.846		
	24.120	414,5	301.6	28,5	3.2	24.6	.;317	.871)	1:714	3,779	3,6332	51.674		
þ	29,120	+14.3	٥٠(راد	۵, ۶۶	63.5	19.8	. 254	.699	1.370	3,034	2.8131	40.012		
•	29.128	414,3	3.1.7	28.5	<b>63.</b> 3	13.1	•+ 16B	.462	•91∂	2.007	1.7459	24.83/		
	29.120	414,2	301.7	28.6	83.4	13 <u>.</u> 0	•3164	• 460	•90 <u>/</u>	1.999	1.7418	24-77: 1		
	24.125	414.5	301.7	28.5	83.4	19.7	•*253	.695	1.368	3.015	2.8213	40.124		
	24.124	117.5	331.7	28.5	ø3 <b>.</b> 3	25.0	.,321	.883	1.735	3.832	3.7372	53,15		
	29.128	414.3	331.6	28.4	83.2	29,3	• 5 <b>37</b> 6	1.035	2 <u>.</u> 03 <u>8</u>	4,493	4.5269	64.38/		
!	29 . uns	413.1	301.5	29.3	ø3.·	3∂•4	• 494	1.356	2-669	5.885	6.3558	90.400		
	29.131	+13.,	301.4	21.4	ø2 <b>∙</b> 8	47.1	•9 <b>6</b> 36	1,663	3,474	7.218	8.4287	119.58.		
	27.11.1	413.,	301.3	28.1	62.7	55.7	+ 1717	1.966	3.874	8 <u>.</u> 536	10.7618	153,069		
	56.441	+14+4	3.1.3	∠b • 1	b2•6	64.9	•9837	2.293	4.510	9 956	13.7171	1954103		
	26.940	F1 x + 1	3,.10.2	28 - 1	62.5	73.4	•1794A	2.592	2•i0à	11.254	17.5611	249,77		
	****	+ <u>  </u>   +	6.1(E	25.4 ****	42.7	78.5	•1014	z•77ž	5 <u>•</u> 457	12:034	21•1163	300-345		
	24.1.0	+14.	301.6	28.5	83.2		-	~						
	100+	• 7	• 2	<b>+</b> € <sup>4</sup>	•3	DEATALION	5			* **		,		

PAGE: 1 DATE: 9-8-76

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST YUMBER S

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HLES THAN

TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10-HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW IN REVERSE DIRECTION. TEST-SPECIMEN (S/N-023) INLET PRESSURE = 1000 PSIA NOMINAL.

### FLOW FETER CONDITIONS

From Fig. Countings	
· · · · · · · · · · · · · · · · · · ·	

TEST SPECIMEN INCET CONDITIONS				
	TEST	SPECIMEN"	YNEFT"CON	TTYONS
		u = 2.11_11		V4 1 4 * III =
*******************	***	***	***	*****

	•		•		<del>-</del>			<del></del>
******	ት୮ዐጫ፣ ነርሩ በህር ት	****	****	FLOWMETER TWO	) *********			
FLOW RATE	(hài'a) byf pànyf	TrmP (Leg: F)	FLOW RATE (ACEM)	PRESSURE (PSLA)	TEMP (DEG: F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	FLOW RATE (ACEM)
• <u>\$</u> 7	5 <sub>9</sub> • 4	76•7	•92	46 <u>.</u> 3	¢2•4	1011.9	79.5	•0435
• 77	20.5	75•≀	• 81	48.5	81•7	1007.9	78•9	.0388
<u>.</u> 69	무보흡수	75.7	•71	48 <u>.</u> 9	H1 • 3	1.07.9	78,•5	•0345
•60	<b>□4 + 0</b>	75.7	•61	49.5	21.1	1007.9	78 <u>•</u> 4	•0301
•50	⊅ų • 4	75.9	•5v	49.7	81.2	1/107.9	78.6	•0250
<u>.41</u>	⊅ų•1	7n <u>.</u> 6	•40	49.5	81 <u>.</u> 5	1011.9	79.0	•0200
<u>•</u> 32	47,9	77•9	•30	49.5	81.7	1 (07.9	79.4	•0153
:26	2 ، باد	77•7	•25	49.9	22•1	1/11.9	79 <u>•</u> 9	.0128
•55	ρά∓ j	7h•4	•S1	49.9	65•2	1015.9	80.5	<u>•0104</u>
<u>.</u> 15	49.7	79-1	•13	49.5	H2.9	1915.9	81.0	• 0069
•15	ခမ္ - မ	84:1	-13	50+2	<b>∂3•4</b>	1015.9	81•7	•0070
•22	26.45	80:1	• 20	50.0	53.4	1615.9	81.8	•0104-
• ₹8	ع ب • ح	80 = 0	• 26	49.9	43.4	1 15.9	81.7	0132
.32	44.9	79•8	+31	49 •5	<b>93.4</b>	1%15.9	81.6	•0155
.42	añ • 1	79 <u>+</u> 3	•41	49•5	33.2	1-15.9	81•5	•0203
•51	44.9	74 <u>*</u> 6	•51	49 <u>•</u> 1	-2.9	1,15.9	80.8	•0247
•60	<b>5</b> 0€ • 4	77-7	-61	49.5	<b>⊘2</b> • 4	1.15.9	80-1	0299
±69	DC 44	76.9	•70	49.1	81.6	ļ:15•9	79•3	•0341
•78	51.4	74:2	•61	48.7	81+3	1-15.9	78+7	•0387
•86	55.5	75 5	•91	46.3	80.45	1007.9	78.0	.0434

PAGE: 2 DATE: 9-8-76

# TABLE 60 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION

PLEC TRLY

TEST . UMBER 5

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN<sub>2</sub> IMPACT CYCLES. FLOW IN REVERSE DIRECTION. TEST SPECIMEN (S/N 023) INLET PRESSURE = 1000 PSIA NOMINAL.

	haanaaaaaaaaaa Frimfu infil cou					**************************************	- x	
PRESSURE (PSIA)	AVG LEMP (DÊG. F)	FLOW RATE ("Crh)	ARGSS DIFF• PRESS PRĪMARY (PSIJ)	GRUSS DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF• PRESS (PSID)	v
1011.7	79.5	.9435	78,585	79.3/7	78.95 <u>6</u>	-0.000	78 956	
1007.9	18.9	88Ey•	68.118	<b>58.897</b>	68 <b>.</b> 5ŋ <u>ਖ਼</u>	-0.000	ea <u>*</u> 20ā	
100/.7	14.5	•0345	59,479	60.048	59.764	-0.000	* 159 <sub>•</sub> 76 <sub>4</sub> . **	
1003.4	10.4	• 03 01	50.331	5,.883	50.607	-0.000	50-607	
1007.9	fd•6	•0250	40.404	41.401	40.902	-0.000	40.902	ıl
1011.7	79.0	.02.00	32.002	32.258	32.130	-0.000	.35 <sup>4</sup> j.30.	,
1007.9	19.4	• 0153	23.601	23.7/3	23.652	÷0.000	23.652	
1011.9	19.9	• )128	19.425	19.526	19.475	-0.000	19.475	•
1015.9	د بر•ِڠ	•01 :4	15,250	15.343	15,300	<del>~</del> 0.000	15,301	•
1615.7	n1.u	•0469	9,695	9.745	9.720	=0.000	9.720	
1015.9	01.7	•00/v	9.927	19.030	9.979	~0.000	. <del>9.979.</del>	- 4
1615.9	~1 <u>*</u> 8	•01 4	15.431	15.572	15.502	-0.000	12°20S_	· '
1015.9	b1.7	•4132	20.298	2,.437	20.367	-0.000	50.368	-
1015.9	ø1•¢	.6155	24.354	24.5 6	24.436	-0.000	24-430	*
1015.9	1.2	.02,3	32.871	33, 63	32,967	-0.000	32.967	
1015.7	* v.8	• 0247	41,563	41.817	41.69u	-0-000	41.690	
1015.7	1.00	• 05,88	51.,63	51,931	51.457	-0.000	51,457	٠ .ا
1015.7	19.3	• 9341	59,479	60.048	59.764	-0.000	59.764	1
1015.9	18.7	.0347	69,493	70.162	69.827	-0.000	69 <u>-</u> 827	•
1667.9	18.0	.0434	78.833	79,643	79,238	-0.000	79,238	-

PARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM) 492 +

PAGE: 3 -DATE:- 9-8-76

# TABLE 60 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5

PART ZJUR

TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL -PRESSURE DATA ACQUIRED AFTER 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES. FLOW IN REVERSE DIRECTION. TEST SPECIMEN (S/N 023) INLET PRESSURE = 1000 PSIA NOMINAL.

tı	****	***	ដុំឯងសុសុសុសុសុសុស			EL CONDITIONS			INLET PRI		O PSIA NOMINAL. NET DIFFERENTI	ALI PRESS
¥	PRESS	#8848844 htt	***	IEMPERATURE	***	****	***	FLOW RATE	******	***		
	KG/SQ CM	P514	DEG <sub>e</sub> K	DE⊌• Ç	ņ <u>eg∙</u> <u>F</u>	LITERS/ Min	ACEM	SCEM	Ŕġ∖Hĸ ĕ⋈S	GN2 LBS/HR	KG/SQ CM DIFFERENTIAL	PSID
	71.144	1011,7	299.6	26.4	79.5	83.2	. 435	2,939	5.78	12.759	5,5512	78.956
	70.865	1007.7	299.2	26.⊍	78.9	74•0	•0388	2.614	5.14/	11.346	4.8166	68,508
ır	70.865	1007.7	299•6	25.8	78.5	66 <u>.</u> g	.6345	2.330	4 <u>•</u> 58 <u>ë</u>	10.115	4.2018	59,764
1	70,865	1907.7	298.9	25•8	78.4	57.5	.0301	2.031	3.999	8.817	3,5581	50-607
	70.865	1007.7	299.0	25.9	78.6	47 <u>.</u> 8	• 0250	1.687	ã∙ãSŤ	7,322	2.8757	40.902
	71:144	101127	299•3	26 • <u>i</u>	[9+i]	38•ુ3	•0500	1.351	5-661	5,866	2•2590	32,130
	70_865	100/-7	299.5	26,3	79.4	29.2	• 153	1.030	2.02 <u>5</u>	4.471	1,6629	23,652,
	71.144	1011.7	299.8	26.6	79.9	24.6	•./128	.867	1.705	3.765	1.3692	19,475
p	71.423	1y15.7	300.1	26.9	⊌ŭ.5	19•9	•0104	.704	1,385	3.056	1.0757	15.301
ţ	71,423	1,15.7	300.4	27.2	81.0	13,1	• აე69	.464	•914	2.014	.6834	9.720
	71.423	1015,7	300.8	27.0	81.7	13:4	•0070	.473	•835	2.054	.7016	9,979
	71.423	1615,9	300.8	27.7	81.8	19•9	.0104	•702	1•38½	3.048	1.0899	15,502
	71.423	1015.7	300.8	27.6	81.7	25.4	132	.895	1.763	3.887	1.4320	20.368
	71.423	1015-7	300.7	27.5	81.6	29 • 7	• 0155	1.048	2.064	4.550	1.7176	24,430
	71,423	1915,7	309.5	Ž7•.₫	81.2	38.8	.0203	1.371	2.700	5.953	2 <b>.</b> 3178	32.967
	71:423	1015.7	300.2	27.1	80.8	47 <u>•</u> 4	• 1247	1.675	3•59₽	7 <u>•</u> 271	2.9311	41.690
	71.423	1015.7	299.9	26•(	80.1	57 <u>•</u> 4	• 0299	2.027	3.991	8,799	3.6178	51.457
	71:423	19155	299.5	26+3	79•3	65•5	• y <b>3</b> <u>4</u> <u>1</u>	2•313	4.555	10:043.	4:2018	59,764.
	71:423	1015+3	299:1	25+9	78+7	74.0	• 3387	2.634	5:18/	11:435	4.9094	69.827
	70+805 #####	100/27	298•7 ****	0•55 *****	7d•g	83:1	• 0 4 34	2.934	5.170	. 12:734 .	5,5710	79+238
	71:214	1014.9	299.8	26.6	79.9			## # ## WA				1
	• 239	5 ۽ خ	•6	•6	1.1	DEVIATIONS	5	* * * *		AN INCOMPRESENT THE STATE OF		- <del></del>

PAGE: 1 DATE: 7/23/76

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION- IMPACT/FIOW RATE VERSUS DIFFERENTIAL
PRESSURE. PRIOR TO IMPACT DATA. TEST SPECIMEN (S/N 024)
TEST OFSCRIPTION INLET PRESSURE=415 PSIA (NOMINAL)

ŤĖSŤ NUOĐER 6

PÄŘŤ SE

***	***	FI NVMETFF	CONDITIONS	***	***********	ŤESŤ SPE	ČÍMEN ÍNLET Ö	ONDĪTĪONS:
 	FLOUMCTER ON	***	***	FLOWMFTER TWO	****	, , , , , , , , , , , , , , , , , , , ,		
FLOW RATE (ACFM)	PRESSURE (PSIA)	ŤĖMP (DEG• Ē)	FLOW RITE (ACFM)	PRESSURE.	TEMP (DEG. F)	PRESSURE (PSIX)	TEMP (DEG. F)	ĀVĢ <u>Flow Rāte</u> (ĀCFM)
.47	49.7	8จ๋∙ĭั	• 48	4B.9	84.9	416.6	я́3.6	.0566
.44	50,4	ห็จ่∗รั	. 44	49,9	34.7	416.5	" Å3,6″ ~~	.0529
.40	<b>5</b> ນ.]	93๋∙โ	,41	49.5	Á4.Ĭ	416.4	83,6	.0487
•35	50.4	84.1	• 75	49.9	ค⊼ั. เ	416.7	ê <b>3.</b> 6	.0457
.31	50.2	ยร่• เ	•á1	<b>49.9</b>	āĀ.Þ	476.4	83,5	.0368.
•26	49.9	ยำ•ำ	,35	49.Š	<b>8</b> 4 • 4	416.4	83.8	.0306
•21	50 <b>.</b> ∑	A5	•ão	49.9	84.6	416.4	64.1	. ñ2¥9·
<b>.</b> 16	50.4	83.5	•15	50.3	8 <b>4</b> .6	416.À —	64.1	.0190
•12	5.04	93•8	•11	รัก•โ	84.8	416.5	84.3 T	• 6134
.12	p.i. • J	83.7	•īi	49.9	Ř <b>4.</b> 6	476.6	64.2	.0133
.16	49.9	B : • 7	•16	49.9	84.7	4=6.6	84.2	.0195
•21	49,9	44.7	•21	49.7	84.7	416.6	84.2 T	• 0523.
.26	49.7	84+5	, -6	49.3	84.7	416.5	84.2	.6312
.31	49.7	8-1-6	. 20	49.4	вй"я	416.	84.2	.0363
•35	49.9	৪৯•5	. 45	49.3	84.7	416.5	64.1	.0402
.4h	49.9	₽\$+5	•41	ă9 <b>.</b> 3	84.7	416. à	84.1	• ñ482°
.44	49.7	8֥6	. 4	49.7	94.7	416.5	84.2	.0553
.48	49.7	8 ~ • 7	.48	۸8.9	84 <b>.</b> 7	475.3	84.2	• n569°

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7/23/76

CEERN CONDITION-IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. PRIOR TO IMPACT DATA. TEST SPECIMEN (S/N 024)
TEST DESCRIPTION INLET PRESSURE = 415 PSIA (NOMINAL)

ŤĖSŤ NŮMĀEP 6 PART ZE

			lima Con	-00			
PRESSURE (PSIA)	AVG TEMP (DEG. F)	ÄVG FLOW RATE (ÄCFM)	YROSS DIFF. PRESS PRIMARY (PSID)	GRAŠS DIFF• PRESS SECONDARY (PSIA)	_ ĀVĢ GROSS DIFF• PRESS (PSID)	TARE DIFF. PRESS (PSID)	DIFE. PRESS (PSID)
416.5	83.6	<u>.</u> ;566	296.502	296.502	296.502		ž96.ŠñŽ
416.0	83.6	• 1529	255.Ï52.	255.152	. 255.152		
416.0	83.6	"č487	210_536	278,536	218.536	, ,•ôQô	<u> </u>
416.0	⊎3.6	<u>.</u> 2427	179_080	179.080	179.080	000	179.079
416.0	83.6	.ភ្.68	144.674	144.674	144.674	. <u>0</u> . 00 0	144,679
416.0	<b>83</b> ⁴8	_0306	1141055	114.355	114.055	000	ĨĨ4.ñŚŚ <sup>,</sup>
416.0	84.1	.ñ249	87.677	88.172	87,88 <u>9</u>	, <u></u> ô <u>0</u> ō	87.869 <sup>.</sup>
416.0	84.1	.0190	64,969	64.498	64.204	000	64.203
416,0	84.3	.õĩ34	44.843	44,615	44.729	<u> </u>	
416,5	34.2	.:[33	44.285	44.096	_ 44,190	000 <u>0</u>	44,196
416.6	84-2	,∧195	65 <sub>-4</sub> 59	66.192	65.901	000	65.900
416.6	84.2	. 0253	89 073	90.066	89.570	• ġġġ	89,569
416.0	94.2		116.896	₹ã6,896	116.896		<u> 776.696</u>
416.0	84.2	. กิ363	143.411	143.411	143,411	• ō ḍ ā	143.411
416.0	84.1	.;422	ĩ77.8ĩ7	177.877	177.817	500	<u> </u>
416.0	84.1	•ñ48ż	217.273	217,273 .	_ 217.273	<u> ōoō</u>	<u> </u>
416.0	84,2	<b>"</b> 1523	255_152	255. 152	255.152		25 <u>\$</u> , <u>151</u>
415.4	64.2	<u>.</u> 2569	3ñ\$.9 <b>7</b> 2	3ñ5 <b>.</b> 97ã	302.975	. ô o ō	365.971

TARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 7.56933E-01 (ACFM)\*\*2 +

PAGE: 3 DATE: 7/23/76

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEANCONDITION-IMPÁCT/FLOW RATE VERSUS DIFFERENTIAL
PRESSURE. PRIOR TO IMPACT DATA. TEST SPECIMEN (\$10 024)
TEST DESCRIPTION INLET PRESSURE = 415 PSIA (NOMINAL)

TEST NUMBER 6

PART SE

	***	ង់សង្គង់ <b>ង</b> សំងង់	******	ŤEŚT S	SPEČIMEN ÍNL Marana	EL CONDILION	S «««អំពល់សំសំសំ	សំសំសំសំសំសំសំសំសំសំសំសំ	*******	*****	NET DIFFERENT	TALI PRESS	<del></del>
ŀ	PREŠSV		ងងង់ងងងងង់	TEMPER TURE	***	***	*******	FLOW RATE	·	 		· · · · · · · · · · · · · · · · · · ·	
	KG/SQ CM	PS1A	ĐEĠ. K	DEG. C	DÉG. F	LITERS/ Min	AČF14	ŚČFM	K <b>G</b> \H <sup>®</sup> GNŞ	GNŽ LAS/HR	ŘG/SQ ČÚ DÍFFERENTIÁL	PSID	[J
	29,293	416.6	3.1.8	28.7	83.6	44.3	. 1566	ĭ.564	3.079	6.788	20.8461	296,502	
	29.247	416.0	301.5	>A.7	83.6	4].7	• 1529	Ĩ.46ñ	2.875	6.338	17.9389	255,151	
	ž9,247	416.0	361.8	2Å.7	83.6	38.0	. 1487	1,342	2.643	Ĕ.ŝē7	15,3646	218,536	
ļ,	ž9.247	416.	3.1.8	28.7	вз.6	33+1	• 427	i.i78	2•3 <u>79</u>	Ś•īïž	12,5905	179.079	
	29.247	416.0	301.8	58.7	83.6	58.6 *	.0368	1.015	1.999	4·4n7	10.1715	144,673	,
	<del>2</del> 9,247	416,0	301.9	2គ៌.8	83.8	23.6	.0306	.843	1.660	3.660	8.0189	114,055	
	29.247	416,1	302.1	28.9	84.1	19.1	• · 249	.686	1.351	2.979	6. 792	87.889	
	29.247	416.0	1.508	28.9	84.1	14.5	•0199	.523	1.029	2.269	4,5139	64,263	
	29.247	416.	зňź.ž	žọ.1	84.3	ាំកំ∗ា	.1134	<u>.</u> 369	.7ž?	1.602	3,1447	44.729	
ŀ	ž9.293	416,6	39.2	29.11	84.5	10.n	. 1133	.368	•7 <u>24</u>	ĩ• <u>š</u> 96	3.1069	44.190	
	29,293	416.6	3,2.2	ຮຸ່ອຸ້ນ	84.2	ĩã.1	•a195	537	1.058	2.333	4,6333	65,900	 !
	ž9,293	416.6	3,5.5	ຊິ9.າ	8 <b>4.</b> Ā	ĩ9.5	• 6253	.699	1.376	3.834	6,2973	89,569	
	ž9.247	416.0	oôz.i	žo, o	87.ž	24.2	•7412	.859	1.691	4.728	8,2186	116.896	_
	ē9.247	416.0	3,2,5	29.0	64.2	ลีก์∙1	.0363	1.000	1.969	4.346	10.0828	143,411	
	ž9,247	4i6.0	3ก่อ.i	žή.9	84.1	35.7	,nåżã	1.143	ż.290	5.049	12,5,18	177,917	
ij	ź9,247	416,5	302.1	ż8 <b>.</b> 9	84.1	37.5	• ŋ4̃8ž	ĩ.328	2.674	5,763	15,2758	217,273.	
	29.247	416.0	302.1	29.0	84 <b>.</b> ž	46.7	•n523	ĩ.442	2.839	6.265	17.9389	255,151	 ti
	29.201 ****	415.3	302.2	\$9.1	84.5 *****	44.3	•0569	ī.565	3•u8j	6.793	21,5119	305,271	<sup>U</sup>
	ž9,254	416,1	305.0	28.9	84.n			-					
	.017	.2	٠í	)	•s	DEVIATIONS	5						

FLOW PATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1

DATE: 7/23/76

CLEAN CONDITION-IMPACT/FLOW RATE VERSUS DIFFERENTIAL,
PRESSURE, PRIOR TO IMPACT DATA, TEST SPECIMEN (SIN 024)

TEST DESCRIPTION INLET PRESSURE = 700 PSIA NOMINAL

TEST HINGER 6 Qé takq

	***	***	PLOWMFTFF (	? :ONOITIONS	****	****	ŤEŠŤ SPE	CIMEN INLET C	ONDITIONS	
ť	****	FLOWMUTEP ONI-	***	****	FiOWMETER TWO	***	•	,		
	FLOW RATE (ACFM)	PRESSURE (PSIA)	ŤEMP (DEG• Ē)	ř ow Råte (AČFM)	PRESSURF, (PSIA)	TEMP (Deg. F)	PRESSUAE (PSIA)	TEMP (DEG. F)	AVG FLOW BATE (ACFM)	
	.84	49.7	7 • <del>7</del>	•91	ĄŤ∙ā	75.5	700.0 T	74.1	.0608	
	.76	50.5	75.4	.81	48,5	75.4	7âว₌ก็	73.9	, 0552	
	•67	5.4	75·6	•71	49.ĩ	75.5	786.4	74.1	• 6489'	
B	•58	+9.7	7 • <del>7</del>	•60	8.7	76.7	756.8	74.2	.0416	
	.49	49.7	74.0	.50	48.9	76.3	755.6	74,5	.0348	J
	.40	44.9	73.4	• 40	40.3	76.2	707.0	74.A	.02A0	'
	•31	\$1.05	73.7	•31	49.9	76.5	784.8	75.1	, 022n	
	.26	50.4	Ťĩ•ĺ	•25	ē0.Ī	76.7	7ព៌ក <b>ុ</b> ក៌	75.4 °	, 615j	
	•21	49.9	74.6	.20	49.9	77.0	700-0	75.8	. 6147	
Ĺ	•14	۵٬ •S	75•1	•14	5^•Ĭ	77.3	700.0	76.2	.0100	-
	•14	2"15	76• 4	• 1 4	59 <b>.</b> Î	78.2	703.9	77.á	. 0099	ij
	.82	49.7	76.3	.žl	<b>49</b> •5	78.2	713.9	77.ž	. čīšī	- '
	.26	49.9	74.1	.26	49.7	7Ã.≯	7ก็ <b>з</b> ื่อ	77.1	.0186	-
	.31	49,7	7ë.9	•31	49.á	48•5	7≒3.9	77.Ī	. 0216	•
	• 40	50.4	75.6	04.	<u>49.9</u>	78.2	7ñã.9	76.9	. ñ264	-
1	.49	49.7	7≅∙å	<u>.</u> 50	48.9	78.3	700.0	76.5	.0347	
	<b>.</b> 58	49.7	74•ŝ	•6 °	48. <del>7</del>	77.7	755.5	76.1	.0414	u
	<b>.</b> 67	50.1	Ź~•Ī	71	8.7	77.9	7ភិកិ.តិ	76.0	.0484	1
	.76	5 .4	73.5	.81	48.7	77.1	7ŏŏ.ñ	75.4	.0554	
	.84	5 •S	72.4	•91	48.3	76.5	700.0	75.ô	. 0616	

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7/23/76

TEST NULHER 6

PART 50

CLEAN CONDITION-IMPACT/FLOW RATE VERSUS DIFFERENTIAL
PRESSURE. PRIOR TO IMPACT DATA. TEST SPECIMEN (S/N 024)
TEST DESCRIPTION INLET PRESSURE=200 PSIA NOMINAL

TĻST	žbE∨ĭW€N	INLET	CANDIT	InNS.	
***	***	****	*#####	****	*###

PRESSURE (PSIA)	AVG TEMP (DEG. F)	řiow Rath ("ČFM)	GRASS DIEE, PPESS PRIMARY (PSID)	GRASS DIFF. PRESS SECONDARY (PSIO)	īve egoss Dīff. Press (PSID)	DIFF. PRESS (PSID)	ĎIFF• PRESS (PSID)	
700.0	74.1	. <u>ō</u> é08	ž49 360	249 <b>.</b> 36ñ	249,360	0.000	249.360	
700.0	73,9	. 1552	217.441	217.440	217,440	÷ô.ŏ00	2ī <u>7.44</u> 0	<del></del>
700.0	74.1	. ñã89	184.887	184.887	184.887	-0.000	184.8 <u>87</u>	
700.0	74.2	_6416	<b>151.07</b> 0	151.070	151.070	-0.001	<u>īšī.ô</u> 70	<del></del>
700.0	74.5	.7348	īzī,362	121.362	121.362	÷0.001	<u>īžī.36ž</u>	
700.0	7/+8	• 0580	92.917	93.466	93.391	÷ō.00Ī	93.391	. d
700.0	75 <b>.</b> ĭ	<b>.</b> 0220	<b>7</b> 6_70∩	71.426	71,063	-0.001	71.763	
700.0	75.4	.ñ183	57.054	57.836	57 <b>.</b> 446	<u>.</u> 0.001	57.446	
700.0	75.8	. 147	45 7999	45.77Å	45,88 <u>4</u>	-0.001	45,884	
700.0	76.2	.0170	30.541	30.22 <u>1</u>	30,380	-0.001	30.380	<del></del>
703.9	77.3	• ენგგ	30.353	31,221	30.287			
703,9	5.77	.ñĩ51	47,548	47.091	47.319	<u>-0.001</u>	47.319°	<sup>1</sup>
7n3.9	77.1	• ·186	58,811	59,733	59,272	-0.001	59 <u>. ž</u> 72	-
703.9	77.1	.ភិខាក	69 <sup>-</sup> 9 <sup>-</sup> 1	71.11å	70,531	₹0.001	<u></u>	
703.2	76.9	.294	94.61ī	95,765	95,186	<u>-0.001</u>	95. 186	_
700.0	76,5	. 634 <b>7</b>	ĨŹĪ_046	121.026	121.046	<u> -0.001</u>	ĨŽĨ.ñ46	·
700.0	76.1	.6414	<b>เริก</b> โ122	150.122	150.122	-0.001	Ţšô,īžē	
700.0	76•č	<u>.</u> 7,484	ĩ83 <b>.</b> 623	183,623	Ĩ83.623	-ā.000 <u>.</u>	<u> </u>	)
700.0	75.4	<u>.</u> 0554	<b>219.652</b>	239,6=2	219,652	-0.000	žī9.65Ž	
700.0	75,0	.0616	255 049	255,049	255,049		255 <u>. ñ 49'</u>	

IARE DIFF. PRESS = -3.60000F=04 + -3.37610E=02 (ACFM) + 6.33359E=01 (ACFM) ##2 +

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 7/23/76

CLEAN. CONDITION-IMPACT/FLOW RATE VERSUS DIFFERENTIAL
PRESSURE. PRIOR TO MEACT DATA. TEST SPECIMEN (S/N 024)
INLET PRESSURE = 700 PSIA(NOMINAL)

TEST WIMBER 6 PĀRŤ 50

	***	- នងដត់តំងងដ <b>ាំ</b> ងត	******	ŤEST S	PEČIMEN ÍNĽ	FT CONDITION	ទ តំត់ទំនិត់តំនក់តំន		តិម៉ាតិម៉ាម៉ាម៉ាម៉ាម៉ាម៉ា	****	NET DIFFERENT	TĂL: PRESS:
ij	PRESS!	)ŘĒ ******	***	Temper Ture	***	****		FLOW RATE	****	********		
	KG/SG CM	Pala	DEG. K	ñEG. C	pėg, è	LIŤ;RS/ MIN	4ĈFH	ŚČFM	KĞ∕H¢ GNŞ	GNŽ ĽBS/HR	KG/SQ ČÜ DIFFERENTIÄL:	PSID
	49.212	700+4	ž96 <b>.</b> 6	ži.4	74.1	85̃•9	•668	2.87ī	5,653	12.463	17.5318	249,360
	49.212	700.0	296.4	53.3	73.9	75.1	• วิธีธิรั	2.611	5.141	ĭī.4335	15.2875	217.440
	49,212	700.V	296,5	23.4	74.3	66.4	.9489	ŝ.3 <u>1</u> 3	4,553	วีกั•ก์39	12,9989	184.587
ï	49,212	700	296,6	âi.4	74.ž	56.2	,÷416	1,966	3.871	8,534	10.6213	151.070
	49,212	700.0	296.8	24.6	74.5	46.7	•1448	1.645	3.238	7.139	6,5326	121.362
	49,212	700.0	296.9	29.8	74.8	37.2	.028n	Ĩ.322	2.663	5.739 <sup>-</sup>	6,5661	93,391
	<b>49.</b> 212	700. U	297.1	24.n	75.1	29.3	•0 <u>2</u> 20	ĩ,À37	2.042	4.502	4,9962	71.063:
	49.212	700.0	ã9 <b>7.</b> 3	Ž4.1	75.4	24.1	.~183	<b>.</b> 860	1.694	3.735	4.0389	57,946
	49.212	700.0	597 <b>.</b> 5	24.3	75.á	٦ <b>٠</b> ،۸	.0147	.694	1.367	3.014	3.2260	45, 564.
ŧ,	49,212	700.0	297.7	ē4.6	76.Ž	Ĩ3•0	.0100	471	•9ē?	2.643	2,1359	30.380
	49.489	763.9	298.3	25.2	77.3	<b>13</b> •0	•0099	•47ō	•9 <u>2</u> 5	2.639	2.1294	30.267
	49,489	703.9	ž98 <b>.</b> 3	ž5 <b>.</b> 1	7Ť.š	19.9	•0151	.7îĭ	1.400	3•ñ86	3.3569	47.319
	49,489	703.9	298.2	25.1	77.1	ē4.6	.0186	.881	i.734	3.823	4.1672	59,272,
	49,489	7,3,9	298.2	25.i	77.1	28.8	.4214	1.722	2.012	4.435	4,9586	70.531
	49.489	703.9	598.Ĭ	54.9	76.9	38̂•0	.0584	1.341	2.640	5.82Î	6,6923	95, 186
ľ	49.212	760.U	297 <b>.</b> 9	2 <b>4.</b> 7	76.5	46.4	.0347	1.633	3.215	7.68	8,5104	121.046
	49,212	700.0	297.6	24.5	76.₹	55.8	.3414	1.950	3.840	8.466	īó,\$546	īšo.122
	<b>49.212</b>	700.0	297.6	27.5	76.0	6Е5	.0484	2.281	4•491	9.900	12,9100	183,623
	49,212	700.0	297.3	ž4.1	75. <del>4</del>	75.1	•nŝ54	2,611	5.141	ĭī,334°	15.4431	219, 052.
	49.212	700 • · ·	297.4 ****	23.9 688688	75.ň ******	83.9	•n616	2.9ñ6	5.722	72.674	17.9317	255', 049
	49,201	700.9	297.4	24.2	75,6							
	•1n4	1.5	•5	•5	Ĩ • °	DEVIATIONS	s					

PAGE: 1 DATE: 7/23/76

TABLE 63 FLOW RATE VEPSUS DIFFERENTI L PRESSURE

CLEAN CONDITION-IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. PRIOR TO IMPACT DATA. TEST SPECIMEN (S/N 024) INLET PRESSURE = 1000 PSIA (NOMINAL)

TEST NUMBER 6

Å∧RŤ 5C

TEST DESCRIPTION

	*******	***	FLNWVETEF	R CONNITIONS	*****	****	ŤĖSŤ SPE	ČĬMEN ÎNLET Č	ONDŤŤĬONS	
r!	***	FLOWM:TER ONF		****	FLOWMETER TWO	ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្	·*			
	FLOW RATE (ACFM)	PRESSURE (PŠĪ <sub>A</sub> )	ŤĖMP (DEG• É)	FLOW RITE (ACFM)	PRESSURE.	ŤÈMP (ĴEG• Ĕ)	PRESSURE (PSIA)	TEMP (DEG. F)	ĀVĢ FLOW RĀTE (ĀCFM)	"
	•83	50.3	67.0	•91	48.∃	42.3	1407.9	69.6	.0425	
	.75	50,5	66.5	.61	48.7	71.9	inā7.9	69.2	.0384	
	•67	p0.3	66+3	•71	48.7	77.5	Ĩ^ÓŤ.9	68.9	. ñ338	
1	•58	49.7	66 • >	.61	48. ₹	71.1	996.3	68.7	• 0295·	
	.49	49.7	66.5	.50	48.9	77.3	าักกิ7ี <b>.</b> 9	68.9	. ô243	
	<b>.</b> 40	50,1	67.1	.20	19.5	77.6	ĩảnĩ.9	69.4	. 019B	
	•30	49.7	67.7	.30	49.3	77.9	ĩả07.9	69.8	.0149	
	•26	49,9	68.5	.55	49.5	75 <b>.</b> 3	1507.9	76.4	.0126	
	•21	50.1	60.5	0ۥ	49.9	75.6	1407.9	76.9		
•	•13	49.9	69.9	.13	49. a	73.5	1407.9	71.4	.0065	
	•13	49.9	7° •6	•13	49.9	73.8	1/07.9	72.7	.0065	1
	•51	49.7	77.4	.51	49.5	72.9	1407.9	75.7	.0104	
	•56	50.1	71.1	• ē6	49.9	73.9	ī^ô7.9	72.5	.0129'	
	•30	49.5	77.7	• ÷1	49.1	74.8	Ĩ^ō7.9	72.3	. n149'	·····
	•40	49.7	75.0	• 4 0	49.1	73.6	Ĩnō4.ñ	71.6	. ō197·	
i	<b>.49</b>	56.1	69 • Ž	•Š1	49.3	73.2	1604.n	71.2	.0247	•
	•58	50.1	6É.	• 50	8.9	ĩž.ĩ	1704.0	70.5	. 0292	· ——-
	<b>.</b> 67	50.1	67.5	<b>.</b> 71	ልፀ.ን	7ž.ī	โวô4์∗ô	69.8	.0339	
	•75	54.5	64.7	•B1	48.7	71.3	โจก์จั.ก์	69.ñ	. 038A	
	.84	50,3	66.2	.91	48.3	7ñ.6	นึ⊓อั4•ก็	68,4	_0429·	

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# TABLE 63 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7/23/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION- DEPACT VERSUS DIFFERENTIAL

PRESSURE. PRIOR TO INPACT DATA, TEST SPECIMEN (S/N 024)

THE THE PRESSURE = 1000 PSIA (NOMINAL)

RESSÚRE (PSIA)	AVG Temp (deg. F)	TVG FLOW RATE ('ČFM)	ÉRASS DÎFE PRESS PRIMARY (PSID)	GPOSS DIFF. PRESS SECONDARY (PSIO)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS	NET DIFF. PRESS (PSID)
1007.9	69.6	_ñ425		165.281.	. 165.081	_ (RSID)	īéš, áéž
		·	ī65.081 ī45.487				165,487
.007.9	69.2	. 384		145.4R7	145.487	. <u>#0</u> .000	
007.9	68.9	.03nB	1251260 	125.260	125.260	-0.000	
996,0	68.7	•ñā95	104,401	104.421 -	104,401	÷ά.00ō	<u> </u>
007+9	68.9	. 243	84.627	85.122	84 <b>8</b> 7 <u>4</u>	~0.00 <u>0</u>	<u>04.874</u>
.007.9	69•4	.0198	66.699	67.1.7	66.903	~ŏ.00ó	£6.9.66
1007.9	69.8	.ñī49	48.887	49.409	49 <u>.148</u>	-0.000	49,148
.007.9	70.4	•0 <u>1</u> 56	41.515	41.226 .	41.370	000.000	41.371
007.9	70.9	.ôī11	3ž.696	32.4~7	32,551	±0.000	32,552
.007.9	71.4	.កំតិ65	20.720	23.51š .	20.628		ŽŎ,ÁŽĐ
.007.9	72.7	.0065	20.490	20.5 <b>1</b> \$ _	_ <u>2</u> 0.503	<u> </u>	<u>20.503</u>
.007.9	72+7	•öī·4	33.442	33,386	33,414	÷0.000	33.414
.007.9	72.5	.8229	42 <b>.</b> 507	42.12.	. 42.415		42.475°
007.9	7z.3	. ñ Ī 49	48_887	49.449	49.148	±å.å9å	<u> 49.148</u>
004.0	71.8	. 197	66.323	66.797	66.557	-0.000	66.557
.004	71.2.		85 <b>.6</b> 13	86.386 .	85.999	-0.000	85.999
.004.0	70.5	, č292	105.033	105_433	105.033	-à.00à.	<u> วิดีร์ ก็จ๋ว</u>
004.ÿ	69 a R	<u>, : 3</u> 39	ī25 <u>.</u> 576	125.576	125,576	0.000.	125° 576
004.0	69.0	.ñ.384	146_435	146.435.	146.435		Ĩ46.435
004.0	68.4	.0429	167.619	167.619	167.610	±0.000	

TABLE 63 FLOW RATE VERSUS DIFFERENTIAL PRESSURE PAGE: % ... DATE: 7/23/76

CLEAN CONDITION. IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE, FRIOR TO IMPACT DATA. TEST SPECIMEN (S/N 024)
TEST DESCRIPTION INLET PRESSURE = 1000 PAIA (NOMINAL)

TEST MUMAER 6 PART SC

TEST SPECIMEN INLET CONDITIONS
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NET DIFFERENTIÁL PRESS

n	PREŜS		****	TÉMPERATURE BÉBBBBBBBBBBBBB	****	<b>ក្</b> ដក់ម្ខិត្ត ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្នុង ក្ន	ងងប់ឧបកព្រំគំមត់ 	FLOW RATE	******	*******		
	KG/SQ CM	PSIA	DEĆ. K	DEG. C	DEG. F	LİTERS/ MÎN	ÃČĚM	- šcřn	, K <mark>G</mark> \HΒ . GNΣ	GN2 LBS/HR	KG/SO ČH DIFFERENTIĀLI	PSID
	70.865	1007.9	294.1	27.6	69.6	84.4	- 1425	2,913	5.735	12.644	11,6064	165,082: 1
	70.865	1007.9	293.8	žā.7	69.5	76.0	.1384	ź,636	5.191	11.443	10.2žB7	145,487
	70.865	1007.9	-	•	69.9	66.7	_n33A	2.322	4.57į	10.078	8.8666	152,560 (
ļ.		396.A	293.7	27.5		57.3	.n <u>2</u> 95	2.302 2.001	3.940	8.567		104,401
Ī	Ť0.029 ≚- 0.5		293.6	2n.4	69 <b>.</b> 7						7,3401	
	Ť0.865	1007.9	₹9 <b>3.</b> 7	ว่กิ.ช	68.9	47 <b>.</b> 5	.^243	i.673	3•29 <u>3</u>	7.261	5,9673	84.874.
	ŤQ.863	1007.9	293.9	2ñ.8	69.4	3ñ.4	.nī98	1,360	2.679	5.963 ~	4.7038	66, 203
	ŤQ.865	1007.9	294.2	ខ.្ពី 🐧	69 <b>.</b> 8	28.9	, a 149	1.025	\$.019	4.451	3,4555	49,146
	70.865	1007.9	ô94 <b>.</b> 5	21.3	7ñ.4	24 • ?	• 1Ī ¤6	863	1 • 69,5	3.745	2.9ñ86	41,371
,	70.865	1007,9	294,8	żī.6	76.9	19.5	.01nī	,694	1.36?	3.ก็ไล้	2,2896	35. 555
1	70.865	1007,9	295.1	21.9	77.4	ī <b>ē∙</b> 4	• 0065	447	.8 <del>7</del> 9	1,939	1.4503	20.628
	70.865	1007.9	é95.8	22.6	7ã, Ť	12.2	-0065	.442	.8 <del>7</del> 1	ĩ.ợặĩ	1,4415	20.503
	70.865	1007,9	295,8	22.6	7ź.7	19.9	.01ò4	, 7 o 7	1.391	3.ñ67	2,3492	33,214
	70.865	1007.9	295.7	22.5	72.5	24.8	• 129	.881	1.735	3.826	2.9821	42.415
	Ťg.865	1007.9	295.5	22.4	7ž.3	źñ•8	• 1149	ī.óēó	2•00₿	4.426	3.4555	49: 148
	70.586	1004.0	295.3	22.1	វិត្តិ	38.1	.^ĭ97	1.343	2.645	ร็•ช่วกั่	4,6795	66,557
Ĺ	70.586	1004,0	294.9	žĩ.8	îī,ž	47.9	•9247 °	1,681	3.37ô	7.298	6+0+6+	85'-999'
	70.586	1004.6	294.6	21.4	77.5	56.9	• ŋឨ92	ĭ,99ñ	3.919	6.640	7.3846	105.033
	70.586	1004,0	294.3	21.1	69.8	66.6	•0339	j.313	4.555	10.043	8,8589	125.576
	70.586	1004.3	293.7	27.6	69 i	7š.7	. 1384	5.638	5,175	11.409	10,2954	146,435
	70,586	1004.u	293.4 #####	27.2 44444	68.4	84.9	. 1429	. 94q	5•7ėB	72.761	11.7942	167.610
•	70.740	1006.5	2,4.5	žī.₃3 ,	75.4		,, .		,,			
	.163	5.4	.7	.7	ĩ•2	QEVÎATÎ DN	s	• .		بيدر رستيست د .		

## FLOW RATE VERSUS 61 FLERENTIAL PRESSURE

FLUWMETER TWO

PAGE: 1 DATE:--7-26-76-

TEST NUMBER 6

FLOWMLIER ONE

IS THAN

TEST DESCRIPTION

CLEAN CONDITION - IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE: AFTER 80 HIGH PRESSURE (10,000 PSIA) GN2 IMPACTS. TEST SPECIMEN (S/N 024) INLET PRESSURE = 415 PSIA NOMINAL.

TEST SPECIMEN INLET CONDITIONS

 $\mathsf{FLOWMETER} \ \ \mathsf{CONDITIONS}$ 

ı	***	· · · · · · · · · · · · · · · · · · ·			*******	****				
,,	FLOW HATE	PHLODUKE	Τ <sub>Ε</sub> ΜΡ (ΔΕG. F)	FLOW RATE	PRESSURE, (PSIA)	ŢĘMP (PĒĠ, F)	KRESSURE. (PSIA)	AVG TEMP. (DEG. F)	AVG FLOW RATE (ACEM)	
	" (ALEM)			(AC <u>F</u> M)						
	÷ŘΤ	44.1	78+5	•61	47 <u>•</u> 9	8:.3	416.5	79.4	₹0 <b>3</b> 8₽,	
	<u>• !6</u>	アンセー	78.3	•er	4 <b>5.7</b>	84, • 3	415.2	79.3	•0535	
	ិ៍ខ្ព	74.4	78•1	•,71	49.1	50.2	413.9	79.2	* ០ដី១ី <b>ខុ</b> .	
	• 59	₽⊻•#	78+=	•6 <u>}</u>	49.7	8n • 1	413.9	79.1	0726	
ķ	∙⊅ប្	⊅č*ô	77 <u>•</u> 9	•51	49-9	80.1	<b>419.9</b>	79.0	.0616	
	±41	à차호	78.,,	<u>•</u> 4 <u>1</u>	50.1	80.1	413.9	79.1	•0494·	u u
	•ុន្ធរ	P 4	78.4	-31	ลัก•์S	<b>გ</b> ი•3	413.9	7 <u>9.</u> 4	.0383.	
	<u>•</u> 46	P5.6	76.6	.26	50.4	8n <u>.</u> 4	413.9	79.5	.0321	
	•22	# <b>#</b> *]	B1 <u>±</u> 8	•51	49,7	¹ 82 <u>•</u> 7	<del>4</del> 21•1	82.3	10254	
	<u>.</u> 15	57.1	81 ±9	•15	50.1	<b>62.</b> 8	421.1	82 <u>.</u> 4	•0j80	
ľ	.15	24.1	0.58	٠١۶	Sv.1	82.5	421.1	82.3	<u>•0179</u>	
	<u>.</u> 42	Py•1	A1 •8	•22	49.9	82.3	421.1	82.0	±0264·	Ä
	<u>.</u> 2?	#7.9	81 • 7	•5ē	49.9	85 <b>•</b> ę	420.4	85•5	*0316,	
	•वह	1 ۽ ٻڙ	81 <b>±7</b>	•32	49.9	82.7	419.8	82•2	•0380	
	<u>.</u> 41	47.9	81 4	•41	44.3	7 ج ح	419.8	82.1	.0487	
	<u>.</u> 50	#7.	81:1	•51	47.1	¢2 <u>•</u> 5	<del>2</del> 19•1	81.6	,0593	
1	• 5 9	** ** * * * * * * * * * * * * * * * *	°6 <u>∗</u> 9	<u>.</u> 61	48.7	82.5	418.5	81.7	, q <b>7</b> 05.	1
	• 08	47.1	B <u></u> ‡7	.71	48 <u>•</u> 5	85.5	417.8	81 <u>•</u> 5	· 0815.	U
	ه ژه	77.5	9 • 7	.81	47.9	85.5	416.5	81.5	,0919	
	ទិនិរ	47.5	81 • 1	<u>.</u> 87	47.8	95.5	<del>4</del> 15.9	81.7	*0885	

LTOM BALE AFRANS DIFFERENTIAL BRESSÄKE

PAGE: 2

DATE: 7-26-76

CLEAN CONDITION - IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. AFTER 80 HIGH PRESSURE TEST HUMBER 6 IS TRAG TEST DESCRIPTION (10,000 PSIA) GN2 IMPACTS. TEST SPECIMEN (S/N 024) INLET PRESSURE = 415 PSIA NOMINAL. IEST PROLIMEN INLET CONDITIONS GROSS DIFF: PRESS GROSS DIFF PRESS. SECONDARY NET' DIFF PRESS DIFF. PHESS AVG AVG i DIFF. PRESS PRESSURE FLON RATE PRIMARY 18,40 (PSIU) (PSID) . . ... (P\$10) .''(PSID)\_\_\_\_ <u>(PSID)</u> (Paint (DEG. F) (ACFIII) 298.978 298,980 298,980 416.7 14.4 . ღ9ა5 298.980 260.421 415.6 19.3 . 1929 200.422 260.422 . 260 . 464 .001 205,429 205.430 205.430 .001.... .0836 205.430 41207 17.2 163.060 163.050 .001 163.078 19.1 . 3725 163.080 413.2 127.083 127.681 127.683 .001 413.7 19. .,616 127.684 94.814 94.449 .000 ---- 94.447 . 6474 94.08\_ 410.7 (9.1 ---69,219 68,911 69.53n 69.220 .000 413.7 19.4 EGC0. 56.292 413 7 14.5 -3341 56,014 59.572 56.493 434935 43,936 441.4 02.3 . 254 43.346 44.526 .000 29.858 30.310 .000 . . .. .... 30+309. .01dc 30./62 421.1 02.4 30.548 .01/9 34.992 30.54% .000 461.1 36.3 30.100 . .46.298 . . ... 46.299 .000 45.50/ 47.091 461.1 4200 .::204 57,646 58,157 57 54! .000 .0316 57.142 464.3 24.55 71.042 . 71.045 419.0 06.2 .0386 70.661 71,426 .000. 96.710 96.716 .0.00 \_\_ .. 96.709 ... 417.0 oc.1 . 487 96.71: 125,154 \_\_125,153.\_ .\_. \_ 417.4 41.6 د د د د د د 125,154 125.154 .000 159.919 159.919 159.919 ......... 159 918 414.7 21:7 .07.5 f 501.69! .001 201.636 . 3814 201.63/ 201.637 411.0 01.5 . 1919 248.411 248,412 244.412 244.414 .001. 410.0 61.5 291.075 .6962 291.070 291.178 415.3 D1.7 imRE D1FF. (MESP = -3.40000E-05 + -4.44000E-04 (ACEM) + 1.50933E-01 (ACEM) \*2 + \_ 0\_(ACEM) ##2\_\_\_\_\_\_

# TABLE 64 FLUW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 7-26-76

			•		, , ,	•	4.1	•	,		• • • • •	
			 	***	FLOW RATE	**	***	***	LENDER, TUKC	***	RE	**************************************
 	PSAD.	KG/SQ CM DIFFERENTIAL	Γ₽ <mark>5</mark> /ḤR	KPNHK RNS	sç <u>F</u> M	· ct···	LIŢĘRȘ/ MIN	DES. F	DEG. "	∩څوځ لا	Ьэ́та	Kē\žā čw
-	298.778	21.0203	11,203	ุร•ัจอัร <u>(</u>	2.742	. 4985	79,0	79.4	3.6	299,5	410,0	58°584
-	260,321	18.3094	11.319	5.134	2.608	.0939	74.9	79.3	26.3	294.4	415**	5å*Tå¢
•	205.429	14.4431	10.043	4.555	2.314	. 336	, 66 <u>.</u> 3	79.2	26∙∠	299.4	41212	Så•iî€i
•	163.078	11.4656	8 <u>.</u> 728	4.25%	2.010	7_6	57.6	(9.1	56*1	,199.3	41465	Săitái
-	127.981	8.9769	7.400	3.45/	1.705	<u>.</u> :-516	48.4	79.0	26.1	299.3	417.5	55.101
1I	94,447	<u>6•6</u> 403	5.938	2.693	1.368	· 474	38.6	79.1	<b>∠</b> 6∙∠	299.3	415.7	Sã≅⊺∩Í
- '	69.419	4.8666	4.596	5•085	1.059	•°383	59.6	19.4	26,3	299,5	412,2	Sà∓īñŤ
	56.492	3.9577	3-856	1:/47	ំពត់គ	• 351	24.7	79.5	26.4	299.6	415:5	Să≆ıni
-	43,735	3.0889	3.091	1.402	.7 <u>1</u> 2	. ,224	19.9	<b>5</b> 2∗3	۲۰۶۶	301.1	+21:1	29.504
-	30.308.	2.1309	5-192	-994	•ទល្	•010H	14•U	b2.4	28.₩	301.1	421.4	55.564
-	30.748	2.1477	2:179	.982	<b>.</b> 5,2	. 1119	13.9	¢2.3	₹•75	3, 1, 1	451.1	29.504
0	46,498	3.2550	3.20€	1,459	•739	264	20.7	ã5 <b>∙</b> 0	27.8	-01.0	451.1	29.004
-	57.246	4.0529	3.835	1.740	.884	••316	24.9	82.2	27.9	3.1.0	42/.2	5à°22¤
	71.042	4,9947	4.599	ร์•ักค5	1.059	,038g	Jo.0	ģ2 <b>,</b> 2	27.4.	301.1	419.0	5â <b>°</b> 21 दे
	96./09	6.7993	5.901	2.679	1.359	, 4u7	38.3	ÿ <b>2•</b> 1	27.8	361.	#14.5	Sã•21¢
-	125,153.	8.7991	7 <u>.</u> 175	3.257	1.653	•>59₃	46.9	ទ្ធា , ម	.7.5	300.6	415*	59:460
-	159,718	11.2434	8,524	3.565	1.964	.0705	56 <u>•</u> 11	#1.7	27.0	300.7	410.5	Sa <sup>*</sup> 4k1
, .	201.936	14.1764	9.892	4.48/	2.279	919	65.4	ង្គ1.5	27.5	361.6	41(20	59,475
,	240-411	17.4650	11.065	5 <u>•</u> 017	2.549	./919	73:3	<b>91.</b> 5	27.5	300.0	415,5	29,284
-	291.077	20.4648	11.794	P 444	2,717	. 982	78.4	91.7	27.0 44444	361.0 *****	415.2	89.230 88484
-								99.9	27,1	3ຫນ້.3	<u> 11/11</u>	29.243
-			***************************************				ńęalyľ 1002	1.3	:!	• 7	۵.5	<b>់</b> 183

PAGE: 1 DATE: 7-26-76

#### TABLE 65 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

Trot WUVGEK 6 He TRAG

CLEAN CONDITION - IMPACT/FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. AFTER 80 HIGH PRESSURE
TEST DESCRIPTION (10,000 PSIA) GN2 IMPACTS. TEST SPECIMEN
(S/N 024) INLET PRESSURE = 700 PSIA NOMINAL.

FLOW ETER CONDITIONS	TEST SPECIMEN INLET CONDITIONS
种种部分的合物性的特殊性性的特殊性性的特殊性性的特殊性性的特殊性性的特殊性性的特殊性性的特殊	*****************

			• • • • • • • • • • • • • • • • • • • •			•			•	
				******	FLOWMETER TWO	特殊计数数数数格格数数数	*****	44454444444444444444444444444444444444		
	AVG FLOW RATE (ACEM)	AVG TEMP (DEG. F)	ress <sub>u</sub> re (Psi <sub>A</sub> )	TEMP (DEG. F)	PRESSIRE. (PSIA)	FLOW R TE (ACFM)	TEMP (DEG: F)	(5517) bkf 57' kf	FLOW RATE	
_	.0610	75.2	703.9	76+8	4/•9	,91	73•7	77.9	• ន៦	
	• 0550	74.8	7n3,9	76.3	48.7	∗Ð í	73+2	p(.2	,76	
	0485	74.7	703.9	76. 2	49.1	•7ú	7~•1	5y . 4	• 67	
	40421	74.7	7 <sub>0</sub> 3.9	76.3	49.5	.60	73 • 1	⊃ı.4	.58	
	• 03591	74.8	700.0	76.3	49.9	•51	73•3	9;+4	•50	
	.0295	75.1	[00+0	76.5	49.9	• 41	73+6	5, .4	• 41	
	.0221	75•5	7n3.9	76.8	19.7	*31	74.2	47.9	,31	
	•0189	75.7	703.9	77.0	49.9	*50	74.5	55.1	.27	
	.0152	76.1	7.43.9	77.3	49.3	•2°	74-7	44.0	•22	
	.0096	76.6	703.9	77.7	49.2	•13	75.5	47.5	.14	
Ų	•0098	77.6	/03.9	78.3	50+1	.13	76.8	$\mathfrak{s}^{\tilde{n}+1}$	.14	
	•0157	77.7	7n3.9	78.5	511.1	• 22	76.9	50.2	•55	
. ~	0186	77.8	783.9	78.7	50.2	. 26	76.8	5 <sub>14</sub> .4	.26	
• •	• 0225	77.7	7,3.9	78.7	5,,.1	.31	74.7	\$6.5	•35	
-	.0291	77.5	703.9	78.7	49.7	.41	76-4	94.1	<u>,•</u> 41	
	.0353.	77.3	?n3.9	7B <sub>+</sub> 6	48.9	.51	76 • 1	45.7	<u>.</u> 50	
Ų	•041B	77.1	7,3,9	78.5	48.9	•61	75.7	47.9	•59	
····	•0484	76.8	703.9	78.;	48.3	,71	75:4	47.5	.68	
	.0546	76.5	700.0	78.0	47.B	.81	75.1	47.6	• 76	
	.0610	76.2	700.0	77•7	47 •B	.91	74.7	+7.7	<u>.</u> 84	

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TABLE 65
FLOW RATE VEPSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7-26-76

LEGA WAIE ACADOS DILÍCUENTITE EUCOSON

IARE DIFF. PRESS = -3,60000E-04 + -3,31610E-02 (ACFM) + 6,33369E-01 (ACFM) +2 +

PART 2H

TEST WUMBER 6

CLEAN CONDITION - IMPACT/FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. AFTER 80 HIGH PRESSURE
TEST DESCRIPTION (10,000 PSIA) GN2 IMPACTS. TEST SPECIMEN
(S/N 024) INLET PRESSURE = 700 PSIA NOMINAL.

10" (ACFM) ##3

TEST SPECIMEN INLET CONDITIONS \*\*\*\* gR05\$ GROSS DIFF. PRESS SECONDARY DIFF. PRESS AVG GROSS DIFF. PRESS DIFF' PRESS TARE 1ENP ۷VG DIFF. PRESS PRESSURE FLOW RATE (PSID) (PSIN) (PSID) "(PSID) (PSIA) (DEG. F) (xcfid) (PSIU) 703.9 15,2 124,206 124,206 124.205 40.000 124,209 .0610 108.720 108,720 -0.000 108.720 703.7 14.B .0550 108,720 92,918 92.334 91.746 -0.000 72.332 703.7 14.7 . 4485 78, 1163 77.704 77,704 703.7 14.7 . 421 77.344 -0.001 700.5 63,841 63.564 -0.001 63.664 14.8 . 359 63,486 708.7 .1295 15.1 50.580 31,199 50.890 -0.001 50.890 703.7 15.5 37,999 17,889 37.944 37,944 . "221 -0.001 703.7 15.7 ...189 32.395 31,9.16 32.00j -0.001 ~~32~701~ 705.7 16.1 . 152 25,490 25,3:3 25,401 -0.001 25,401 703.9 .009: 16.268 16,026 16.147 -0.001 16.147 13.6 , 4648 16,381 705.7 17.6 16,393 16,369 -0.001 16,381 26.951 703.7 17.7 . 157 26,993 26,910 -0.001 26,951 32,440 703.7 77.8 .0156 32.469 32,423 -0.001 32,446 39,857 703.7 39,923 39,790 -0.001 39.857 17.7 .(225 17.5 . 1291 51,832 52,464 52.148 52,148 702.7 -0.001 64.859 703.7 17:1 .1350 64.613 65,116 -0.7001 64.859 703.7 77.1 79.712 78.730 78,735 . . 418 78,461 -0.001 . 484 93,866 702.9 16.8 92,961 93.412 **→0.000** - ,9374131 107.140 700.7 107.143 107.140 #0.000° 1077140 16.5 .45.6 123,890 700.0 16.2 123\_89 123,890 123,890 ,061. -0.000

PAGE: 3 7-26-76 DATE:

TABLE 65 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PART of TEST NUMBER 6

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• 5

CLEAN CONDITION - IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. AFTER 80 HIGH PRESSURE TEST DESCRIPTION (10,000 PSIA) GN2 IMPACTS. TEST SPECIMEN (S/N 024) INLET PRESSURE = 700 PSIA NOMINAL.

NET DIFFERENTIAL PRESS TEST SPECIMEN INLET CONDITIONS \*\*\* PRESSURE FLOW RATE TEMPER TUPE \*\*\*\*\*\*\*\*\* KG/SQ~CM~ GNS GN2 LIT=RS/ PSID DIFFERENTIAL уСЕи SCEM ĸĞŹĤĶ LBS/HR KG/SQ CM DEG. F MIN **B**214 DEG. K nEG : 124-206 2.891 5.694 12,550 8.7326 297.2 75.2 83.3 . 161a 49.489 703.7 24. 108,720 2.610 5 · 1 3 5 11.329 7.6438 75.9 • 4550 49 - 489 703:7 296.9 74.8 23.0 92,332 9.987 6,4916 65.9 .485 2,301 4.530 49.487 103,7 296.9 23.7 74.7 77.704 1.997 3.931 8.667 5.4631 56.9 . 421 49.489 103.7 296.9 23.1 74.7 63.064. 1.694 7.356 4.4760 297,0 74.8 48.2 .0359 3.33/ 49.212 100.4 21.0 3.5779 50.490 2,73! 15.1 .0295 1.390 6.034 49.214 700.4 297.1 23.7 39.1 37.244 2.6677 . 1221 1.046 2.05% 4.540 75.5 29.5 49,489 703.7 297.3 24.1 2 2499 35.001 .1169 .893 1.755 3.876 75.7 49.489 703.7 297.5 25.0 74.3 1.7858 25, 101 ,719 1.412 3,121 .:152 49,489 100,7 297.7 24.5 76.1 2.1.2 16.147 \*895 1.975 1.1352 76.6 .. 096 .455 297.9 12.5 49.487 103.7 24.0 16.381 900 1,998 1.1517 .0098 .460 49.489 103.7 298.5 77.6 19.7 25.3 26,251 1.8949 .739 1.450 3.209 49.489 100.7 298.6 **25.4** 77.7 20.6 . 3157 32.446 2.2812 77.8 . 185 .879 1:731 3.817 49.489 103.7 298.6 15.4 24.5 39.457 2.8022 77.7 29.9 ·#225 1.061 2:087 4.606 49.489 703.7 298.5 25.4 .0291 1,376 2.70% 5.972 3,6664 52.148 98.5 77.5 38.8 49.489 /03.7 75.3 64,459 3.28 4,5601 . 1353 1.669 7.246 49.489 (03.7 298.3 25.2 77.3 47.3 78.736 1.977 3.896 8.580 5.5357 .416 49.489 103.7 298.2 77.1 56.5 25.4 6.5676 9.928 93,413 49.489 76.8 . 484 2.287 4.502 103.7 <sub>3</sub>98. 24.5 65.6 107.140 5.057 7.5327 .0540 2,567 297.9 76.5 73.8 11,144 49.214 700.0 24.1 8.7103 123.890 2.872 5.655 12:467 49.212 700 . . 297.7 24.6 76.2 8,58 ·061a \*\*\* \*\*\* \*\*\* \*\*\* \*\*\* 49.433 703.1 297.8 24.6 76.3

DEVIATIONS

PAGE:

DATE:

# TABLE 66 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST YUMAER 6

PART of

TEST DESCRIPTION

CLEAN CONDITION - IMPACT/FLOW RATE VERSUS DIFFERENTIAL PRESSURE. AFTER 80 HIGH PRESSURE (10,000 PSIA) GN2. IMPACTS. TEST\_SPECIMEN\_\_\_\_ (S/N 024) INLET PRESSURE = 1000 PSIA NOMINAL.

## TEST SPECIMEN INLET CONDITIONS

J	FLOUNCIER UNF		****	FLOWMETER TWO			F 1 317FF			
	FLOW RATE	PRESSURE	TEMP (DEG: F)	FLOW RATE (ACEM)	PRESSURE, (PSÍA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	FLOW RATE: (ACFM)	II 
	<u>.</u> 84	47.5	6x•7	•91	47.5	73.8	1'07.9	71.2	• 0419	-
	• 75	5.4.4	6º • 7	•81	48.8	73.7	1~07.9	71.2	• 038 <u>4</u> ·	
i	.67	Ð	69:3	.71	49.0	74.0	1:07.9	71.6	• 0337	
•	<u>•</u> 59	5, 6	69.7	.61	49.8	74.3	1,07.9	72.0	. 0298	
	•49	₽9.8	7 . • 6	.51	44.6	74.8	1.07.9	72.7	. 0248	
	<u>•</u> 40	무일.1	71.2	-41	49.6	75.2	1007.9	73.2	•0500	
	١؋ؚ	20.4	71+8	•31	57.0	75.5	1+07.9	73.7	.0155	
	•26	5,•5	72.6	.20	50.0	76.1.	1,007.9	74•3	0131	
•	• 52	4ž.9	73.4	.21	44 <b>.</b> 8	76.4	1407.9	74.9	•0105	
	, 15	÷.∗5	74•3	•14	59.2	76.9	1007.9	75.6	•0072·	_
	<u>•</u> 15	2. ve	75•7	•14	5 <b>∛.</b> 2	77.6	1007.9	76.6	.0072	]
	•ss	#7.5	75 <u>.</u> 5	• 55	49.2	77.7	1507.9	76.6	•0109	-
	.27	47.5	75.3	•2?	49.2	77.7	1107.9	76.5	.0130	-
	•35	47,5	74-8	·31	49.2	77.7	1.07.9	76.3	•0154	
ין	•41	47.1	74+1	• 4 1	49.2	77.5	1407.9	75.8	.0202.	
	<u>.</u> 50	٠٠ <u>.</u> 1	73.2	.51	49.4	77.2	1007.9	75.2	0249	
	<u>.</u> 58	47.7	72.1	•61	48.8	76.6	1407.9	74.4	.0291	
	<u>.</u> 67	47.9	71:-	.71	A8.5	76.0	1007.9	73.7	• 0337	
	• <u>1</u> 6	47.5	73.6	,81	41.9	75.5	1004.0	73.0	.0381	
	<u>.</u> 85	47.9	69:7	•94	47.9	74.7	1104.0	72.2	0429	

PAGE: 2 DATE: 7-26-76

## TABLE 66 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION

CLEAN CONDITION - IMPACT/FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. AFTER 80 HIGH PRESSURE
(1,000 PSIA) GN2 IMPACTS. TEST SPECIMEN
(S/N 024) INLET PRESSURE = 1000 PSIA NOMINAL.

PART 25

TEST AUGGER 6

TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* .. .. /. GROSS DIFF. PRESS GROSS DIFF. PRESS AVG GRUSSS DIFF. PHESS DIFF. PRESS LOW RATE TARE иVG PRESSURE LEMP SECONDARY DIFF. PRESS PHIMARY (PŠL4) (PSIU) (PSID) (PSID) --(PSĮD)-(DEG. F) ( CFM) 86,653 97,334 86.994 **=0.000** 86,994 1007.7 /1.2 . 4419 1007.7 11.2 . 384 77,758 78,485 78.121 -0.000 78,122 66.820 100/.7 11.6 .0337 66.533 67.1 7 -0.000 66.820 1007.9 /2.1 . 1298 57,139 57.942 57.540 -0.000 57,541 1007.7 12.7 · 1248 47,428 46.880 47.154 -0.000 47.154 1007.9 73.2 .0200 37.217 988. E 37.097 -0.000 37.098 28,204 1007.7 (3.7 . 155 28 389 28,019 -0.000 58,202. 1007.7 23.786 23.431 23.605 **∓0.000** 23.609 (4.3 .0131 1007.7 18,928 18,677 18,862 18,803 14.9 .01.5 -0.000 1007.9 75.6 .4372 12,941 12,735 12,835 -0.000 12,835 100 .9 15.6 -0672 12,879 12.8 5 12.86¢ -0.000 ..15:825. 1007.7 19,925 19,879 19.902 197902" 16.6 .0179 -0.000 24,118 24,139 1007.7 (5.5 .0130 24,16 -0.000 24,139 28.978 1001.9 16.0 .0154 28,949 28.943 **40**000 28.944 1007.7 38,254 15.8 .02 2 38,385 38.320 -0.000 38.320 1007.9 48.144 48,405 (5.2 . 1249 48,665 48.405 1007.7 56,888 57.626 57.25? 14.4 . . 291 57,257 -0.000 1007.7 13.7 67,283 67,739 67.511 67.511 . 337 -0.000 13.5 77.212 1004.9 .: 381 76.88B 77.437 -0.000 77.213 . 429 68,737 89,546 89,141 1004,0 15.5 -0.000

| ARE DIFF. PRES= = -1.34000E-04+ -1.24930E-02 (ACFM) + 2.48070E=01 (ACFM) + - -

O (ACFMINA)

TABLE 66
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3...

DATE: 7-26-76

CLEAN CONDITION - IMPACT/FLOW RATE YERSUS ...

DIFFERENTIAL PRESSURE. AFTER 80 HIGH PRESSURE
(10,000 PSIA) GN2 IMPACTS ... TEST SPECIMEN ...
(S/N 024) INLET PRESSURE = 1000 PSIA NOMINAL.

TEST NUMBER 6

TEST DESCRIPTION PART 96

	***	***	***	TEST S	PECIMEN INL	ET CONDITIONS	} }	****	***	***	NET"DIFFERENTI	., , , , , , , , , , , , , , , , , , ,
ij	PHES5		******	LEMPEH, TURE	***	***	*****	FLOW RATE		***		<u></u>
	K@∕≌G CM	bär⊬	DEG. K	DEG. C	DEG. F	LIT#R\$/ MIN	\ <b>c</b> FM	scęм	KĞ\HH GNS	ΓΒΖ΄\HB GNS.	KG/SQ-CM DIF <u>F</u> ERENTIAL	PS <sup>AD</sup>
	70.865	1907.2	295.	21.6	71.2	8.58	. 419	2.866	5•644	12:441	6.1 <u>163</u>	86,994
	70 <u>.</u> 865	1007.7	94.9م	, l •8	71.2	75.9	.0364	630 و	5 <u>.</u> 17 <u>8</u>	11+416	5.4925	78.122
	70.865	140/.7	295.2	22.1	71.6	66.4	.0337	2,306	4 540	10,009	4.6979	66.820
•	70.865	1,07.2	295.4	22.4	72.0	58+4	• #298	2.035	4.005	8∙834	4.0455	57',541
	70.865	100/-2	r95.8	85.0	7,,7	48.1		1,691	3.330	7:341	3,3153_	47.154
	70 <u>.</u> 865	1907-2	296.0	27.9	73.2	38.6	.0200	1.363	2.684	5,918	2.6082	37'- 098-
	70 865	1007.7	296,3	23.2	73,7	29.8	.0155	1.053	2.074	4.571	1.9830	28, 205
	70.865	1007.7	296.7	83.5	74.3	25:0	• 0131	.890	1 • 754	3.862	1.6599	23.609
þ	70.865	1007.7	97.6	;3•8	74.9	~n•0	.0105	.716	1.407	3.107	1.3220	18.503
J.	70.865	1007.2	297.4	24.7	75.6	13.4	. 2072	.487	.95₽	2:113	.2025	12.536
	70,865	1307.7	298.	24•8	76.6	13.4	•0072	.486	<u>.</u> 455	2.109	.9043	12.465: A
	70.865	1007.7	298.0	24. <sup>8</sup>	76.6	~g_6	.0109	.735	1.445	3.190	1.3993	19,902,
	70.865	1007.2	297.9	24.7	76.5	24.8	.013e	.884	1.740	3.836	1.6972	ž4, 139.
•	70.865	1007.7	297.8	. 24.6	76.3	29.5	. ,154	1.047	2,961	4 <u>•</u> 545	2.0349	28-344
	70.865	100/•2	297.5	24.3	75.8	38,7	.020>	1.369	5.695	5,943	2.6942	36,320
·	70.865	1007.7	297.2	24.4	75.2	48.2	.0249	1,691	3 <b>∙</b> 330	7.341	3.4032	48.405
	70.865	1907+7	296.7	53.5	74.4	56.7	•1,291	1.980	3•888	8 594	4.0256	57.257
	70.865	1007.7	>96.3	1.54	73.7	65.9	.0337	2.295	4.517	9.962	4.7465	67,511
	70 586	1904.0	295.9	22,8	73.0	74.6	.038]	2,588	5 <u>.</u> 095	11,234	5,4266	77,213
	70.586 ****	1004+1/ #####	295.5 ****	27•3 ****	2.2	84+2	• 1429	2.915	5 <u>•</u> 732	12 <u>•</u> 652	6.2673	89-142
	70.837	ئ' <u>ڏ</u> 001	296.5	23.4	74.n			•	٠			,···.
	.050	•!	•9	•9	1.6	DEVIATIONS	5	•			~ · · · · · · · · · · · · · · · · · · ·	

PAGE· 1 DATE: 10-7-76

TABLE 67
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

FLOW RATE WERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER THE APPLICATION OF 10 HIGH PRESSURE (10,000 PSIA NOMINAL).

SIDE DOWNSTREAM) OF THE SPECIMEN. DATA ACQUIRED IN THE TEST DESCRIPTION FLOW DIRECTION AT A TEST SPECIMEN INLET PRESSURE = 415 PSIA (NOMINAL).

TEST NUMBER 10

PART 27N

	******	*****		confilions .	******	存在存款标准存款存储	TEST SPECIMEN INLET CONDITIONS				
Ŋ	***	FLOWMETER ONE	*******	***	FLOWMETER TWO				·		
-	ELOW RATE (ACEM)	(½21. <sup>1</sup> ) <u>64£ 2208</u> F	TEMP (NEG+ F)	FLOW R.TE	PRESSURE (PSIA)	TEMP (DEG. F)	PRESSURE . (PSIA)	AVG IEMP (DEG. F)	FLOW RATE :		
	•49	5 <sub>1, • 4</sub>	74.7	.49	49. 5	76.4	416.2	75.6	• 0590		
	•41	`5 <sub>V•4</sub>	7++b	• 4 }	49.7	75.4	416.2	75.6	•0491		
	•30	50.2	75.00	• 3(	49.9	76.5	416+2	75•7	• 0363		
Ä	•26	$\mathfrak{D}(\iota \bullet \underline{1}$	75+2	• 25	49.7	76.7	416.2	75.9	• 0307		
	•21	50.A	75.2	• 2 ग	30.1	76.7	416.2	75•9	.0250		
•	.14	5,.5	7° •6	.13	49.9	76.9	416.2	76,2	.0165		
	<u>•</u> 14	⇒ <sub>(/ • 4</sub>	75.2	.)3	5: •1	77.3	416.2	76.7	.0165		
	•22	50.1	76+1	.21	49.7	77.2	416.2	76.7	.0259		
	<u>•</u> 26	49•1	75.1	• 76	46.6	17.2	415.6	76•6	•0302		
r	•31	56.1	72+3	•31	49.5	77.3	414.9	76.7	•0369		
	•36	45.9	74.9	.36	49.7	77.3	414.9	76.6	• 0425		
	•40	49.9	75•9	• 40	49.2	77.2	414.3	76.5	•0483		
	•45	49.7	75.9	• 45	49	77.2	413.7	76•5	• 0540		
• •	•50	50.1	7=•9	•Su	49,2	17.2	413.7	76.5	.0600		

PAGE· 2 DATE: 10-7-76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER TABLE 67
FLOW RATE VEHSUS DIFFERENTIAL PRESSURE THE APPLICATION OF 10 HIGH PRESSURE (10,000 PSIA NOMINAL) -

TEST NUMBER 10

PART 27N

GN2 IMPACT CYCLES TO THE REVERSE SIDE (HPOF SPECIMEN S/N SIDE DOWNSTREAM) OF THE SPECIMEN. DATA ACQUIRED IN-THE-TEST DESCRIPTIONNARD FLOW DIRECTION AT A TEST SPECIMEN INLET PRESSURE = 415 PSIA (NOMINAL).

					415 PSIA (NOMINA	L).	•
	TEST SPECIMEN_INLET -CON()						
ι	AVG PRESSURE [EIIP (PSIA!()EGF)	AVO FLI)W RATE (ACFM)	GROSS DIFF+ PRESS PRIMARY (PSI:1)	GR.SS DIFF. PRESS SECONDARY (PS10)	AVG GRUSS DIFF. PRESS (PSIO)	TARE DIFF. PRESS (PSID)	NET. DIFF. PRESS (PSID)
	416.4 /5.6 .	.0590	259.417	250.417	250.417	•000	250,416
	416.2 /5.6	491	177.817	177.817	177.817	•000	177.817
	416.4	., 363	114.371	114,371	114,371	•000	114,371
	416.2 /5.9	.0307	92.568	92,591	92.579	•000	92.579
*	416.2 /5.9	.0250	71.224	71.442	71.333	.000	71.333
	416+2 /0+2 .	•n165	43.899.	43.911	43.940	- ~0+000-	43.940
	416.2 76.7	. 165	43.957	43.981	43.969	-0-000	43.968
	416*4 . /6*7	259	74.972	75.230	75.101	.000	75+101
	A15.6 16.6	.03 '2	91.820	91.90	91.890	000.	-91.889
	414.9 /0.7	. 369	118,139	118.1-9	118.159	•000	118.158.
11	414.9 76.6.	. 425	144,989	144.989	144.989	•000	144.989
	.414.3 /6.5	£64¢,.	. 174.029	174+929	174.029		174+029 j
	413.2 (6.5 .	.0540	212,854	212.854	212.854	• 0 0 0	212+654
	413.7	.0610	269,356	269,3,6	269.355	•000	269,356
	A DATE OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PART		+4.4400uE-04 (/	ACE E40.32E.	-01 /ACEUV882 +	0.(ACFM)	
ß	IDRE VALLE.	5 = -3,40000E-00	- + (=++4400BC=0+ ()	(O) M1 + 1,00733E-	TOI THURSTY TE T	o i (noi ii)	To the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of the state of th
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PAGE· 3 DATE: 10-7-76

TABLE 67

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER THE APPLICATION OF 10 HIGH PRESSURE (10,000 PSIA NOMINAL)

ON IMPACT CYCLES TO THE REVERSE SIDE (HPOF SPECIMEN S/N SIDE DOWNSTREAM) OF THE SPECIMEN. DATA ACQUIRED IN THE SIDE OWNSTREAM) OF THE SPECIMEN. DATA ACQUIRED IN THE STORY OF THE SPECIMEN. DATA ACQUIRED IN THE STORY OF THE SPECIMEN. DATA ACQUIRED IN THE STORY OF THE SPECIMEN. DATA ACQUIRED IN THE STORY OF THE SPECIMEN. DATA ACQUIRED IN THE STORY OF THE SPECIMEN. DATA ACQUIRED IN THE STORY OF THE SPECIMEN. DATA ACQUIRED IN THE STORY OF THE SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TE

TEST NUMBER 14

	SSURE	JEN9671 *********************					FLOW RATE			• • •		
KG/SQ ÇM	4 PSIA	DEG. K	DEG. C	DEG. F	LITEKS/ MIN	۸CFM	SCFM	кё\нн еиз	GN2 . LBS/HR	KG/SQ_CM DIFFERENTIAL	PSĪD	
29.265	416.4	297.4	24.4	75.6	45.8	159	1.653	3,254	7.174	17.6060	250.416	
29.265	416.2	297.4	24.2	75.6	39.0	.0491	1.376	2:710	5.974	12.5018	177.817	
29.265	416.4	297.5	24.3	75.7	28.8	• 9353	1.016	5.000	4+408	8.0411	114.371	
29,265	416.4	297.6	24.4	75.9	24.4	.0307	.861	1.595	3.737	6.5089	92.579	
29,265	416.2	297,0	24.4	75 <b>.</b> 9	19.8	.4250	.701	1,380	3.043	5.0152	71.333	
29•265	416.4	297.7	24.0	76.2	13•1	• v 165	.462	•910	2.006	3.0893	43.940	
29 • 265	416.2	298. 3	24.0	76.7	13•0	.0165	•46ŋ	±90!	1,999	3.0913	43.968	
29 • 26 5	410.2	298.1	24.6	76.7	<b>Հ</b> ս•5	• (1259	.723	1.424	3.140	5.2801	75.101	
29.518	415.0	297, 9	24.8	76.6	23.9	\$0EU.	.844	1•664	3,666	6.4605	91.889	
29•174	414.9	298.0	24.8	76.7	29•1	•0369	1.028	2.024	4.462	8.3074	118.158	
29 • 174	414.9	297.9	24.8	76.6	33.6	• 425	1.186	2:334	5•146	10-1937	144-989	
. 59•15å	414.2	297.9	24.7	76.5	38-1	• .463	1.344	2,646	5.834	12.2354	174.029	
29.083	- 413 <u>• (</u>	297.9	24.7	76.5	42,5	• v 54 (	1.500	2.954	6.512	14.9651	212.654	
29.083		297.9 #####	24.1 *****	76.5 «*** <u>*</u>	47.3	.0600	1.669	3.286	7•244	18.9376	269.356	
. 29.213	415.5_	297.B	24.0	76.3						-	· ····	
060	. ـ ا	~ •2	+4	.4	DEVIATI, MS				•			

PAGE · 1 DATE: 10-7-76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF
TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER
THE APPLICATION OF 10 HIGH PRESSURE (10,000 PSIA NOMINAL)
CN2 IMPACT CYCLES TO THE REVERSE SIDE (HPOF SPECIMEN S/N
SIDE DOWNSTREAM) OF THE SPECIMEN. DATA ACQUIRED IN THE
PART 27ml

1EST DESCRIPTIONS PLOW DIRECTION AT A TEST SPECIMEN INLET PRESSURE =
1000 PSIA (NOMINAL).

Tr51 NUP988 10

	***	***	FLOYMETER Runnaceneese	CONDITIONS	***	TEST SPECIMEN INLET CONDITIONS				
1	*****	FLO+MLIEH ONE	·******	<b>松外谷公孙孙孙长存存存</b>	FL 70N21FH Tv()					
	FLOW RATE (ACFM)	(L217)	TEMP (DEG• F)	FLOW RITE	PHESSURE (PSIV)	TEMP (Obg. F)	PRESSURE (PSIA)	TEMP (DEG. F)	FLOW RATE (ACEM)	:
	.85	უ₀.4	64.4	-91	45-4	73.	1"17.2	70.7	.04 <sub>2</sub> 7	
	.76	45.5	97.F	13,	48.2	72.2	1 17.2	69.7	.0377	
	•67	⇒11 • 1	60.2	•73	40.6	71.6	1 17.2	68.9	•0332	
1	•58	p. •1	6=+9	• 10	48 • P	71.3	1 17.2	68•6	•0288	
	•49	5., , 2	Ď-+H	•50	49.2	5-17	1 17.2	68.5	.0243	
	• 40	⇒ <sub>1</sub> , <sub>•</sub> 4	n4.	• 44)	49.9	71.2	1 17.2	68.6	•0196	ţ
	•30	44.9	66 • 4	•3u	49.3	71.5	1917.2	69•0	•0148	
	•26	D 4	66.4	5م.	49.9	71.8	1:17.2	69.3	•0126	
	•21	ಏ∨•೭	57.7	•20	49.9	72.0	1 117.2	69+6	•0102	
Į	.14	47.4	50 • 1	• 1 4	49.5	72.4	1 417.2	70.2	•0068	
	•14	5.00	61.2	•)3	54.3	72.8	1 17.2	71.0	•0069	
	.21	50.1	6-1-2	•24	49.7	73+ 1	1 17.2	71.1	•0102	į
	• 26	56.4	64.4	۶۶.	§0 • ]	72.8	1:17.2	70.9	.0125	
	•31	5 <sub>0 •</sub> 4	h=+7	•31	49.9	72.7	1.17.2	70.7	•0152	
	•41	۶.,د	5∂ • 1	• 4 1	49.5	72.3	1 17.2	70+2	•0200	
ij	•49	50.2	67.2	• 5 ()	49.3	71.8	1-17.2	69.5	•0243	
	.58	5.a.c	ñe∗1	•60	44.1	71.3	1 -17.2	68.7	.0289	
	.67	ጋ •ሩ	¤s•∃	•7ง	40.8	7).7	1 13.2	68.0	,0335	Ý
	.75	p *J	64.4	.31	48.4	59 <sub>•</sub> 11	1 13,2	67.1	.0379	
	.84	49,9	69+9	•91	47.6	;8.7	1013.2	66.3	+0419	

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PÁGE 2 DATE: 10-7-76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF
TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER
THE APPLICATION OF 10 HIGH PRESSURE (10,000 PSIA NOMINAL)

FLOW RATE VERSUS DIFFERENTIAL PRESSURE
TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER
THE APPLICATION OF 10 HIGH PRESSURE (10,000 PSIA NOMINAL)

FLOW RATE VERSUS DIFFERENTIAL PRESSURE (HARACTERISTICS OF
TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 NOMINAL)

FLOW RATE VERSUS DIFFERENTIAL PRESSURE SIDE (HARACTERISTICS OF
TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER
THE APPLICATION OF THE SPECIMEN. DATA ACQUIRED IN THE
PART 27!\*

TEST DESCRIPTIONORWARD FLOW DIRECTION AT A TEST SPECIMEN INLET PRESSURE =
1000 PSIA (NOMINAL).

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TEST SPELIMEN INLET CONDITIONS

PRESSURE (PSIA)	۸۷۵ ۱ <u>۱</u> ۸۲ (UŁĠ• F)	eron hale and	ROSS DIFF. PRESS PRIMARY (PSIJ)	JR SS DIFF. PRESS SECUIDARY (PSID)	AVG GRUSS DIFF. PRESS (PSIL)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)	
1017.2	16.7	427	148,251	(48.25]	148.251	-0.000	148,251	
1017.2	69.7	- 1377	127.734	121.734	127.734	-0.000	127.734	
1017.4	58.9	StE , •	148.795	1.0.795	108.795	-0.000	108.795	
1017-2	50.6	-/ <sub>4</sub> Sap	40.99	»1.434	91.212	-0.000	91.212	
1017.2	<b>υ</b> δ.5	. 1243	73.641	14.,173	73.857	<b>"0 • 0 0 0</b>	73.857	
1017.2	5.6¢	190	57,154	57.559	57.396	-0.000	57.397	
1017.4	<b>⊏</b> 5•6	•4148	41,871	41.676	41.874	-0.000	41.874	
1017.2	09.3	. 126	34.745	34.846	34.796	-0.000	34.796	
1017.2	9 <b>9.</b> 0	*0102	27.323	≥7.375	27.352	-0.000	27.352	
1017.4	10.2	.0000	17.537	17.517	17.52 ?	-0.000	17.527	
1017.4	11.0	.0769	17,826	17.975	17.900	-0.000	17.901	
1017.2	71.1	\$010	27.212	27.375	27.294	~0.000	27.294	3
1017-2	14.9	125	34.745	34.961	34.853	-0.000	34-853	
1017-2	1,.7	• 1122	43.262	43.139	43.200	-0.000	43-201	
1017.2	. 13.2	.050	58_885	59,237	59.062	-0.000	59.062	
1017.2	5. لاد	.11243	74.14	74,329	74.265	-0.000	74,265	
1017.4	១ដ•7	289	42-165	9265	92•.)65	-0.000	92•065	
1013.2	¢8.,,	.,,335	149.425	139.426	109.425	<b>70 - 000</b>	109.426	1
1013+4	e7 • 1	•4379	128.990	126.496	128•396	-0-000	128.997	
1013.4	66.3	419	145.567	148.567	148.567	-0.000	148.567	

PAGE: 3 DATE 10-7-76

TEST SPECIMEN INLET CUMPITIONS

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF
TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER
FLOW RATE VanSos () IFFERENTIAL PRESSURE
THE APPLICATION OF 10 HIGH PRESSURE (10,000 PSIA NOMINAL)
GN2 IMPACT CYCLES TO THE REVERSE SIDE (HPOF SPECIMEN S/N
SIDE DOWNSTREAM) OF THE SPECIMEN. DATA ACQUIRED IN THE
PART 27.4
TEST DESCRIPTIONORWARD FLOW DIRECTION AT A TEST SPECIMEN INLET PRESSURE

NET DIFFERENTIAL PRESS

T55T AUMBER 1: 1000 PSIA (NOMINAL).

	****	おお母女女女女女女女女女女女女女女女女女女女女女女女女女女女女女女女女女女女								****			
1	PRE55		*****	TE SEK TURF	****	*****	***	FLOW RATE	*********	***			
	KG/SQ CM	PSIA	LEG. K	DEG.,	υ <u>ε</u> 6. F	LITEAS/	·cf%	SCFM	γē\H <del>i</del> ρΝΣ	GN2 LB5/HR	KG/SQ CM DIFFERENTIAL	PSĬĎ	
	71.514	1017-2	294.6	21.5	79.7	<b>दे3•</b> 6	. 427	2.953	5.015	12.821	10.4231	148.251	
	71,514	1311.4	294.1	2u • 9	69,7	77.9	. 377	2,609	5 • 13 ¤	11.328	8,9806	127./34	
	71.514	1:17.2	293.7	24.5	<b>೪</b> ಕ.9	66.1	. 332	2.331	4,530	9.988	7.6490	108.795	
ï	71.514	1017.4	293,5	3, رح	68.6	56.b	• 5 <sub>국</sub> 뉴	1.999	3 <u>.</u> 93/	6.679	6,4128	91.212	
	71.514	1017.4	293.4	8.3	o∂.5	47.7	. 243	1.663	3,314	7.306	5.1927	73.857	
	71.514	1,1/.4	293.5	21,0	68,6	34.0	- 190	1.362	∠ <u>•</u> 682	5.914	4.0354	57.397	į
	71,514	1,17.4	293.7	24,5	69.1	29.1	148	1.027	5.455	4.460	2.9440	41.874	
	71.514	1,17,4	293.9	24.1	69.3	24.7	. 126	.874	1,720	3.793	2,4464	34.796	
	71.514	1,11,4	294.0	24.9	69.6	20•0	•0102	.707	1 • 392	3.068	1.9230	27.352	
,	71.514	1.17.4	294.4	S1 • 4	7 }.2	13.4	• 05~	.472	•930	2.151	1.2323	17.527	
	71.514	1017.4	294.6	21.7	11.0	13.5	• • 769	.475	•431	2.066	1.2585	17.901	
	71,514	1.11.4	294.9	21.7	71.1	19.9	• -102	.7u2	1+382	3.448	1.9189	27.294	ı
	71.514	1:17-6	294.8	21.6	76.9	24.5	• 125	.867	1.70!	3.763	2.4504	34+853	
	71.514	1,17+4	294.7	21.5	70.7	24.3	152	1.053	2.174	4.572	3.0373	43.201	
	71.514	1:1(.2	294.4	21+2	7 ?	39.2	• 1547	1.385	2.728	6.013	4,1525	59,062	
3	71.514	101/*4	294.3	20.0	69.5	47.6	• .5+3	1.680	3 <u>•</u> 300	7.293	5.2213	74.265	
	71.514	1.1/.2	293.5	2 ' • 4	65.7	5n.7	•• 599	2.003	3,945	8.697	6.4728	92.065	
	71.235	1/1314	243.2	24.	b8.(	65.7	• 335	2.319	4.561	10+1168	7.6934	109.426	ļ
	71:235	101300	292.7	19.5	67.1	14.5	379	2.629	5 <u>+</u> 178	11-415	9.0694	128.997	
	71•235 ****	1,13°C	297•2	14•, *****	©6.3 ****	H>.4	• ,414	5.919	5 <u>.</u> 720	12.628	10.4453	148.567	,
	71-472	1410.0	293+9	21.7	69.3								
	.071	1,,	٠,٥	• 5	1.0	υΕVΙΑΤΙζισ	<b>ಶ</b>						

PAGE: 1 DATE: 10-7-76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF · TABLE-69 TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER FLOW RATE VERSUS DIFFERENTIAL PRESSURE THE APPLICATION OF 10 HIGH PRESSURE (10,000 PSIA NOMINAL)

GN2 IMPACT CYCLES TO THE REVERSE SIDE (HPOF SPECIMEN S/N TEST DESCRIPTIONSIDE DOWNSTREAM) OF THE SPECIMEN. DATA ACQUIRED IN THE TEST NUMBER 10 PART 27LK.

REVERSE FLOW DIRECTION AT A TEST SPECIMEN, INLET PRESSURE 415 PSTA (NOMINAL) FLOWMETER CONDITIONS TEST SPECIMEN INLET CONDITIONS \_ \_ FLOWNLIER\_ONE.. . FLUWMETER TWO \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\* AVG-PRE 55URE. (P.214) FLOW RATE TEMP FLOW HATE PRESSURE TEMP PRESSURE TEMP LDEG. E) FLOW RATE (ACFM) (DEG+ F) ... (DÉG...E) . . (PSIA) .. \_\_\_49.\_\_. --. 51.4. 79.5 .50 49.3. -- ...... .40 50.2 79.7 . 40 49.3 80.4 .31 20.4 80.0 .31 49.9 414.3 .....80.6..... ---- +26 56.4 .... 49.9. 4:. 2 .25 .21 56.8 413.7.... 84.4 .20 50.3 +0252-.13 50.6 B(1+7 .13 \_413\_7\_\_ 50-1 30.8 81 • 1 .13 . .50.43. 413.7 .22 44.9 49.3 81 • 1 .21 .26 50.2 81.0 49.7 \_ 413.7\_\_. 81.6.... • 25 .31 50.2 81.1 .31 • 40 20.1 81.2 • 40 44.2 .46 49.9 81.4 .46 49.0 

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TABLE 69 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER THE APPLICATION OF 10 HIGH PRESSURE (10,000 PSIA NOMINAL)

GN2 IMPACT CYCLES TO THE REVERSE SIDE (HPOF SPECIMEN S/N REVERSE FLOW DIRECTION AT A TEST SPECIMEN INLET PRESSURE =

TEST NUMBER 10 PART 27LR

415 PSIA (NOMINAL).

TEST	SPECTMEN	INLET	CONDITIONS
******	*******		REBRESSER

PRESSURE (PSIA)	AVG TEMP (DEG. F)	AVG FLOW RATE (ACFM)	.cROSS DIFF. PPESS PRIMAPY (PSID)	-GROSS DIFF• PRESS SEGONDARY (PSIO)	AVG GROSS DIFF. PRESS . (PSIU)	TAREDIFFPRESS (PSID)	NET
414.3	8 <sub>0+</sub> 2	• n597	297.133	297.133	297.133	• 000	297-133
414.3	80•4	•9478	188.234	186.234	188.234	•000	188.233
414.3	80.6	• 1372	127.628	127.628	127.628	•000	127.628
413.7	<b>∀0.8</b>	.0311	100,167	163.167	100.167	.000	100.166
413.7	81.0	. 1525	76,221	75.)77	76.199	•000	76.199
413.7	81.2	•0160	44,768	44.612	44.690	-0.000	44.690
413./	ರ1.6	.0159	44.710	44.612	44,661	-0.000	44,661
413.7	81.7	. 4257	78,344	78.387	78.365	•000	78.365
413.7	81 <b>.</b> 6	.0304	99.220	99.220	99.220	.000	99.219
413.7	81.7	.0373	129,522	129.522	129.522	•000	129.522
413.7	81.8	.9480	189,496	189,496	189,496	•000	189,496
413.7	81.9	.0547	241,894	241.894	241.894	•000	241.894

IADE DIFF. PRESS = -3.40000E-05 + -4.4400GE-04 (ACFM) + 1.50933E-01 (ACFM) #\*2 + 0 (ACFM) ##3

PAGE: 3 DATE: 10-7-76

TABLE 69 FLOW PATE VENSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER THE APPLICATION OF 10 HIGH PRESSURE (10,000 FSIA NOMINAL)

GN2 IMPACT CYCLES TO THE REVERSE SIDE (RPOF SPECIMEN S/N

TEST DESCRIPTIONSIDE DOWNSTREAM) OF THE SPECIMEN. DATA ACQUIRED IN THE

TEST NUMBER 10 PART 271 k

		•	. T	EST NUMBER 10	PART	27LK	T <u>FST</u> _	R	EVERSE FLOW D	IRECTION AT A	CIMEN. DATA ACQUIR TEST SPECIMEN INI	
	*****	****	***	TEST SP	ECIMEN IN	_FT_CUNDITIONS	*****************		15 PSTA (NOMI		NET DIFFERENT	
1.	PRESSU		* * * * * * * * * * * * * * * * * * * *	TEMPERATURE	****			ELOW HATE	***	***		
	KG/SQ CM	P\$1a	DEG. K	DEG. C	DEG. F	LITERS/ MIN	-AGFM	SCEM	K∂∖HҢ ₽NS	GNZ LBSZHR	KG/SQ CM DIFFERENTIAL	psin
	. 2 <sup>9</sup> .12 <sup>8</sup> .	. 414.J	299.9	26.8	b0.₽.	A67			3.248	7. <sub>161</sub>	20.8905	297+133
	29,125	414,5	300.0	26,7	មិល «។	37.4.	.J47E	1,322	2.604	5,740	13,2341	188,233
	29.125	414.3	300.T	27.0	84.6	29-1	.0372	1.02B	-2-025	4.463	8.9731.	127.628.
Ţ	29.083	413.7	300.3	27.1	8,,8	24.3	4311	858	1 • 68 5	3.724	7-0424	100.166
	29.083	413./	300.4	27.2	81.A	19-7	-0252	696	13.70	3-019	5+3573	76-199
	29.083	413.!	300.5	27.4	01.2	12.5	.016n	440	<u></u>	1.911	3.1420	44.690_
	29.083	413.1	300.7	27.6	Bl.5.	12-A	4159	439	.864	1.904	3.1400	44.661
	29,083	4 <u>1</u> 3.7	300.8	27.0	81.7	20.0 .	.0257	7a7	1.392	3=068	5.5095	78.365
	29,083	413-!	300.7	27.6	81.6	24.0	<u>-030</u> 8	848	_1.667	3.680	6.9758	99.219
L.	29.083	413,[	300.8	27.0	81.7	29-1	•u373	1.028	. <u>2•u24</u>	4.462	9-1063	129.522
	29.083	413./	360.6	27.6	២].8	37.4	•#48n	.1.322 .	. 2 <u>.</u> 604	5.74.0	13.3229	189.496
	29.083 ****	413./ ****	300.9 ****	27.7	81.9 *****	42.6	. 3547	1_505_,	2,764	6.534	17-0068	2 <u>41.894</u> '
	29,094	413.8	300.5	27.3	91.2	v						
	•017	• ជ	•3	•3	•5	. DEVIATIONS		, , , , , , , , , , , , , , , , , , ,				
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										* a w 10 100 100 100 100 100 100 100 100 10		
						-	•	, m. n	*	***************************************		<del></del>
										•		

PAGE: 1 DATE: 10-7-76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER THE APPLICATION OF 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES TO THE REVERSE SIDE (HPOF SPECIMEN S/N SIDE DOWNSTREAM) OF THE SPECIMEN. DATA ACQUIRED IN THE JEST DESCRIPTIONREVERSE FLOW DIRECTION AT A TEST SPECIMEN INLET PRESSURE =

TANK HIMAGO T PART 27KR

1000 PSIA (NOMINAL).

FLOWMETER COM ITTOMS TEST SPECIMEN INLET CONDITIONS

	**	************		19844849944444444 (	****	*****		44444444444 CIMEN INCÉ: C	****	
ŀ	****	FLOWN, 1ER ONF	***	******	FilosMFTEX TX()	)				
	FLOW RATE	PRESSURE (FSIA)	年(197 (9月5年 年)	FLOA KLÎF (\CFM)	PRESSURF (PSI.)	TFNP (byg. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	AVG FLOW RATE (ACFM)	ı
	.78	Du . 4	70.45	.al	44.5	÷ •7	1 09.2	78,6	.0388	
	• 69	300€1	75.0	• <b>7</b> a	"A.7	2 ⋅• 2	1 09.2	78.0	.0341	
	•60	D: • 4	75.6	·fit	49.1	79.9	1 09.2	77.8	•0296	
ŧ	•51	20.5	7 - • 5	-51	49.5	74.4	1 09.2	77.7	.0250	
	•41	⊃t.1	7=+0	.44	44.3	29.8	1 05.3	77.9	•0200	
	•31	51.4	7++4	•34	50 • 1	10.1	1 05.3	78.3	•0153	ā
	•27	58	74.4	.25	ÇA	, •5	1.05.3	78.4	.0131	
	.21	p/ *5	7 2 . 9	•24 -	~u•1	n),3	1.05.3	78.6	.0104	
	•14	30.4	7714	-13	5ೇ+2	4r.6	1 05.3	79•0	•0070	
ľ	•14	54	75.0	٠1 ځ	11+2	•∺	1.05.3	79•4	•0070	
	•22	೨೯.೪	7~.4	-21	80.42	50 · B	1 05+3	79•3	•0107	
	<u>.</u> 26	<b>5 ۰,</b> 4	77•/	<b>،</b> 25	-0.1	~ 1.7	1 05.3	79.2	.0128	ĵ
	•32	45.9	77+3	•31	49,5	8 ° 6	1 (05.3	79 • 0	•0154	
	.41	3.7.4	7 🕶	<b>-4</b> 1	49.4	4	1 05.3	78.6	•0204	
	•51	5.4	78.1	+ <sup>2</sup> ~ <b>1</b> .	49.5	10.1	1 05.3	78.1	•0251	
ŀ	.59	D <sub>U + 4</sub>	75.47	•6)	47.5	79+4	1 05.3	77.3	•0295	
	.68	D1 . 4	7 - 1	.77	4H.9	16.6	1 01.3	76.4	.0342	
	.75	D1 . 4	7) <sub>4</sub> ች	1	40.5	· S • 1	1.01.3	75.7	•0384	ſş
	.84	5.4	7:+5	.91	ш <b>д</b> "Я	77.3	1001.3	74.9	•0432	

PAGE: 2 DATE: 10-7-76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER FLOW RATE VERSUS DIFFERENTIAL PRESSURE (10,000 PSIA NOMINAL)

CN2 IMPACT CYCLES TO THE REVERSE SIDE (HPOF SPECIMEN S/N SIDE DOWNSTREAM) OF THE SPECIMEN. DATA ACQUIRED IN THE PROPERTY OF THE PRESSURE FLOW DIRECTION AT A TEST SPECIMEN INLET PRESSURE =

T ST 904 En 10

1000 PSIA (NOMINAL).

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(bžia) - bšessuke	и/G јенр (реф. г)	FLDP HATE VS	ગરે ફેડ biff: ટેલ્ટ્લર Pai't, ay (છ51,,)	AR SS DIFF. PRESS SECOMPLAY (PSID)	AVG GROSS DIFF. PRESS (PSIU)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)	1
1009•	10.6	. 288	138.075	130.476	138.670	-0.000	138.677	
1009•़<	16.0	. 341	117,525	117. 28	117.528	-0.000	117.528	
1009.4	17.8	230	98.27J	96.173	98.273	-0.000	98.273	
1009•4	17.7	. 125.	19.469	79.500	79.717	-0.000	79.717	
1005.3	77.9	+ (1,2° +1)	o# = 240	8126	60.680	-0-000	60.686	
1005.3	. /0+3	. 1 > 3	44.300	44.676	44•33 <sup>5</sup>	~0.00	44.340	4
1005.3	1844	. 131	3762 .	37.1 B	37.125	-0.000	37.125	
1005,3	/6.6	.91.4	28,564	23,599	28,584	-0.000	28.582	
1005.3	19.0	•90 (a	18.251	15.250	18.265	-0.000	18.266	
1005.3	19.4	.007	13.201	15.952	19.321	<b>-0</b> • 0 0 0	18.352	
1005.3	19.3	.)1.7	29.370	29.5 8	29.447	-0.000	29.447	
1005.3	19.8	•:159	35.444	36.650	36.54]	-0.000	36.547	ij
1005-3	19.4	.3154	44.1.3	44.720	44.915	-0.000	44.916	
1005.3	10.0	•02 4	42. 197	62.n 4	62.351	-0.000	62.351	
1005.3	/B.1	. 251	8216	5912	80.565	-0.000	80.565	
1005.3	17.3	. 295	98.273	98,273	98.273	-0.000	98.273	
1001.3	16.4	.: 342	119.1,0	119+1 .6	119.1ne	-0.000	119.106	
1001+3	12.7	• n344	140.253	143.2-5	140.255	-0.000	140.255	ŋ
1001.3	1++9	• 1.437	104.244	104.244	164.244	-6-000	164.244	

PAGE: 3 DATE: 10-7-76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF TEST SPECIMEN S/N 027 AT THE COMPLETION OF TEST 10 AND AFTER THE APPLICATION OF 10 HIGH PRESSURE (10,000 PSIA NOMINAL) GN<sub>2</sub> IMPACT CYCLES TO THE REVERSE SIDE (HPOF SPECIMEN S/N SIDE DOWNSTREAM) OF THE SPECIMEN. DATA ACQUIRED IN THE SIDE TO THE SPECIMEN INLET PRESSURE = 1000 PSIA (NOMINAL).

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	*****	CNLTT18700 T4_AAI hahaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaa								NET DIFFERENT			
ß	PRESS		•		****	***							
	KG/SQ CM	Pola	offer k	1₹ <b>5</b> ± 1*	neu. F	\25. T1J W] @	cF	SCFM	KG/HK	CAS/HR	KG/SQ CM DIFFERENTIAL	PSĮD	•
	70.956	1.07.6	-49	المراجع المح	70,0	14.7	. 34,	2.624	5.159	11-374	9.7499	138,677	
	70.956	1 107.6	294.7	25	75. (	64.3	. 34.	2.3,7	4.546	10.014	8.2630	117.528	
	70.956	1107.4	298.0	نيدن عاني	77,5	z+ +7	. 244	2.0.22	3.443	8.692	6.9093	98.273	
;	70.956	1 107 • 6	296.5	*51.44	77,7	47.9	• 25 ·	1.691	3.327	7.341	5.6047	79.717	
	70.677	1,05.3	296.7	75.0	77.9	30.03	+ P 10	1.359	2.059	5.462	4.2667	60.686	
	70.677	1,05.5	294.5	25.1	74.3	29.1	• 15"	1.628	2- 24	4.463	3.1174	44.340	1
	70,677	1905.3	296.9	d. ۵	74,4,	24.9	. 131	•931	1./34	3,423	2,6101	37,125	
	70,677	1,05,3	\$66*	8-, 3	74,0	19,5	• 1 4	.7:1	1.381	3,044	2.0095	28.582	
	70.677	1,05,3	299.3	84.1	79.	13.2	• 07	.468	•ASİ	2.4.30	1.2842	18.266	
ř	70.677	1405.3	299.5	ರಿಕ್ಕಾತೆ	79,4	13.2	- 1 17 -	.467	• <b>≯</b> 2u	2.328	1.2902	18.352	
	70,677	1,05.5	290.5	25.3	79.3	٤٠.٤	+61 17	.715	1-413	3.107	2.0703	29.447	
	70,677	1,05.3	2 <del>99</del> .4	c++ • c'	79.2	24·4	. 123	.861	1.690	3.740	2.5695	36.547	li
	70,677	1000.3	239.2	<r +="" 1<="" td=""><td>79.</td><td>24∙3</td><td>• 144</td><td>1.035</td><td>2. 30</td><td>4.492</td><td>3.1579</td><td>44.916</td><td></td></r>	79.	24∙3	• 144	1.035	2. 30	4.492	3.1579	44.916	
	70.677	1005.0	299.	24.9	70.5	39.4	- 12 4	1.376	2.707	5.973	4.3837	62.351	
	70.677	1,05.3	29H.5	24.6	78.1	47.9	• 25.	1.693	3,333	7.349	5.6643	80.565	
;	70,677	1(05.3	298.3	24.4	77.3	51,.4	. 29.	1.991	3.315	8.540	6.9093	98•273	
	70,398	1 01-3	297.9	4.7	74.4	65.2	. 34/	2.3.1	4.531	9.990	8.3740	119.106	
	70.398	1,81.0	297.4	c4.5	75.7	73+3	٠, ٠٤	2.549	598	11.239	9.8609	140.255	3
	70.398 ****	1.01.2	297.0 ****	6.85 *****	74.9 ######	4, ,5	• 43r	2.914	5,738	(2.65)	11.5475	164.244	
	70.691	1305.5	98.7 و	<u> </u>	78.0							•	
	•111	1.0	•5	ď•	•è	OEVIATION.	•						

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PAGE: 1 DATE: 10-7-76

TABLE 71

TABLE 71

FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA IN THE FORWARD DIRECTION (S/N SIDE UPSTREAM). ACQUIRED ON TEST SPECIMEN S/N 028 AFTER COMPLETION OF NORMAL TEST 12 SEQUENCE TEST SPECIMEN INLET PRESSURE = 415 PSIA.

TFST 40 MbR 12

75.0

>1, • 1

PIRT 2HU

TEST DESCRIPTION

****	CINDITIONS . The abstract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substract and a substrac				******	TEST ŠPECIMEN INLET CONDITIONS				
****	FLOWM, JER ON;	\$ 4 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	****	FLUMMETER TWO	) *****					
FLOW RATE	PK_25UKE (P514)	Temp (SEG. F)	FLOW RATE	PRESSURE (PSIA)	TEMP (DE3. F)	PRESSURE (PSI <sub>A</sub> )	AVG Temp (deg. f)	AVG FLOW RATE (ACFM)		
•40	⊅ <sub>U•</sub> 4	. 74.4	•40	49.9	77.4	414.3	75.7	. <sub>0</sub> 485		
,36	90.6	7541	.35	49.9	76.5	414.3	75.8	•0431		
.30	5,.6	74-1	•30	<pre><pre><pre><pre></pre></pre></pre></pre>	76.5	413.7	75.8	.0368		
.26	54.5	72	.25	19.9	76.7	413.7	75.9	.030 <sup>8</sup>		
.21	50.4	75.5	.20	49.4	70.7	413.7	76.1	.0248		
.14	¤6•1	75.7	•)3	49.9	76.9	413.7	76.3	•0168	,	
<u>•</u> 14	90.1	79.9	•13	49.7	77.1	413.7	76.5	•0167		
• 21	50.1	75.5	.21	49.7	17.0	413.0	76.5	.0254		
.26	44.9	75-9	.75	49.3	77.1	413.0	76.5	.0305		
.31	49.5	7 6	•31	49.3	77.1	413.0	76.4	•0368		
•36	44.9	75.8	• 36	49.2	77 • L	412.4	76.4	•0428		

49.3

17.2

411.7

76.5

. 44

+0485

PAGE · 2 DATE · 10-7-76

# TABLE 71 FLOW RATE VE-SUS DIFFERENTIAL PRESSURE

FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA IN THE FORWARD DIRECTION (S/N SIDE UPSTREAM). ACQUIRED ON TEST SPECIMEN S/N 028 AFTER COMPLETION OF NORMAL TEST 12 SEQUENCE TEST SPECIMEN INLET PRESSURE = 415 PSIA.

THIST HUMBER 12

LAS TRUE

FFST DESCRIPTION

# TEST SPECIMEN INLET CONSITIONS

PRESSURE (PSI <sub>A</sub> )	AVA (EMP (DEG. F)	FLOY PATE (ACFR)	RHUSS DIFF• PRESS PPIMINGY (PSID)	GR \$5 DIFF. PRESS SECURDARY (PSID)	AVG GRUSS DIFF• FRESS (PSID)	TARE DIFF• PRESS (PSID)	NET DIFF• PRESS (PSID)	į
414.3	15.7	4.,455	274.823	74. 273	274-223	*000	274.222	
414.3	75.8	+, 431	185.73.	192.13	185./3.	•000	185.729	
413.1	15.5	•#3¢ 4	130.730	1334	130.739	•000	130.737	
413.7	15.9	-t3 H	41.249	ୱଳ୍କ ବ୍ୟବ	96.289	•000	96.288	
413.7	10+1	• 1648	67.3/	67.465	<sub>0</sub> 7.576	•000	67•576	
413+7	16.3	$*e1^{fin}$	3 <sup>9</sup> • 1 4 <sup>9</sup>	39.404	39.287	•000	39.287	,
413.7	76.5	. 157	34.910	39.145	39.1150	.000	39.055	
413.0	16,5	<u>. 6</u> 254	70.561	71,005	70.783	.006	70.783	
413.0	70.5	្នក្សា កើ	95, 125	45.435	95.025	.000	95,024	
413.0	10.4	•: 30fi	132.450	132.50	132.9511	•000	132.950	
412.4	16.4	. 42,	132.809	142.544	182.085	, •000	182.885	
411./	15.5	.p405	279.595	279.545	279.595	•000	279.595	Á

1AQE DIFF. 0 F9S = -3.46000E-05 + -4.440006-94 (ACFM) + 1.56933E-01 (ACFM) 442 +

e (ACFM) \*\*3

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PAGE: 3 DATE: 10-7-76

TABLE 71

### FLOW PLIF VERSUS DIFFERENTI L PRESSURE

FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA IN THE FORWARD DIRECTION (S/N SIDE UPSTREAM). ACQUIRED ON TEST SPECIMEN S/N 028 AFTER COMPLETION OF NORMAL TEST 12 SEQUENCE TEST SPECIMEN INLET PRESSURE = 415 PSIA.

TEST OUTBER 18 PART 250

25[1

TEST DESCRIPTION

												IAL PRESS	
ß	PRESS		***	16 15 LA LAUE	***	****	<b>} \$</b> \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	FLOW RATE	****	***			
	KG/SQ CM	PSIA	<b>⊬⊑6•</b> ⊀	υ <b>ξ</b> α• ε	D€G• F	LITS/ MIN	۰c۴۰۰	SCFM	K@\HK ₽'n5	GNS FR	KG/SA CM DIFFERENTI <sub>A</sub> L	PSĮĎ	1
	2 <sup>9</sup> •12 <sup>8</sup>	414.3	297.4	:4.3	75.7	3 <sup>A</sup> •3	• 1 4 3 17	1.353	2.664	5,873	19.2798	274.222	
	29,128	414.5	297.5	×4.3	75.8	34.1	. 43]	1.24.3	2,368	5.221	13.0581	185.729	
	29.083	413,1	297.5	24.3	75,8	29.0	• 036H	1.024	2.,16	4.446	9.1918	130+737	
:	29.083	413.	297.6	24.4	75,9	24.3	•030"	.858	1.690	3.726	6.7697	96°588	
	29.083	413.1	297.7	24.5	76.1	19.6	• 124-4	•091	1,360	2.999	4.7510	67.576	
	29.083	413,1	297.8	24.6	76,3	13.2	•v1 <sup>68</sup>	,467	•91 <sup>9</sup>	2.026	2.7621	39,287	1 _
	29.083	413.1	297.9	,4.7	76.5	13.1	• 167	.463	•912	2.010	2.7459	39.055	
	29.037	413.0	297.9	24.7	76,5	მე•0	.0254	.796	1,391	3.066	4.9765	70.783	
	2 <sup>9</sup> •03 <sup>7</sup>	413.0	297.9	24.1	76,5	24+3	•4317	.847	1:667	3,675	6,6809	95.024	
ş	29.037	413.6	297.7	24.7	76.4	24.9	. <sub>0</sub> 35∃	1.022	2•v11	4.434	9.3473	132.950	
•	28.992	412.4	297.9	7•4ج	76,4	33.6	9 ج 4 . •	1.186	2.335	5.148	12.8581	185.895	
	28.946 *****	411.7	297.9	24.7	76.5	38.9	,5485	1 • 341	2,940	5,820	19.6575	279,595	ĺ
	29 • <u>06</u> 0	413 <u>. 3</u>	297.7	4.6	76,2								
	042	;0	•\$	. •5	,3	OFALTIVE	3						

PAGE: 1 DATE: 10-7-76

TABLE 72

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA IN THE FORWARD DIRECTION (S/N SIDE UPSTREAM). DATA ACQUIRED ON TEST SPECIME. S/N 028 AFTER COMPLETION OF NORMAL TEST 12 SEQUENCE TEST SPECIMEN INLET PRESSURE = 1000 PSIA.

TIST HURAEK 12 PHRT THT

TEST DESCRIPTION

	*****	****	FLOWNETEF PROGRESSERVERS SER	COMDITIONS	****	外数分数八指引擎数数价	TEST SPE	CIMEN INCET C	ONDITIONS	
i,	****	FLOWMELER ONE		*****	FLOMMETER TOO					
	ELOW RATE	PKLSSURL (PSIA)	Timp (ngg, F)	FLOW R. TE (SCFM)	PAESSURE (PSIA)	Temp (*)n3. F)	PRESSURE (FSIA)	TEMP (DEG. F)	FLOWANGTE (ACFM)	đ
	.87	ნე	64.8	۱۴.	48.	72.7	1:05.3	70.5	• <sub>0</sub> 435	
	.78	5e.1	67.4	with.	48.4	72.	1 05.3	69.7	.0391	
	.69	>u_5	57.1	•71	49.0	71.5	1 +05.3	69.3	.0346	
ļ	•60	50.1	65.1	• 50	48,8	71."	1.05.3	68.8	.0296	
,	• <b>5</b> 1	50.5	6n.4	• 20	49.5	72.2	1905.3	69,5	.0251	
	.41	50.1	6n.ad	∪ م	9.3	72.3	1 05.3	69.6	.02 <u>0</u> 2	J
	•32	44.9	57.3	•31	49.3	71.4	1,05.3	69.3	.0154	
	.26	50 <b>.</b> 1	67.8	.25	49.7	/1.9	1,05,3	69.8	.01 <del>2</del> 8	
	,21	ي. نڅ	61.4	.20	49.9	72.4	1005,3	70.4	.0104	
βl	- • 14	49,7	6°,3	.13	49.5	72.A	1605.3	71.1	.0069	
Įt.	,14	49.9	71.8	.13	49.7	73.8	1005,3	72,3	.0069	
	, žž	ອັບູເລ	78 .	.21	49.9	73,8	1,05,3	72.3	, ô10 <sup>8</sup>	1
	26	20.5	79	. 25	50.1	74.0	1605,3	72.4	•0129	

PAGE: 2 DATE: 10-7-76

THOW PATE VERSUS DIFFERENTIAL PRESSURE

TABLE 72

FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA IN THE FORWARD DIRECTION (S/N SIDE UPSTREAM). DATA ACQUIRED ON TEST SPECIMEN S/N 028 AFTER COMPLETION OF NORMAL TEST 12 SEQUENCE TEST SPECIMEN INLET PRESSURE. = 1000 PSIA.

TEST AUMHER 15 PART 28T

TEST DESCRIPTION

ſ

PRESSURE (PSIA)	lemp (Uto• F)	FLOW RATE	jRijSS DIFF• PKESS PRI:1:"Y (PSI <sub>U</sub> )	UIFF. PRESS SECONDARY (PSID)	AVG GRUSS DIFF• PRESS (PSID)	TARE UIFF• PRESS (PSIO)	NET DIFF• PRESS (PŞID)	-1
1002°3	14.5	, 435	225 <u>,</u> 973	×25,973	225,473	-0,000	225, <sup>9</sup> 73	ļ
1005,3	59_7	.13 <sup>9</sup> 1	เหริว35	[d5] 155	185 835	-0.000	185.835	
1005,3	4. J	* 134A	151.07:	151,174	151.070	-0.000	151.070	
1005 • 3	។ ဗ.្ឌន	2%	117.485	117, 385	117,885	-0.000	117.885	
1005.3	<b>৬</b> ৬ৢ५	<u>, </u> 251	46.415	41.705	90. <sup>8</sup> 10	-0.000	90.810	
1005.3	29.6	.0202	64.753	64.7159	64.786	-0.000	64.787	,
1005,2	69_3	.0154	44.264	43, 730	44.097	-0.000	44.097	'
1005.3	₽ <b>9</b> *8	.r12H	33.995	34.,34	34.04v	-0.000	34.040	
1005.3	/ <sub>U.2</sub> 4	• o 1 × 4	25,5%4	25.824	გ5 <b>•</b> ი <sup>ი</sup> ნ	-0-000	25.606	
1005.3	(1.1	•0000	14.909	14.745	14.96.	-0.000	14.907	
1005.3	/d <sub>=</sub> 3	.0064	14.909	15, 19	14,964	-0.000	14.964	
1005.3	12,3	•elod	25.918	27. "7	26.962	-0.000	26,963	ıı
1005•3	12.4	+(129	34.411	34.545	34.473	-0.000	34.473	v
					_			

LARE DIFF. PAFSS = -1.64000E-04 + -1.2593.E-02 (ACF.) + 2.48070E-01 (ACF.)\*42 +

0 (ACFM) ##3

4.

PAGE: 3 DATE: 10-7-76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TABLE 72

FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATA IN THE FORWARD DIRECTION (S/N SIDE UPSTREAM). DATA ACQUIRED ON TEST SPECIMEN S/N 028 AFTER COMPLETION OF NORMAL TEST...12 SEQUENCE TEST SPECIMEN INLET PRESSURE = 1000 PSIA.

TEST SPECIMEN INLET PRESSURE = 1000 PS:

TEST JU; BER 12

PART 28T

TEST DESCRIPTION

TEST SPECIMEN INLET CUNDITIONS										***	NET DIFFERENT	
Ą	PŘEŠŠ	ÚRE ******		TF 1PERATURE	***	***	****	FLOW RATE	****	***		ŕ
	Kē\ād CM	PSIA	T ĎĚĠ. K	J€6. €	DEG. F	Ľ1ŢÇ₹S/ NIN	.cFM	ScFM	KĞ\HK GNS	Γ <sup>B</sup> S\HB GNS	KG/SQ CM DIFFERENTIAL	
	70 • 677	1005.3	294.5	21.4	79.5	84.1	. 435	2.971	5.849	12, <sup>895</sup>	15.8875	225,973
	70 <u>+</u> 677	1,05,3	294.1	و. <sub>د</sub> رد 2	69.7	75.8	• 3 <sup>9</sup> 1	2.676	5 • 269	11,615	13.0655	185.835
	70.677	1005.3	293.9	20.7	69.3	67 • U	. 1346	2,367	4.661	10.276	10.6213	151.070
ħ	70.677	100B.d*	. ž93 <b>.</b> 6	20.5	68.8	57.5	. 1296	2.331	3,998	8,815	8,2882	117.885
-	70.677	1005.3	294.0	20.8	69.5	48,6	.4251	1.716	3,380	7,451	6.3846	, à0•5 <b>Ĭ</b> Q
	70.677	1005.3	294.0	20.9	69,6	39•1	.0202	1.379	2.716	5,987	4,5549	64.787
•	70,677	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	293,9	20.1	69,3	29.8	.0154	1.053	2.673	4,571	3,1003	44.097
	70,677	ئ <sub>•</sub> ,5000	294.2	21.6	69.8	24.7	.0128	.874 ´	1.721	3,794	2,3932	34 <b>,</b> 040
	70,677	1005,3	294,5	51.3	70.4	20.2	.0104	,712	1.401	3,090	1.8003	. 52 <u>.60</u> 6
ĺ	~ 70 <u>.677</u> ~	1005.3	294,9	21,7	71.1	13,3	.0069	.468	• <sub>2</sub> 5ř	2.032	1.0481	14,207
	70,677	1005,3	295,0	22,4	72.3	13,3	.0069	.469	•923	2,035	1,0521	14,754
-	<u> </u>	1005,3	295,6	27,4	72.3	20.9	.010 <sup>8</sup>	.738	1 453	~ 3,2 <sub>0</sub> 4	1-8957	<u> </u>
	70.677	1005.3	295,6	22.5	72.4	24.B	12 <sup>9</sup>	.876	1.725	3 <u>.</u> 8 <sub>0</sub> 4	2.4237	34.473
	70,677	# <del>##٩٩</del> د 1005	294.5	##### 21 <u>.3</u>	特殊特殊禁止。 7 n A							
 {!	0	• • • • •		•6	70.4. 1.v	DEVIATIONS					****** 1.4 *****************************	halikkin demonstrative and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and service and ser
•			· , ,	•	-							

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PAGE: 1 DATE: 10-7-76

TABLE 73

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF TEST SPECIMEN S/N 025 AFTER 100 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES AND CONTAMINATED WITH 46 MG OF Fe203. FLOW DATA ACQUIRED AT AN INLET PRESSURE OF 1,000 PSIA NOMINAL AND IN THE FORWARD (S/N SIDE UPSTREAM) DIRECTION

TEST MUGRER B

PART 25Z

TEST DESCRIPTION

	****	****	FLOUMETER PREESTANDERS	TEST SPECIMEN INLET CONDITIONS					
ď		FLOWME LER UME		*****	FLOWMETER THO				·
	FLOW RATE	PRESSUPE	. Т <u>е</u> мр (ОЕG• F)	FLOW RITE (ACFM)	PAESSURE	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	FLOW RATE
	•27	50.6	79.7	. >6	50.2	′າ <b>1 •</b> 5	1709.2	80.6	•0132
	• 22	₽¢•6	79.7	•51	50.2	31.6	1:09.2	80 • 6	•0106
	•16 °	56,8	70.0	•15	50.4	B1.7	1009.2	80.8	•0079
j,	•11	47.5	∂ 1 = 3	-10	49.3	<b>ा.</b> 8	1,09.2	81.0	•0052
	•11	44.5	BC+6	.10	49.3	32.1	1009.2	81.4	.0052
	.17	44.7	8 .5	.16	49.5	85*5	1009.2	81.3	•0079 <sup>-1</sup>
	.21	49,7	8 .3	•50	49.5	1.50	1009.2	81.2	•0101
	.25	49.5	79.9	.24	49.3	<sup>14</sup> S∗0	1009.2	80.9	•01ŹŌ "

PAGE · 2 DATE · 10-7-76

FLOW RATE VERSOS DIFFERENTIAL PRESSURE

TABLE 73

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF TEST SPECIMEN S/N 025 AFTER 100 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES AND CONTAMINATED WITH 46 MG OF Fe203. FLOW DATA ACQUIRED AT AN INLET PRESSURE OF 1,000 PSIA NOMINAL AND IN THE FORWARD (S/N SIDE UPSTREAM) DIRECTIO .

TEST NUMBER 8 PART 252 TEST DESCRIPTION

# TEST SPECIMEN THET CONDITIONS

PRESSURE (PSIA) .	/ (DFG• F)	AVO FLOW RATE (ACEM)	GHUSS DIFF• "RESS PRIMAHY (PSIU)	GR SS O)IFF. PRESS SECONDARY (PSID)	(bētā) · DIELē bkēžs Vag ēkdēz	TARE DIFF. PRESS (PSID)	NET DIFF• PRESS (PSID)
100 <sup>9</sup> •4	7,00	•. 1 <sup>3</sup> 2	264.510	264.0.6	264.510	-0.000	264.516
1009 <u>.</u> ç	ho∙t	.0196	196,967	1,40.967	196.967	-0.000	196.967
1009•4	7,.8	9/ يار	136, 145	136.445	136.,40	-0.000	136.046
1009.4	81 · a	•01.55	83.: 25	33,332	83.178	-0.000	83+179
1009,4	~1•4	•0 ½55	32.409	33.,16	82•7 <u>05</u>	-0.000	82.709
1009.2	±1 <u>.</u> 3	.9079	135.146	136. 46	136.046	-0.000	136.046
1009,2	<sup>1</sup> .2	, 01 al	18425	184,.25	184,425	-0.000	184,025
1009.2	20 <b>.</b> 9	,a126	232,951	232,951	535 951	-0.000	232,951

1ANE DIFF. PAFSS = -1.64000E-04 + -1.26930E-02 (ACFA) + 2.48070E-01 (ACFA)\*\*2 +

U (ACFM) ##3

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PAGE: 3 DATE: 10-7-76

TABLE 73

FLOW RATE VERSUS DIFFERENTIAL PRESSURE CHARACTERISTICS OF TEST SPECIMEN S/N 025 AFTER 100 HIGH PRESSURE (10,000 PSIA NOMINAL) GN2 IMPACT CYCLES AND CONTAMINATED WITH 46 MG OF Fe2 03. FLOW DATA ACQUIRED AT AN INLET PRESSURE OF 1,000 PSIA NOMINAL AND IN THE FORWARD (S/N SIDE UPSTREAM) DIRECTION.

TEST WILL BER 8

PART 252

TEST DESCRIPTION

	• ម៉ំនុង ម៉ូនី ស៊ី ស៊ី ស៊ី ស៊ី ស៊ី ស៊ី	• <del>4 4 4</del> 4 4 4 4 <del>4</del> 4 4 4 4 4 4 4 4 4 4	•	TEST S	PECINEN INL	EL CONDILIONS	****	***	****	***	NET DIFFERENT		
fı	PRESSI ******		{E:PFR TUKE ***********************			***	****	•					
	KĞ,SQ CM	PSI <sub>A</sub>	"ຍ່ເອົີ. κ	. DEG. C	DEG. F	Fitārs/ Min	,cF⊶	SCFM	ке∕нн ем5	₽₽Ş`HB	KG/SD CM DIFFERENTIAL	' PSID '	
	70.956	1009.4	300.2	27.a	80.6	25.2	. 132	.891	1.754	3,868	18.5973	264.516	
	70.956	1409.4	300.2	27.€	80.6	20,1	.0110	.711	1.401	3.088	13.8481	196.967	
	70.956	100 <sup>5</sup> , =	300.3	27.1	8 <sub>0 ,</sub> R	15.1	• 107°	.532	1 • ,48	2,311	9,5650	136.046	
£	70.956	1009.4	300.4	27.2	81.0	10.0	• <b>005</b> 2	.352	• 694	1.527	5.8481	83.179	
•	70.956	1009.2	300.5	27.4	81.4	<b>9.</b> 9	•0052	.349	.68	1.514	5.8150	82 <b>.</b> 709	
	70.956	1009.2	300.6	27.4	81.3	15.1	•u079	.532	1.048	2.311	9.565 <sub>0</sub>	136.046	A
	70.956	1009.4	300.5	27.3	81.2	19-1	-0101	.676	1.331	2.935	12.9383	184.025	
	70.956 *****	1009°C	300.3	27 <b>.</b> 2	80.9	22.8	.0126	.805	1 • 585	3,495	16,3781	232.951	
	7 <sub>0</sub> •9 <u>56</u>	1009.4	30v•4	27.2	81.0								
ı,	9		•1	•1	•2	DEATVITOUS							

#LOWMETER TWO

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER S PART A

TEST DESCRIPTION

Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 415 psia (nominal)

PAGE: 1

DATE: 4/29/76

FLOWMETER CONDITIONS

FLOWMETER ONE

TEST SPECIMEN INLET CONDITIONS

**************************************			****	****	**********	***				_
	FLOW RATE	PRESOURE (PSTA)	T <sub>F</sub> MP (DEG. F)	FLOW ReTE (ACEM)	PRESSURE, (PSIA)	TEMP (DEG. F)	PRESSURE (PSI)	AVG TEMP (DEG. F)	FLOW RATE (ACFM)	1
	D	42	A4-2	.13	47.6	s, 1 • 4	413.7	<sub>8</sub> 2,5	.0149	
	t.	<b>~~.4</b>	Bp.8	•21	49.9	82.	413.	82.4	• 0254	
	c	,a.9	81.6	5ج•	4 <sup>9</sup> •4	8,,5	411.7	82.1	•0303	
1	٢	5.4	80.7	.31	49.7	82.8	424.7	81.7	. 0362	-
	·	49.5	79.6	• 413	47.6	82.8	424	81.2	• 0450	J
	ι	49,5	7P+3	• 49	48.2	8,2.5	422.7	80.4	90564	य
	ሶ	49.5	77,5	.60	4 <sup>8</sup> •0	85*J	422,1	79.8	\$995	•
	(	4 <del>7</del> •:	76 • 3	•70	45 • 5	87.43	42n•8	78.8	• 5756	
	\$1	44	7 <b>5.9</b>	.80	44 • 4	80.9	4.0.1	78.4	•08≩6	
I	ŷ	4=.7	75. 2	.91	43, 3	80° S	418.8	77, 7	<del>-09</del> 42	-
	î	42.3	74.8	1 • 1	42.7	79.6	417.5	77.2	•1 <sub>0</sub> 35'	ij
	•	4 <b>m</b> • 5	74.6	1 • 1	42.9	78.9	416.2	76.7	•1043°	•
	p	a A • 6	74.7	•91	44:4	78•9	416.	76•8		•
	Į,	40.7	74:7	,81	46,7	78,9	415,6	76,8	.0909	
	h	51.1	74 • 7	•71	· 48+4	79•	415.6	76.9	•0824	
ł	11	4 ° • p	74 • 9	•6 <sup>t)</sup>	18+8	79.1	¼ 1s •6	77.0		
	· ·	5 .6	75.1	.50	49,5	79,3	415.6	77,2	. 0596	
	<b>;</b> "	5 .€	75.4	• 4 )	4 <sup>9</sup> •7	79•6	415.6	77.5	+0487	ij
		<b>ቴ .</b> €	75.9	.30	49.9	8n.n	415.6	78.0	0359	-
	r	5. •1	74.4	• >5	49.5	8-•3	416.2	78.3	•0301	

. \_\_ . . . .

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2

DATE: 4/29/76

TEST NUMBER 5

PART A

TEST DESCRIPTION Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 415 psia (nominal)

FLOWMETER CONDITIONS 

TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*

***	FI OWMETER ONE		****	FLO METER TWO		,			
FLOW RATE	PRESCURE	(DEG. F)	FLOW RATE (ACEM)	PRESSURE.	TEMP	PRESSURE (PSIA)	AVG TEMP (DEG. F)	FLOW RATE. (ACFM)	
(.	មា ្រ	77.1	•20	50.5	80 • 7	416,2	₹B•9		
,•	49.]	77 • 8	+13	48.6	8 <b>5 </b>	416.9	79+4	•ó151	

TABLE 74 FLOW RATE VERSUS DIFFERENTIAL PRESSURE PAGE: 3.

DATE: 4/29/76

TEST NUMBER 5

PART A

TEST DESCRIPTION

Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 415 psia (nominal)

TEST SPECIMEN INLET CONDITIONS

PRESSURE (PSIA)	AVG TEMP (DEG• F)	.VG FLON R∆TE (,CF <sup>14</sup> )	aauss DIFF. PRESS PRTM.dY (9514)	GRASS DIFF. PRESS SECONDARY (PSIn)	iVG GROSS DIFF• PRESS (PSID)	TARE DIFF. PRESS (PSIn)	NET DÎFF• PRESS (PSID)
413.0	<sub>5</sub> 2.5	.0149	17.719	17.055	ĭ7.087	~0.000	Ĩ7:087
413.0	. F2.4	.n254	29 056	29 <sub>.</sub> 837	<sup>2</sup> 9 896	.000	29,896
411.7	82.1	•93 3	36.78 <sup>9</sup>	36.161	36.275	•000	36.275
424.7	<sup>A</sup> 1.7	•/302	44.4 1	44.172	44.386	• 0 0 0	44,386
٧٠٠٠ 4 ج	81.o	.0450	57.157	57.520	57•33 <sup>9</sup>	.000	57•33 <sup>9</sup>
422.1	40.4	.0564	74.903	74,903	74.853	.000	74,853
1.554	79.8	• 16 <sup>8</sup> 2	94.0.2	95•13 <sub>0</sub>	95.016	•001	95.016
٠٠٠ ير4	78•8	• 1756	108,454	108.7 <sub>2</sub> n	108.720	.001	108.720
421.1	78,4	, n <sup>R46</sup>	156.918	126,418	126,418	.001	126,418
41d.8	77.7	. 942	148.954	145.858	148.858	• 001	148,858
417.5	77.2	.1035	173.i <sup>93</sup>	173,193	173,193	•002	173,193
416.4	76.7	•1 43	173.425	173,825	173.825	• 0 0 2	173,825
416.2	76.8	•n97 <u>4</u>	155•;; <sup>9</sup> 5	155 • 4 <sup>9</sup> 5	155 • A 95	•001	155•4 <sup>9</sup> 5
415,0	76, 8	.0909	138,420	138,428	138,428	.001	138,428
415.0	76.9	<b>.</b> 0824	120.43.	120.731	120.730	•001	120.730
4 15 •6	77 • 6	• 07 94	98 - 84	97.974	98.1 <sub>2</sub> 9	.001	98+129
415.6	77.2	• 15 <sup>96</sup>	79 585	79,012	79,148	.000	79,148
415.0	77.5	. 487	61 •46 <sup>9</sup>	61 •62°	61 •649	•000	61 •649
4 <sup>1</sup> 5•6	78 • 5	*"359	43.784	44.768	43 • 876	•000	43.876
416.4	78.3	,0301	35,255	35,701	35,829	•000	35,829

FLOW PATE VESSUS DIFFERENTIAL PRESSURE

PAGE: 4

DATE: 4/29/76

PART A TEST NUMBER 5

TEST DESCRIPTION

Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 415 psia (nominal)

TEST SPECIFEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*\*\*

pRESSUHE (PSI4)	αyg TEMp (DEG• F)	AVG FL <sub>C</sub> W RATE (acfii)	GÓDSS DIFF. PRESS PRTMARY (PCIU)	GROSS DIFF. PRESS SECOMDARY (PSIn)	AVG GROSŠ DIFF• prēss (psid)	TARE OIFF. PRESS (PSID)	NET DIFF: PRESS (PSID)
416.2	78 • 9	.n246	2g. 246	28.75 <sub>7</sub>	28.201	.000	28.201
416.9	79•4	. ~151	17.9.5	16.99a	17.152	_0.000	17.152

THE DIFF. FRESS = -3,40000E-05 + -4,44500E-04 (ACFM) + 1,50933E-01 (ACFM) +42 +

a (ACFM) ##3

# TABLE 74 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 5

DATE: 4/29/76

TEST NUMBER 5 PART A

TEST DESCRIPTION

Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 415 psia (nominal)

	***	****	****	NEŢ DIFFEREN	TIAL PRESS								
J	PRESSY		***	TEMPERATURE	***	****	****	FLOW RATE	***	***	,	u 10	
	KG/SQ CM	PSI	neg. K	ĢEG. C	DEG. F	LITERS/ MIN	∆CFM	SCFM	ĸĠ∖Hਔ ⋳⋈≌	GV2 L <sub>B</sub> S/HR	KG/SQ CM Differentiál	PSI <sub>D</sub>	.1
	29.437	<i>4</i> 13, -	301.2	20.0	<sub>8</sub> 2,5	11.6	•014g	.410	2803	1.781	1,2013	17.0g7	
	5 <sub>9</sub> •€31	413.	3,1.2	2 <sup>9</sup> •0	82.4	19.7	• 2 <sup>54</sup>	.696	1:371	3•522	2•101 <sup>9</sup>	29.896	
	2 <sup>8</sup> •946	411.7	301.1	27.8	82*1	23.5	•0303	.830	1:633	3.601	2.5504	36.275	
	29,851	424.7	300.13	27.6	81.7	29.0	.0362	1,023	S.015	4.443	3,1207	44,386	-
	58*815	424 • •	369.5	27.3	81.2	36.0	. j45 <sub>t</sub> ;	1.271	غ <sub>9</sub> 5ء	5,517	4.0313	57.339	
	2 <sup>9</sup> •721	-22.7	300.1	26.9	80.4	45.1	.0564	1,591	3:133	6.907	5.2627	74.853.	.1
	29,675	422,1	299.7	26.5	79.8	54.5	.0682	1,923	3,787	8,349	6,68 <sub>0</sub> 3	95,016	
	29,584	421 eli	299.2	26 •"	78.₽	60.3	<b>.</b> ∙ 756	2.129/	ي9 1• 4	9 • 244	7 •6438	108.720	
	29,538	A2( +1	298.9	25.∂	78,4	67.4	<u>.</u> 846	2.379	4-684	10:327	8.8881	126.418	
1	29.447	, lo. u `	2 <sup>98</sup> .5	25 • 4	77.7	74.9	• ^ 9 4 %	2.645	5.07	11.480	10.4657	148.858	
	29,356	41/.5	298.3	25,1	77.2	82.1	1935	2,901	5,7 <sub>1</sub> 4	12,5 <sup>95</sup>	12,1767	173,193	It
	29.245	410.2	298.	24.9	76.7	82.6	•1 43	2.917	5 • 74 3	12.662	12 •221 i	173.8 <sub>25</sub>	ц
	2 <sup>9</sup> •2 <sup>65</sup>	, 16 • <sub>3</sub>	298.4	24 • <sup>9</sup>	76.8	77.1	• "974	2.724	5 <u> </u>	11:825	10.9324	155 • 4 <sup>9</sup> 5	
	29,219	415.+	294.0	24,9	76.8	71.8	• 0909	2 537	4,995	11,013	9,7325	138,428	
	56.512	415.4	298.1	24.9	76.9	65.1	824	2+300	4•53:.	9.986	8.4881	120.730	
,	56.518	415.m	298.2	25.0	77.0	55.6	.0704	1.964	3.86]	8.525	6.8992~	98; 129	
	29.219	215.€	29A.3	25•1	77.2	47.1	• 5 <sup>4</sup> 6	1.663	3.274	7:217	5-5647	79.148	
	29.219	, 15 es.	298 <sub>*4</sub>	25 • 3	77 •5	38.5	• '497	1.359	2.676	5 •899	4 *3343	61-649	j
	59,519	415.5	298 7	25 5	78 <sub>+</sub> n	28.3	<b>.</b> 2359	1,000	1.970	4,342	3,0848	43, 876	
	29.205	/10.2	598.9	25.7	78,3	23.8	•6301	.639	1 • 65 <u>ì</u>	3•64∩	2.5190	35,829	

FLOW PATE VERSUS DIFFERENTIAL PRESSURE

DATE: 4/29/76

TEST NUMBER 5

PART A

Clean Condition - Flow Rate versus
Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 415 psia (nominal)

PAGE: 6

		TEST SPECIMEN INLET CONDITIONS  ***********************************											
ļ	PRESSY		**********			***	***	***		•			
	KG/SQ C4	PSĮ,	DEG. K	DEG. C	0€Ģ. F	LITERS/ MIN	ACFM	SCFM	Kė̀\H凇 ¢uS	GN2 LBS/HR	kg/sq cm Differential	·PSID	
	20,265	410.2	299.2	26.1	78 • 9	19.4	.0246	.6g6	1,350	2.976	1.9827	28:201	
	29.311	10.9 ****	595.5	26.3 ****#	79.4 *#####	11.9	• 1 <sup>5</sup> 1	.421	1853	1.827	1.2059	17.152	
	29 <b>.</b> 35 e	417.5	299.2	26.1	78 ec								
	-199	٤.٤	•9	•9	1 • 7	DEVIATIONS	6						

# TABLE '75 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1

DATE: 4/29/76

TEST NUMBER 5

PART A

TEST DESCRIPTION

Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 700 psia (nominal)

FLOWMETER CONDITIONS TEST SPECIMEN INLET CONDITIONS \*\*\*\*\* 

FLOWMETEK UNF			***	FLOWMETER TWO	***	ı		e an	
FLOW RA		TEMP (DEG. F)	FLON RATE (ACEM)	Pressure. (Psia)	T <sub>FMP</sub> (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	FLOW RATE (ACFM)	
t	50.6	75 • በ	.13	50.5	74.1	490.3	75.6	.0097	
r	5, .8	74.2	• 20	50.5	76.4	686,4	75,3	+0147	
ı	51 + 6	72+3	• > 5	50.7	76.5	697.4	74.9	.0187	
6	5).2	72.6	.29	50 <b>.7</b>	76.5	686,4	74.5	.0217	•
•	40.7	7 · • 4	•39	49	76.4	686,4	73,9	•0280	Ú
**	. 4.7	71	• 49	%8•0	7 <u>5</u> .9	686,4	73.0	+0344	ч
ŗ	49.2	6F+3	•59	47.1	75+0	686,4	71.7	•0405	
	42.3	66.4	-69	47.1	73.8	686.4	70+1	• ō474	
	S. "A	64.7	•84	46.5	72.3	682.5	68.5	• 6544	
t	49.5	64.3	•90	45.3	71.9	682,5	67.1	~~;613	
t	48.0	61.6	1.01	45.4	68,9	694,3	65,2	. 0660	ı,
•	65-1	61.48	1.01	45.4	67.4	694.3	64.1	• ō663	1
t,	43.5	61.9	. 98	46•₹	67.;	690.3	64.0	0605	
í	52	61.0	.80	48,6	67.1	690,3	64.0	.0562	
J	52	61.3	•76	48.6	67.4	69n <b>.</b> 3	64.3	±0490	
	۲،۰5	6).9	•60	49.0	67.8	690.3	64.8	-0422	
•	S. A	62.2	• 49	49•4	68. <sub>7</sub>	696.3	65•2	• 0353	
J	4~.l	63+^	• 39	48•4	68.9	690	65+ <del>9</del>	•0277	j
	42,9	64.1	•30	48,4	69,6	690,3	66,9	.0207	٠,
	5 • <b>1</b>	64 • 9	• 25	49•5	70.4	690.3	67•6	+0179	

### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 4/29/76

TEST NUMBER 5

PART B

TEST DESCRIPTION

Clean Condition - Flow Rate versus
Differential Pressure (Test Specimen
[S/N 6] Inlet Pressure 700 psia (nominal)

TEST SPECIMEN INLET CONDITIONS

****	FIONMETER ONE			FLOWMETER TWO	***			
FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG. F)	FLOW RATE (ac <u>f</u> m)	PRESSURE, (PSIA)	ŢEMP	PRESSURE (PSIA)	TEMP (DEG; F)	FLOW RATE!
n	44.7	45+8	• 50	48.4	70+9	¿90.;3 <sup></sup>	68.4	.0138
Ų	47.4	66.9	•i3	47.1	75.6	69ñ.3	69.2	0087

.

TABLE 75

PAGE: 3 DATE: 4/29/76

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

Clean Condition - Flow Rate versus

TFST NUMBER 5 PART B TEST DESCRIPTION Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 700 psia (nominal)

TEST <PECIOEN INLET CONDITIUMS

J,

PRESSURE (PŠIA)	AVG Temp (Deg. F)	AVG FLOW RATE ()CFM)	GEOSS DIFF. PRESS PRIMARY (PCID)	GROSS DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS: (PSID)	ì
69n• <del>3</del>	75.6	• 9097	10.519	9.97a	9.995	-0.001	9.995	
6 <sup>8</sup> 6•4	75∙3	.0147	15.319	14.997	15.00ª	<b>40.001</b>	15.008	
690.3	74.9	.0187	19,436	19.516	19.577	-0.001	19,578	
686.4	74.5	.6217	23.793	23.000	23.101	÷0.001	23,102	
646.4	73.9	•0280	30.789	30.641	30.715	-0.001	30.716	
686.4	73.0	,n344	38.468	38,580	38,724	<b>=0.001</b>	38,724	Ŋ
646.4	71:7	.0416	47.ànl	46.885	47.093	#0•001	47.094	<u>.</u>
686.4	7r•1	. 6474	56,845	56,116	56.482	-0.00 <u>1</u>	56.483	
682.5	68 <u>.</u> 5	.0544	67.510	66.242	· 66 • 62 <u>6</u>	<b>⇔</b> 0.000	66,626	
<b>6</b> μ5• <i>Ά</i>	67.1	.0613	18_23	77.00ĭ	77.50?	-0.000	77.507	
694.3	65.2	. 9664	85,955	85.861	85.9 <sub>0</sub> 8	• 0 0 0	85.909	a
690.3	64.1	.0663	85,955	85.861	85.908	•000	85.909	4
690.3	64.0	.0605	76.567	76.368	76.318	#0.000	76.318	
69n <u>•</u> 3	64 <b>.</b> s	. 6562	69. ñ 15	69,406	69.210	⇒0•000	69.211	
69(1+3	64.3	.n4 <sup>9</sup> 0	58.731	58,964	58,847	<b>4</b> 0 = 000	58,848	
69(-3	64•8	• ñ422	5n.149	49.774	49.96]	=0+001	49.962	
690.3	65.2	.0353	40.254	40.423	40.63 <u>6</u>	-0.001	40.639	
690.3	65,9	.0277	30.789	30,354	30.572	#0 <u>.</u> 001	30,572	J
eāt•a	66.9	·62^7	22.597	22.093	22.300	-0.001	22.300	
691+3	67.6	.0179	19.502	18.829	19.015	<b>⇒0,001</b>	19.016	

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 4

DATE: 4/29/76

TEST NUMBER 5 PART 8 TEST DESCRIPTION Clean Condution - Flow Rate versus Differential Pressure (Test Specimen [S.N 6] Inlet Pressure 700 psia (nominal)

TEST <PECI·EN INLET CONDITIONS

			ദ്ദ്രട	GROSS				-
PRESSURE (PSIA)	LVG TEMP (DEG. F)	AVG FLOW RATE (-CFM)	DIFF. PRESS PRIMARY (PSID)	DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)	J
690,3	6a • 4	.013 <sub>H</sub>	14.510	14.254	14 <sub>4</sub> 3 <sub>8</sub> 6	=0.001	14.3 <sub>87</sub>	
69,,3	69 <b>°</b> 8	.0087	9,506	8 និង	9,046	0.001	9.047	

T.RE DIFF. PRESS = -3.60000E-04 + -3.3161(E-02 (ACFM) + 6.33359E-01 (ACFM) +2 +

0 (ACFM) \*\*3

TEST SPECIMEN INLET CONDITIONS

PAGE: 5 DATE: 4/29/76

## FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 5 PART 8

TEST DESCRIPTION

Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 700 psia (nominal)

NET DIFFERENTIAL PRESS

	***	***	****	****	****	****	***	****	***	***	*****	40.444.4
I,	PRESS <u>.</u> Presser			TEMPERATURE	***	*****	*****	FLOW RATE	***	****	om on a combi	
	KG/SQ CM	P\$I,	DEG. K	DEG. C	DEG. F	LITERS/ MIN	1CFM	SCFM	KĞ\HĞ GN5	GN2 Las/HR	KG/SQ CM DIFFERENTIAL	· · · · PSĮD.
	48,536	E.064	297.4	24.2	75.6	12.8	.0097	.452	•890	1.962	•7027	·9,995
	48,260	486.4	297,2	24.1	75.3	19.2	.0147	,678	1.334	2,941	1.0552	15,008
	48.536	494.B	297.6	23.8	74.9	24.6	· 1·187	.868	1.710	3.769	1.3764	19.578
	48.260	£80 <b>.</b> 4	296.8	23.6	74.5	28.4	•n217	1.003	1.976	4 • 355	1.6242	23.102
	48,260	586.4	296.4	23.3	73.9	36.8	.0280	1,300	2,559	5.642	2,1595	30.716
	48,260	480.4	296.0	22 <b>.</b> 8	73.0	45.3	.0344	1,599	3.149	6.942	2.7226	38,724
	48.26n	486.4	295.2	25•0	71.7	53.5	.0406	1,889	3.719	8,199	.3.3119	******
	48,260	£86 <sub>£</sub> 4	294.3	21.1	7 <sub>0•1</sub>	62.6	.6474	2.211	4.353	9.597	3,97 <sub>11</sub> -	-26.*§3
	47.985	482.5	293.4	20.3	68,5	71.8	.0544	2,535	4,991	11,003	4 26843	- 66 • 656-
1	47.965	A82.5	292.6	19.5	67.j	81.0	. 613	2,861	5.633	12:420	5,4493	77 <del>.</del> 5 <del>07</del>
	48.811	494.3	891.6	18.5	65.2	89.0	.0660	3.143	6.189	13.644	6.0400	85' <b>.</b> 909 <sub>11</sub>
	48,536	490.3 ±	291.0	17.8	64.1	89.2	.0663	3,150	e*50\$	13.674	6.0400	82 <u>-</u> 593
	48,536	F.064	291.9	17.8	64.0	81.3	•a6n5	2,872	5 • 655	12-467	-5:3657	<del>76.</del> 318—
	48,536	£90.3	291.0	17.8	64.n	75.6	• 11562	2.671	5.252	11 <u>.</u> 595	4.8660 ~ ~	69.•\$1 <u>1</u> .
	46,536	£90,3	291,1	18.0	64,3	65.8	.0490	2,325	4,579	10.095	4'-1374" "	28. 9 (8.
ŀ	48,536	E. UPA	291.4	18.2	64.8	56.7	•0422	2.003	3,943	8 693	3.5127	49 <b>,9</b> 62
	48,536	,£90.3	291.6	<sub>]</sub> A • 5	65 <sub>•2</sub>	47.4	.0353	J •674	3 • 296	7.267	2.0572	'40 <del>-639</del> '
	48,536	E.09A	292.0	18.9	65,9	37.1	.0277	1.310	2,579	5,686	2.1494	'30.572'
	48,536	x . nea	292.5	19.4	66.9	27.7	.0207	.978	1 • 925	4 <u>*</u> 544	· · · · · · · · · · · · · · · · · · ·	22 <b>:3</b> 00
	48,536	490,3	293.0	19.8	67,6	23.9	.0179	.843	1 <u>• 6</u> 60	3,660	1.3369	19,016

TABLE 75 PAGE: 6

FLOW RATE VEPSUS DIFFERENTIAL PRESSURE DATE: 4/29/76

TEST NUMBER 5 PART 3

T R TEST DESCRI

TEST DESCRIPTION Clean Condition - Flow Rate versus
Differential Pressure (Test Specimen
[S/N 6] Inlet Pressure 700 psia (nominal)

***	***	***			EŤ CONDITIONS		******	****	****	NET DIFFERENTI	AL PRESS
PRESSU ******			TEMPERATURE	****	***		FLOW RATE	****	***		
KG/SQ CM	P∳I ≀	DFG. K	VEG. C	DEG. F	LIT#RS/ Min	. CFM	SCĘM	KĞ\HÄ ens	rĕ∂\HB Fĕ∂\HB	KG/SQ CM Differential	PSĮD
46.536	400.3	203.4	20.2	68,4	18.5	,7138	,652	. 1.284	2.832	1.0115	14,387
48.53n ****	F , .€.)	293.9 ****	2^•7	59.2 ****	11.6	097	.409	•90ē	1•777	•6361	9.047
48,423	488.7	273.6	z-,5	68,6							
.162	2.4	3.1	s• ,	3.5	LEVIATIONS						

í

# TABLE 76 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1

DATE: 4/29/76

TEST NUMBER 5 PART C

TEST DESCRIPTION

Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 1000 psia (nominal)

TEST SPECIMEN INLET CONDITIONS FL:)WMETER CONDITIONS

***			****	ÉLUMMETER TWO					
FLOW RATE (ACFM)	PhESGURE (PSTA)	Toda (usa. F)	FLOW RATE	PAESSURE. (PSI:)	TEMP (DEG. F)	PRESSURE	AVG TEMP (DEG. F)	AVG / FLOW RATE / (ACFM)	i
o	50.1	ν <b>΄ •</b> 4	.13	49.7	· 3 • u	15n6.7	0,2°5	.0063	
O	5 +1	A #3	•21	49.5	83.0	1906.7	81.7	10102	
0	no.7	70.3	. ~ 5	49.4	8241	1006.7	81.2	.0125	
0	40.7	78.3	.31	49.2	<b>43.</b> 0	1002.7	80.6	.0150	
U	3, ,2	70.4	.41	49.5	82.4	1202.7	79.4	.0200	.t
o	nc.9	70.	•5	49,1	F1.4	1002.7	77.7	•0242	4
Ó	e.5	71 **	•60	46.4	79.9	1002.7	75.7	•0289	
0	40,3	67.1	,7e	47.0	78.2	1002.7	73,6	0335	
0	40.9	P7 • *	•8	47.3	76.4	998.7	71.6	•0379	
r	40	64.5	•91	(7.1	77	998.7	69.1	40427	
r	40.9	69.9	1.51	46,3	71.8	994.8	67.4	40471	n
n	4#.9	61.5	1. 1	46+3	69.4	994.B	65,5	•ô471	Ţ
O	~· .1	151.5	•91	7.8	69.0	994.8	65+3	•0436	
6	40.5	61 , 8	.80	47.6	69.0	994.8	65.4	.0385	
٩	ar + 1	45.5	•7 •	47.6	69.7	994.8_	65.7	<b>∗</b> 0334	
o	48.9	6. ۸	•64	.7.8	69.6	994.8	66.2	•0290	
n	40.5	62.3	•50	48.4	70.1	99ŋ <b>.</b> Წ	66.7	.0244	
ŋ	40.3	64.5	<b>4</b>	49.6	71. 4	99r.H	67.8	•0197	j
43	4.0.7	5¢.9	•3	44.5	72.	994.13	68.9	•0145	
41	φ., τ.	66.7	•8\$	୫,୫	70,7	994.8	69.7	.0123	

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2

DATE: 4/29/76

TEST NUMBER 5

PART C

TEST DESCRIPTION

Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 1000 psia (nominal)

FLOWMETER CONDITIONS

TEST SPECIMEN INLET CONDITIONS

,	****	FLOWMETER ONE			FLOWMETER TWO	****		-	e de desperable delle delle Tags da me
	FLOW RATE	PRESSURE (PSTA)	TEMP (DEG• F)	FLOW RATE (40 <u>°</u> M)	PRESSURE. (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG- TEMP (DEG. F)	FLOW RATE:    (ACEM)-
	0	40.5	67.p	•20	49.0	73.4	994.0	Żn.6	· · • 0096 -
	0	40.3	69+2	+34	48.6	74.4	994.8	71.8	•0067

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TABLE 76

PAGE: 3 DATE: 4/29/76 FLOW BATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 1000 psia (nominal) PART C TEST NUMBER 5

TEST <PECI·EN INLET CONDITIONS

		••							
	PRESSURF (PSIA)	۸۷¢ TEMP (DEG• F)	AVG FLOW RATE (+CFM)	gioss DIFF, PRESS PRTM-RY (PSIU)	GRUSS DIFF. PRESS SECONDARY (PSIn)	AVG GROSS DIFF• PRESS (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)	.1
	1006.7	A\$*S	.0.163	6,191	6,790	6.991	-0.000	6.891	
	1006.7	ч1.7	.0102	11.120	11,112	11.066	-0.000	11.066	
	1006./	°1+2	. 125	13. 195	13.411	13.903	<b>~0.000</b>	13.903	
	1002.7	80.6	,0150	16,43	10.826	16.828	-0.000	16.828	
	1002.7	79.4	- 656	23,13	23. 1167	23.099	-0-000	23.099	
	1002./	77.7	. 'S S	28.023	28.803	28.863	-0.000 °	28.863	ş
•	1002./	75,7	.12 <sup>89</sup>	35 49.,	3,5,241	35,315	-0.000	35,315	
	1002.7	73.6	.~335	41.900	41.749	41.829	-0.000	41.829	
	998./	71.6	79	48.416 /	48.156	48.286	-0.000	48.286	
	998.1	49.1	.0427	55, 984	55,624	55.754	-0.000	55,755	
	994 <b>.</b> ¤	67.4	. 471	63.413	63.2 9	63.311	-0.000	63.311	
	994.8	65.5	. 471	63.464	64.525	63.595	-0.000	63,595	1
	994.8	65.3	.0430	57.490	57,520	57,455	-0.000	57,456	
	994.6	65.4	. 385	49.24	49,542	49,691	-0.000	49,691	
	994.8	65.7	.4324	42,280	4 <b>1.</b> 980	42.130	-0.000	42,130	
	994.8	66.2	.02 <sup>9</sup> 0	36,735	35,816	35,976	-0.000	35,976	
	994.8	65.7	. 2.44	29.794	29.377	29 <b>.</b> 586	-0.000	29.586	
	991.0	67 <b>.</b> 8	. 197	23.555	22.495	23.075	-0.000	23.075	J
	994.8	\$h.9	. 145	16.7 ib	16,426	16.565	=0.000	16.566	
	994,8	69.7	. 160	14. 182	1 3. 454	13+968	-0.000	13.968	

TABLE 76
FLOW RATE VESSIS DIFFERENTIAL PRESSURE

PAGE: 4

DATE: 4/29/76

TEST WIMPER 5

PIPT C

TEST DESCRIPTION

Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 1000 psia (nominal)

TEST RPECTEN INCET FORMITIONS

(bàl7) buesenhe	TE4P (DEG. F)	F. OW RATE (ACFM)	qp/SS DIFF <sub>*</sub> PRESS PRTV·RY (PSIU)	nROSS DIFF. PRESS SECONDARY (PSIO)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)
994.4	7	- <i>Գ</i> ՄՕ-	10.932	19.590	10.715	+0.000	10.715
994.0	71 <sub>+</sub> 8	.0007	7.517	7.347	7,432	-0.000	7.432

T RE DIFF. RESS = -1.6.000F-04 + -1.2603 19-02 (4CFM) + 2.48070E-01 (ACFM) 402 +

n (ACFM)##3

# TABLE 76 FLUM RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 5 DATE: 4/29/76

TEST MUYAER 5 PIRT C

TEST DESCRIPTION Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 1000 psia (nominal)

	***	****	医格尔特氏 经公司 计设计设计	7EST S	PECIMEN INL	ET CONDITION	5 *******	****	****	***	NET DIFFERENTI		
;	PRESS			TENPEK, TURE	***	***	***	FLOW RATE	****	****			
	KG/SQ CM	P51.	DE0. *	ņ∈G. ∕	DEG. F	L(T-65/	" CFM	SCFM	KĜ\HŘ GNS	GN7 LHS/HR	KG/SQ CM Differential	PSĪD	·
	70.775	1~06.7	301.7	27.	82,2	12.0	.0063	.423	.832	1,835	.4845	6,89Ï	
	70.775	1 00.7	310.0	27.5	<b>ย</b> ั.7	19.3	•01/2	•68n	1:340	2.954	.7780	11.066	
	70.775	1 100.7	31 1+5	:7.4	81,5	23.7	•41-5	.837	1.64?	3+631	•9775	13.903	
Į,	70,496	[*02.7	340.8	27.1	øn.6	28.4	.0150	1.003	1.974	4.352	1.1831	16,828	
	70.496	1:02.7	500.7	′ 6 <b>.</b> 3	79,4	38.0	• 1200	1.343	2.645	5.831	1.6240	23.099	1
	70.496	1-0,001	298.5	25.4	77.7	46.2	•"24%	1.630	3.210	7.077	2.0293	28,863	18
	70,496	1-04,7	297.4	24.3	75.7	55.3	.0289	1.953	3.845	8.479	2.4829	35.315 <sup>,</sup>	
	70.496	1102.7	296.3	23.1	73,6	64.2	335	2.266	4.464	9.838	2.9409	41.829	
	70+218	99b.7	295.2	55.	. 71.6	72.8	.0379	2.570	5 <u>.</u> 060	11•155	3.394B	48,286	
ì	70.218	96.7	,93. H	pr.b	69.1	82.3	.0427	2.906	5.722	12,615	3.9199	55.755	
	69,939	٥94 ۽ ۾	292.2	19.6	67.4	90.8	.0471	3,205	6.312	13.915	4.4512	63,311	
	69.939	994 <b>∓</b> ñ	291.5	;8.6	65,5	91.1	. 471	3.217	6 <u>•</u> 334	13.965	4.4712	63,595	,
	69.939	094,A	~91.6	18.5	65.3	84.2	•1)436	2,975	5 • 85월	12:914	4.4395	57,456	
	69.939	09 <b>4.</b> ₫	291.7	18.6	65.4	74.4	, 9385	2,627	5.173	11:404	3.4937	49,69ĩ	
	69.939	n94.4	291.9	18.7	65.7	64.5	• 334	2.277	4.483	9:883	2.9621	42.130	
i	69,939	094,A	292.2	19.0	66.2	56.0	.0290	1.977	3,892	8,581	2,5294	35,976	
	69.661	n9#	292.5	19.3	66.7	46.9	• 244	1.657	3•264	7+191	2.0801	29,586	
	69,661	49. "н	93.	19.9	67,8	37.8	.1197	1.335	2•68 <u>₽</u>	5.795	1.6223	23,075	i
	69,939	794,4	242.4	2 .5	68.9	27.8	. 145	,983	1.935	4.265	1.1647	16,566	
	69.939	n94.a	204.1	5 • è	69.7	23.6	. 123	.834	1.641	- 3-618	.982n	13.968	

FLUW PATE VERSUS DIFFURENTIAL PRESSURE

PAGE: 6

DATE: 4/29/76

TEST NUMBER 5

PART C

Clean Condition - Flow Rate versus
TEST DESCRIPTION Differential Pressure (Test Specimen
[S/N 6] Inlet Pressure 1000 psia (nominal)

	****	***	***			EŤ (UNDITIONS	***	****	****	***	NET DIFFERENTI	
•	PRESSU		计计算机设计计算机	TE, PERATURE	***	***	* * * * * * * * * * * * * * * * * * * *	FLOW RATE	***	***		
-	KG/SQ CM	Pol	ዕዮፍ. የ	DEG. (	DEG. F	FIT-BS/	CFM1	SCFM	Kė\HŘ evS	GN? Las/Hr	KG/SQ CM DIFFERENTIAL	PSID
	69,939	e94.2	794,6	21.5	70.6	18.5	•0006	,652	1.284	2.931	.7534	10.715
	. 69.939 *****	094 <b>.</b> 5 5####	295 <u>.</u> 3	22.) *****	71.8	12.8	.11067	<b>.</b> 452	<b>,</b> 890	1.962	•5225	7,432
	70.180	196.2	295,4	22.2	72.0							
	+313	4.4	>.	2.7	` 5.·	DEVIATIONS						

TABLE 77
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 4/28/76

\*\*\*

TEST NUMBER 5

PART D

TEST DESCRIPTION

Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 2900 psia (nominal) TEST SPECIMEN INLET CONDITIONS

FLOWMETER CONDITIONS

٠,	ងត្តសម្តស្តស្តស្តស្តិ៍ដូចប៉ុស្តែក្តីសង្គប្តីក្នុងស្ត្រីសង្គប្តីក្នុងសង្គប្ត			***	FLOWMETER TWO	***				
	FLOW RATE	PHE SEURE	TEMP	FLOW RATE (ACFM)	PRESSURE,	TEMP (DEG• F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	AVG FLOW RATE TACEMS	ช
	n	\$r.1	78.6	•13	49.7	78+9	2887.8	<b>7</b> 8•8	:. :0055	
	0	5].r	77.2	•20	50 <u>*</u> 4	78.9	2887.8	78.1	•0635	
	o	a1.0	75.6	• 25	, 5 <sup>0</sup> •6	78.8	2891.9	77.2	•0044	
l,	O	€∿•8	73.2	•59	50 <u>•</u> 2	78,4	2891.9	75.8	¿0051"	
	1	40.1	69.8	• 40	48 <u>•</u> 3	77.6	2891.9	73.7	±0066. —	¥
	1)	4B.9	65±p	• 49	47.9	76•r	2891.9	70.6	· 0085	u
	O	49•5	58+6	*5 <sup>9</sup>	4 <sup>8</sup> •1	72+7	2 <sup>891.9</sup>	65•6	₹00 <b>9</b> 8	•
	9	42.1	52.7	•69	48.1	68,9	2887.8	60.8	.0116	•
	U	5r.6	48 • n	•80	48.7	65.1	2887.8	56.6°	• 0135:	
)	Ç	49.1	45.0	. 90	4628	61 • 7	2887•8	53•4	·	
	Ŀ	48.9	42.6	.90	46,6	58,5	2887,8	50,5	.0145	- II
	p	51.2	42 • n	•79	48.3	57.	2883.8	49.5	•0135.	U
	0	54	43.4	.69	48.7	57.7	2883,8	50,5	- Tito:	
	(t	40.5	44+1	•59	48 • 1	58.	2883.8	51.1	1 1 <u>40</u> 098	
	()	49.1	44.9	• 50	47 <u>•</u> 9	58+6	2883.6	51.7	60083	
;	G	5 <sub>1</sub> ,1	46.0	.40	49,3	59,4	2883,6	- 52.7		• ••
	ů.	49.9	47 • 6	• 58	49 • 1	64.4	2883.8	54÷0	• 0049	ıi
	ŗ	45.5	49•3	• 25	48.9	61 • 7	2887.8	55.5	₹0043	y
	0	41.3	51.2	,20	48,7	63.0	2887.8	57,1"	.0035	-
	0	47•3	54.2	•13	48.1	64.2	2887.8	58•7	-0022	

FLUM PATE A. SUS DIFFERENTIAL PRESSURE DATE: 4/28/76

TOST MENGER 6 PART O TEST DESCRIPTION

Clean Condition - Flow Rate versus
Differential Pressure (Test Specimen
[S/N 6] Inlet Pressure 2900 psia (nominal)

PAGE: 2

125T <f< th=""><th>CC1 EN TELET CON</th><th>~ITJUN5</th><th></th><th></th><th>(S/N C) INI</th><th>et riessure 2500</th><th>berg (Howingi)</th><th></th></f<>	CC1 EN TELET CON	~ITJUN5			(S/N C) INI	et riessure 2500	berg (Howingi)	
(,15d) 14n5,22n9 14n5,22n9	ب√: 1 <sub>2</sub> p (رمين+ F)	ren ( CEH)	:7)\$\$ 1)IFF, 1465\$ pq:14,144 (pq[u)	GROSS SECONDARY (PSI)	AVG GRUSS DIFF. PRESS (PSIU)	TARE UIFF. PRESS (PSID)	NET DIFF• PRESS (PSID)	,
2647,4	73.5	, 702Z	3.109	3.188	3.148	-0.000	3.148	
2307.0	79.1	35	4.923	5.010	4.966	-0.000	4.966	
ShA1.A	77.7	¥9544	6.79¥	61378	6•33 <sup>9</sup>	.000	6•339	
2671.7	75.4	ldcn.	7, 361	7,462	7,412	.000	7,412	
5.A1.A	11.7	66	9,793	9.970	9.885	• 0 0 0	9,886	
2441.×	15. +4.	\$269.	12.540	12.590	12.541	•000	12.541	J
5621.2	40.0	้าบิลิต	15,475	15,571	15,524	-0.000	15,525	
2667.3	£ r, _ 3	.0116	ኒጸ, ማኔታ	19,832	18.807	-0.001	18.808	
2607.8	56.6	. 135	22,457	સ્ટ.49H	22.475	-0.002	22.478	
2887.0	5 1 • 4	• 145	24,92,	74.648	24•8 <sub>3</sub> 5	=0.00g	24.8 <sub>3</sub> 6	
2887.0	30.B	•n145	24,947	24,963	24,955	-0.003	24,955	
2603.0	49.5	. 132	22,395	22.326	22.36 .	<b>~0 • 0 0 2</b>	22,361	j
2883+8	<b>#</b> / <b>+ #</b> ,	.^117	19,494	19.576	19.553	-0.001	19.554	
2883 4	51,1	.00 <sup>98</sup>	16,754	16,085	16,125	-0.000	16,125	
2883.0	5 <sub>1,•</sub> 7	•9083	13.595	13.284	13.289	•000	13.290	
۵۰۰ عوم	52.7	•0968	10.61;	13.543	10.577	•000	10,577	
2853.5	54.,	.0049	7 1736	7,576	7,656	.000	7,656	
2021.0	F5• <b>5</b>	•9143	6.49	5+435	6.492	• 0 0 0	6.492	ı
2601.5	£7+1	. 7 , 35	5•-3¤	5.124	5.180	-0.000	5•180	
\$t07.0	50.7	.1788	3.234	3.188	_ 3.211	<b>-0.000</b>	3.211	

T -E .. IFF, "HFSS = -1.24600F-09 + 4.88463--- (ACFit) + -4.00723E 01 (ACFM) 402 +

0 (ACFM) ##3

# TABLE 77 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE; 4/28/76

Ú

TEST NUMBER & PART 5

TEST DESCRIPTION

Clean Condition - Flow Rate versus Differential Pressure (Test Specimen [S/N 6] Inlet Pressure 2900 psia (nominal)

PP:55		******	TEI,PEK.TURE	****	****	****	FLOW RATE	****	****			
KĢ/SQ CM	PōI	DEG K	ĥEG. C	DEG, F	LITCPS/ MIN	"CFH	SCFM	κ <b>ĕ\</b> μὰ <sup>gω</sup> s ,	GNS LRS/HR	KG/SQ CM Differenti <sub>a</sub> l	PSID	,
£5•£0\$	2981.5	2 <sup>99</sup> •1	26	78.8	12.0	•0022	.425	•83ō	1.844	.2213	3.148	
203.633	236727	2 <sup>98</sup> ∗ <sup>d</sup>	25.5	78.1	19.1	.3035	•674	1:32!	2+926	.3491	4.966	
203.312	2791.4	Sah 3	25,1	77.2	24.2	.0844	.853	1,679	3.703	.4457	6,339	
203.310	2491.9	297.5	74.3	75.R	28.0	. 051	.988	11945	4:287	+5211	7.412	•
203.318	491.0	۶۶۴۰۶٫	29.1	73.7	36.6	• 1056	1.291	2:541	5+602	•6950	9,866	
203.310	2091.0	294 5	21,5	70,6	45.5	.7082	1,606	3,162	6.972	8817	12.541	
203.314	2^91.0	2 <sup>9</sup> 1•1	18.7	65,6	55.1	• '0'9B	1.945	3.825	8,441	1.0915	15.525	
203.033	2 <sup>a87</sup> •*	ي. <sup>89</sup> ء	16.0	60.8	65.4	.0116	2.311	4 <u>.</u> 550	10.030	1.3223	18,808	
203.033	2°87 <sub>.</sub> 8	286,4	13.6	56,6	76.9	.3135	2,714	5,344	11.781	1,5804	22.478	
203.033	2087.7	295.	11.9	53.4	83.3	· 145	2.943	5 <u>.</u> 79 <u>5</u>	12.777	1.7461	24.836	
203.033	z687.5	8 <sub>3•5</sub> ,	10.3	50.5	83.8	- 1145	2*959	5.8 <sub>2</sub> !	12:847	1.7545	24° <sup>9</sup> 55	
202.744	£884°	235.9	9.7	49 5	76.4	.1132	2,699	5,315	11,717	1,5721	22,361	•
202.749	5483	283.5	10.3	5,,5	67.4	• 117	2.379	4,684	10.326	1.3748	19,554	
202.747	2.E3.¤	283.4	1 6	51.1	56.6	• 1048	2.000	3 • 93ñ	8.681	1.1337	16.125	
202,749	2983.4	94.1ع	11.0	51.7	47.5	.4063	1,677	3:304	7.282	• <sup>9</sup> 344	13.290	
202.744	8093.8	284.7	11,5	52.7	38.8	.9068	1.370	2,69/	5,946	.7436	10.577	
202.744	ಚ.೬೫೯೬	295.4	12.2	54.3	28.3	• 3049	1.000	1:969	4.341	•5383	7,686	
203.033	ph67.0	286.2	13.1	55.5	24.5	•0043	.864	1:702	3•753	• 4565	6• <del>4</del> 92	
203,633	8287 <b>.</b> .	297.1	14.0	57,1	19.7	.0035	695	1,369	3.017	.3642	5,180	
203•(33 ####	2 187. ·	##### 588*	14* <sup>2</sup> ****	58.7 ****	12.3	•6022	.434	<u>.</u> 054	1 : 882	.2257	3.211	
203,619	2081.0	£, qnS	16,2	61.1								
•102	2.3	5+1	5.1	9.2	DEVIATIONS		<b>s</b>					

TABLE 78 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 7-8-76

TEST NUMBER 56 PART G TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE- TEST SPECIMEN [S/N 020] INLET PRESSURE 415 PSIA (NOMINAL).

FLOWMETER CONDITIONS TESŤ SPECIMEN INLĒT ČONŌIŤÍONS

þ	******	FLOWMEIER ONE		FLOWMETER TWO					* * * * * * *****
	FLOW RATE	PRESSURE (PSTA)	TEMP (DEG <u>*</u> F)	FLOW RÄTE (ACFM)	PRESSURE. (PSI4)	TEVP (DEG. F)	PRESSURE (PSIX)	ĀVÕ TEMP (DEG. F)	FLOW RATE (ACFM)
	•14	49.5	78 <u>:</u> 5	•13	49.1	79.1	417.4	78.8	0164
	.22	42.1	78.2	.21	48.9	78.9	41n.9	78.6	. 0261
	•28	42.9	. 77 <u>*</u> 7	• # 6	49.5	78.9	416.1	78.3	• ō323
ļ	•35	49.1	77•5	•=1	48.7	78.7	△15•Š	₹8 <b>.</b> 1	•0370
	•41	49.7	76.9	.41	49.ì	78.4	4 <u>1</u> 4∎8	77.7	. 5489 · · · · · · · · · · · · · · · · · · ·
	.51	50.1	76.5	•50	40.1	78.2	413.5	77.4	•0666 ~- "
	•60	49.9	7621	•60	48.7	77.9	412.9	77.ŏ	· ···•ô717
	•69	49.5	75 <u>•</u> 8	•71	48.9	77.6	411.6	76.7	*** •0Bj0
	•79	ភ្លំ 5	74•ĭ	.81	48.5	72.9	416.1	73.5	• 0951
'n	.88	99.7	74 <u>.</u> 2	•91	47.8	73.2	415.5	73.7	·1045
	.88	49.7	74 <u>.</u> 4	•91	47.8	77.6	415.5	74.0	
	<b>,</b> 79	49.7	74.6	.81	47.9	74.0	415 <sub>•</sub> 5	74.3	
	•69	5.0¢	74•8	•70	48.9	74.5	415.5	74.6	~~.ô834 <sub>/</sub> ~
	•60	÷0.5	74.8	•60	49.1	7 <b>ĕ.</b> 5	416.Ī	74.7	•0720
	•51	50°1	75•0	•51	49.3	74.6	416.1	74.8	∙õ6ōB
r }	•41	50.1	75 <u>.</u> 2	• 40	49.3	74.8	416.8	75.0	- 0485°
	•35	50.1	75 <u>•</u> 5	• 70	49.9	75.0	416.8	75.3	.037ā
	.27	àú*5	75,8	.26	49.9	75,3	417.4	75.5	.0316
	•22	49.9	75.9	•21	49.7	75.5	477.4	75.7	• 0254
	.15	20.1	76•2	•14	49.9	75.5	418.1	75.9	.0174

il

# TABLE 78 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7-8-76

CLEAN CONDITION - FLOW RATE VERSUS
TEST NUMBER 5G PART G TEST DESCRIPTION DIFFERENTIAL PRESSURE - TEST SPECIMEN
S/N 020 INLET PRESSURE 415 PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS

PRESSURE (PŠŽA)	AVG TEMP (DĒG• F)	ĀVG Flow Rate (TCFM)	GROSS DIFF: PRESS PRIMARY (PSID)	GROSS DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF• PRESS (PSID)	TARE DIFF. PRËSS (PSID)	NEŤ DÍFFS PRESS (PSIO)	
411 <u>.</u> 9	78 <sub>*</sub> 8	•:164	17.686	17.663	17.674	-0.000	<u>17'.674</u>	
410.9	78.6	•0÷61	29,509	29.34z	29.425	•000	<u> </u>	
416.1	78.3	.0329	37,620	37,382	37.501	.000	37.501	
415.5	78+1	•637n	44.159	43.829	43.994	•000	43,994	
414.5	77.7	•0489	59,473	60.786	60.130	•000	60 <u>. 13</u> 0	
413.5	77.4	.0606	7 <del>7</del> .218	78,801	78.010	.000	78.010	_ y
412.9	77 <sub>9</sub> 0	•6717	98,080	98,08ö	98,080	.001	98.080	-
411 <u>•</u> 9	76.7	.0830	118,939	118,939	118.939	.001	116.939	
416.1	73.5	. '951	144,538	144.538	144.53B	•001	144.538	
415 <u>.</u> 5	72,7	.1046	167,610	167.610	167.610	•002	167,610	
415,5	74.0	•î048	167,294	167.294	167.294	•002	167 <u>.</u> 294	
415 <b>.</b> 5	74.3	. 1937	140.746	140.746	140.746	.001	140.746	r
<b>∳15</b> •5	74.6	.0834	118,397	118.307	118.307	•001	<u> </u>	
416.1	74.7	.0720	96.594	97,448	97.o2 <u>1</u>	•001	97.021	
416.Ļ	74.8	•0608	77.591	78.169	77.880	.000	77'+880	
41蕤	75.0	•n485	58,846	59,2r6	59.026	•000	59.026	
416,5	75.3	.ñ372	43.786	43,484	43,635	.000	43, 635	
417.9	75.5	·^316	36,56)	36.232	36.39 <u>6</u>	•000	36,396	J
417.4	75.7	.0254	28,697	28,309	28.503	•000	28 <u>.</u> 503	
418.1	75,9	•0174	19,002	18,691	18.847	•000	18.847	

!ARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM)#42 +

0. (ACFM) \*\*3

# TABLE 78 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 7-8-76

TEST NUMBER 50 PART 6 TEST DESCRIPTION

CLEAN CONDITION - FLOW RATE VERSUS.
DIFFERENTIAL PRESSURE - TEST SPECIMEN
S/N 020 INLET PRESSURE 415 PSIA (NOMINAL).

	****	****	****			ET CONDITION		****	****	******	NET DIFFERENT:	
H	PRESS!		****	TE PERATURE	*****	***	****	FLOW RATE	***	****		· , ,, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
	K₫/ŚĠ CM	PSIA	DEG. K	DEG. c	DEG. F	LITERS/ MIN	"CFM	SCFM	K@∖Hਔ GNS	GNZ LBS/HR	KG/SQ CM DIFFERENTIALI	PSĪĎ
	58.937	411.9	299.1	26.0	78.8	12.2	.0164	•452	<u>.8</u> 90	1.962	1:2426	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
	58*83	410.9	299.0	25.9	78,6	19.9	.0261	.718	1.414	3.117	2.0688	29, 125. "
	29.256	416.1	298.9	25.7	78.3	24.8	.0323	.900	1.772	3.967	2,6366	37.501
1	29.210	415.5	298.8	25.6	78.ì	7•8م	.0370	1.031	2.022	4+474	3.0931	43 794
	29,165	414.5	298,5	25,4	77.7	38.1	.0489	1,361	5•ē8j	5.910	4,2275	60.130
	29.073	413.5	298.4	25,2	77.4	47 <u>•</u> 0	.0606	1.680	3•308	7.293	5,4846	78:010.
	29.028	412.9	298.2	25.0	77.0	55.7	.0717	1,988	3.914	8.630	6.8957	.66.050
	28.937	411.5	298.0	24.8	76.7	64.9	• 0830	2.296	4.521	9,968	8.3622-	11B, 239
	29.256	416.1	296.2	23,1	73.5	75.6	•0951	2.675	5.765	11.611	10.1621"	1447598
1	29.210	415.5	296.3	23.2	73.7	83.1	.1046	2.937	5 <u>•</u> 783	12.749	11.7841	767-270
	29.210	415,5	296.5	23,3	74.0	83.2	•1n48	2.941	5 <u>•</u> 79n	12.766	11.7619	167.294
	29.210	415,5	296.7	23.5	74.3	74.1	,0937	2.628	5 <u>•</u> 175	11.409	9,8954	~140.]4 <u>6</u>
	29.210	415.9	296.8	23,7	74.6	65.8	.0834	2,336	4.500	16.142"	8.3178	118.307
	ž9.256	416.1	296.9	23.7	74.7	56+5	.0721	2.021	3.979	8.772	6.0515	<u>55,-657-</u> _
	29.256	416.1	296.9	2 <b>j</b> .8	74,8	47.7	.0608	1.706	3•325	7.404	5,4755	77.580
ŀ	29.302	416,5	297.ī	23,9	75.0	37.8	• n485	1.362	2.681	5.912	4-1499	29.050
	29.302	41 <u>6.</u> 5	297.2	24.0	75.3	28.9	.0372	1.044	2 <u>•</u> 055	4.531	3.0678	43.035
	29,347	417.4	297.3	24.2	75,5	24.5	.0316	.889	1.750	3,858	2.5589	36,396 ~
	29.347	417.4	297.4	24.3	75.7	19.7	. 1254	.713	1.404	3.096	2.0040	28.503.
	29.393 *****	418 <u>. i</u>	297.5 ****	24•4 ****	75 <b>.</b> 9	13.3	.0174	.489	• <del>9</del> 64	2:124	1.3250	18.047
	29,190	415.6	297.6	24.4	76.0						,	
	•111	155	•8	.8	1.5	DEVIATIONS	5				<u>.</u>	

TABLE 79 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION

PART É

LARE DIFF. PRESS = -3.60000E-04 + -3.31610E-02 (ACFM) + 6.33359E-01 (ACFM) ##2 +

PAGE: 1 DATE: 7-8-76

CLEAN CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE (TEST SPECIMEN S/N 020) INLET PRESSURE 700 PSIA (NOMINAL)

TEST SPECIMEN INLET CONDITIONS

TEST NUMBER F5

PRESSURE (PŠĮA)	AVG TEMP (DĒG• F)	AVG Flow Rate (7cfm)	GROSS DIFF. PRESS PRIMARY (PSID)	GROSS DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS' (PSID)	NET DIFF PRESS (PSID)	 - 
703.9	87.8	,óo93	9,422	9,400	9,411	<b>-0.00</b> ]	9.411	
703 <u>•</u> ¥	87.7	. 5153	16,026	15.855	ī\$.940	-0.001	ĭ5.941	
703.9	87 <u>•</u> 6	.0186	19,909	19.7 g	19.827	-0.001	19.828	
703.9	67.4	.0222	24,219	23.985	24.102	-0.001	24,103	
703.9	e7:1	. 6282	31,351	31.217	31.284	#0.001	31.205	
703.9	66.7	• 0351	40,493	40.210	40.40 <u>1</u>	-0.001	40.402	ij
703 <u>.</u> 9	86.2	.0418	49.797	49,303	49,550	-0.001	49,551	
700.0	85 <b>.</b> 6	.0481	57,331	57 <b>.</b> 520	57 <u>.426</u>	-0.000	57 <b>.</b> 426	
700 <u>•</u> 0	85 <u>•</u> 3	• ñ544	66.602	67.002	66.802	<b>=0.00</b> 0	66.8ō2	
700 <u>.</u> 0	8 <u>5.</u> 0	.0619	78,458	78,695	78,477	.000	Ž8.577	•
700.0	84.5	.0613	77,339	77.747	77,543	<del>-</del> 0.000	77.544	••
700 <u>.</u> 0	84.7	.6542	66,476	67.002	66,739	<b>#0.000</b>	66.740	ij
700 <u>•</u> Ų	84 • 9	.0486	58,083	58,469	58.276	<b>*0.00</b> 0	§8.276	•
700.0	85.3	.0418	49.858	49.303	49.581	-0.001	49.581	
700 <u>.</u> 0	85.8	.0350	40,309	39.906	40.108	#0.001	40,108	
700.0	86.3	• 9585	3i.597	31.217	31.407	-0.001	31,468	•
700.0	86.8	.0220	23.973	23.64 j	23.807	<b>40.001</b>	23.868	
703 <u>.</u> 9	87.4	. 8179	19.231	18.887	19.059	-0.001	19.060	IJ
703 <u>•</u> ₹	87 <u>.</u> 8	.0150	15.902	15.626	15.764	-0.001	15.765	
703.¥	88.4	.ŏo98	10,101	9.800	9.950	-0.001	9,951	

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7-8-76

TEST NUMBER, F5

PART F

TEST DESCRIPTION

CLEAN CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE (TEST SPECIMEN S/N 020) INLET PRESSURE 700 PSIA (NOMINAL)

TESŤ SPECIMEN INLET ČONDÌTIONS FLOWMETER CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*

****	FLOWME]ER ONE		*****	FLOWMETER TWO	***				
FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEG: F)	FLOW RATE (ACFM)	PRESSURE. (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	AVG FLOW RATE (ācfm)	1
•14	49.3	87๋•҈7	•13	49•Ĩ	87.9	7ñ3.9	87.8	.0093	
.23	48.7	87.4	•55	48.3	88.0	703,9	87.7	.0153	
•27	₩å•ð	87.5	. 26	48.5	88.6	7ñ3.9	87.6	• 6186	
•ĝs	<b>47.</b> 3	86,9	•31	48.7	88.0	703.9	87.4	• 0525	
•41	49.3	86.2	.40	48.7	87.9	703.9	87.1	.0282	1
.51	±2.3	85.5	•51	48•3	87.9	703.9	86.7	•0351	u
• 60	42.5	84•8	•60	48.3	87.7	703.9	86.2	. ¢418	
.68	42.5	83.49	•70	47.9	87.3	700.0	85.6	• 0481	
.77	42.1	89.6	•80	ã <b>7.</b> 6	87.0	700.ò	85.7	.0544	
.87	42.7	83 <u>.</u> 2	•91	47.6	86.7	700.0	85.0	•0619	
.87	49.3	85.7	•91	47.2	86.3	700.0	84.5	• ġ6 j 3.	ų
.77	49.1	৪৭•ুণ	•80	47.4	86,4	700.0	84.7	• ō54g	
.69	49.5	83 <u>.</u> 2	•71	47.9	86.5	700.ò	84.9	.0486	
.60	49.5	87.7	.60	∠8 <b>,</b> 5	8 <b>7.</b> 0	700.0	85.3	•04Í8	
•50	42.3	84•2	•50	48.3	A7.4	700.0	85.8	.0350	
•41	49.5	84.4	• <b>4</b> 0	48.9	87.7	700.0	86.3	.0282	
•31	49.9	85•5	• 31	49.5	88.1	700.0	86.8	.0220	
• 56	4¥.5	86•5	.25	49.1	98.6	7n3.9	87.4	.0179	,
• ss	24.5	86.8	•51	50•1	88.8	783.9	87.8	•0150	
.14	49.7	B7•6	.13	49,3	89.2	7n3,9	88.4	.0098	

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 7-8-76

CLEAN CONDITION-FLOW RATE VERSUS DIFFERENTIAL

TFST NUMBER F5 PART F TEST DESCRIPTION PRESSURE (TEST SPECIMEN S/Nº 020) INLET PRESSURE 700 PSIA (NOMINAL)

NET DIFFERENTIAL PRESS TEST SPECIMEN INLET CONDITIONS \*\*\* PRESSURE TEMPERATURE. FLOW RATE \*\*\* \*\*\*\*\* **\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*** LITERS/ GN2 GNS KG/SQ CM KG/SQ CM PSIA SCFM KG/HH DIFFERENTIAL DEG. K DEG\_ C DEG. F MIN ACFM LAS/HR P51D 49.489 703.7 .432 i.877 364.1 31.1 87.8 . 3093 \*825 9.411 11.7 .6617 49.489 703.7 87.7 3.071 15.941 394.1 31.0 19.5 .0150 .707 1:393 1.1508 49,489 703.7 31.9 304.0 87.6 23.9 .0186 .862 1.695 3,743 1.3940 19,628 49,489 703.7 304.0 34.8 87.4 . 1222 1.031 2.,31 4.477 1.6946 28.6 24.103 49.489 703.9 87.1 303.7 30.6 ·0282 1.308 2.570 5.680 2.1995 31.285 36 • 4 49.489 703.7 303.5 86.7 30.4 45,6 .0351 1,629 3.50 2,8405 40.402. 7.071 49,489 703.7 49,551 " 303.3 86.2 54.7 . .418 1.942 3.855 B.432 3.4838 3n.1 49,212 700.0 29.8 85.6 62.7 303.0 .0481 2+225 4.380 9,657 4.0375 57,426 49,212 700.4 302.8 29.6 85.3 71.6 .0544 2.520 4.962 10,939 4.6967 66,802 49.212 700.0 302.6 29.4 85.0 2.868 5.64! 78,577 Bj • 2 619 12:449 5.5245 77.544. 49.212 700.0 29.1 84.5 80.5 .0613 5.59/ 302.3 2.842 ີ 2 - 338 5,4519 49,212 700.v 302.4 29.3 84.7 71.2 .0542 2,512 4.94 10.905 4,6923 66.740 49.212 700.5 302.5 29.4 84.9 . 1486 2,253 4.436 63.6 9.780 4.0972 58,276 49,212 700:0 302.8 85.3 29.6 54.5 . ^418 1.935 3.811 3.4859 49.581 8.401 49,212 700.0 303.0 29.9 85.8 .0356 45.2 1.618 3 782 7.022 2.8199 40.108 49,212 700,0 303.3 30.1 86,3 36.3 .0282 1.304 2,568 5,662 2.2082 31,408 49,212 700.0 303.6 34.4 86.8 28.2 23.808 .0220 1.016 2.001 4.411 1.6738 49.489 703.7 303.9 30.8 87.4 .0179 1.63? 19.060 23.0 .832 3.610 1.3400 49,489 703.7 304.2 87.8 1.317 31.0 19.2 .015n .697 15,765 3.026 1.1084 49.489 703.9 364.5 88.4 .451 31.3 . n 09R <u>•</u>889 j.959 .6996 9.951 12.2 \*\*\* \*\*\* \*\*\* \*\*\* \*\*\*\*

49.350

.138

701.9

2.0

303.4

• 6

30.2

.6

86.4

1.1

DEVIATIONS

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 7-8-76

CLEAN CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE (TEST SPECIMEN S/N'020) INLET PRESSURE 1,000 PSIA (NOMINAL)

TEST NUMBER SE PART # TEST DESCRIPTION

#### ŤESŤ SPECIMEN INLET CONDÍTIONS FLOWMETER CONDITIONS

****	FLOWME LER ONE	***	***	FLOWMETER TWO	****				`
FLOW RATE (ACFM)	PPESSURE (PSIA)	ŤF™P (DFG• F)	FLOW RATE	PRESSURE, (PSI <sub>4</sub> )	TFMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	ĀVĞ FLOW RĀTE (ÃÇFM)	'
<b>,</b> 15	<b>50.4</b>	79+4	.13	50.2	87 <b>.7</b>	976.5	88.6	.0072	
*55	21.0	82.8	.21	50.6	87.8	976.2	88,3	.õlī3	
•27	⊃ <b>4</b>	ฯห• เ	•56	51.2	B <b>7.9</b>	<sup>9</sup> 72.3	88.0	.0138	
•31	5 V . 4	97•4	• ~ l	50+1	87.9	970.3	87.7	.0160	
•41	<b>51.0</b>	85.8	.41	50.2	87.8	972.3	86.8	.ö213	.1
•50	Þv • 1	84.4	.50	49.3	87.4	972.3	85.9	. 6257	"
•59	5v • 1	ลร•ุล	•60	48.9	86.7	972.3	84.7	. ó3ō4-	
•69	48.9	8î•a	.71	48.5	86.1	968.3	83.7	.ñ355	
.77	47°3	79.7	.81	48.3	84.7	968.3	82.2	•0400	
.87	49.5	78•7	•91	47.2	83*b	964.3	81.3	. 0445	
.87	4º 1 • 1	77•7	•91	47.0	87	964.3	80.2	.0444	J
, <b>,</b> 78	45.7	77•8	.81	47.0	82.5	<sup>9</sup> 64.3	80.1	.0392	•
•69	44.5	7#• Ī	•73	48.3	12.5	964.3	80.3	.0352	
•60	44.5	79•≒	+60	48.3	B6	964.7	80.5	. Ö304	
•50	49.9	79•3	•50	48.9	A3.1	964.3	81.2	.ņ258	
.41	>6.5	79.9	•40	49.7	R3.5	964.3	81.7	. 0209	
.31	51.1	8 ñ • 4	•40	49.5	87.9	964.3	82.2	.0157	4
•26	20.1	81•3	. 25	49.9	94.3	964.3	82.8	.ò133	ď
.21	5( ♦%	8ĵ•8 <sup>*</sup>	.51	49.9	84.6	964.3	83.2	.0109	
•14	49.7	Ŗp•5	•13	49+3	84.9	964.3	83.7	.0070	

#### FLOW RATE VEUSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7-8-76

TEST NUMBER SE PART F TEST DESCRIPTION

CLEAN CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE (TEST SPECIMEN S/N 020) INLET PRESSURE 1,000 PSIA (NOMINAL)

# TEST SPECIMEN INLET COMPLITIONS \*\*\*\*\*\*\*\*\*\*

	•							
PRESSURE (PŠIA)	AVG Temp (deg. f)	ÌVG FLOÙ R∆TE (•CFM)	AROSS DIFF. PRESS PRIMARY (PSID)	GR'SS DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF• PRESS (PSID)	NEŤ DIFF• PRESS (PSID)	ı
976.4	88.6	.0072	7,323	7,613	7,468	-0.000	Ť.468	
976.2	HB.3	. 113	11.915	12,236	12.475	-0.000	12.h76	
972.3	<b>₩8</b> •0	.cl 8	14.752	15.150	14.951	<b>~</b> 0.000	14.951	
5،224	87.7	.n16r	17.467	17.838	17.652	-0.000	17.653	
972.3	86.8	., 213	24. 95	24.367	24.23]	-0.000	24.231	
972.3	85.9	.0257	29,990	30.279	30.135	-0.000	30.135	1
972.3	84.7	.0374	36,597	36,95^	36,773	<b>~0.00</b> 0	36,774	
968.3	63.7	.n355	43.73)	44,154	43.943	<b>-0.000</b>	43,943	
968•3	<sup>4</sup> 8•3	• 04 = 0	49.981	5,251	50.116	-0.000	50.116	
964.3	81.3	.0415	56,998	57,520	57.259	+0.000	57.259	
و. 964	80.2	.0444	57_248	57,520	57.384	-0.000	57.385	
964.2	8n+1	S9E.	49.619	49,619	49.619	-0.000	49.619	7
964.3	80:3	Scęn.	43.312	43,750	43.531	-0.000	43.532	
964.3	80.5	.0304	36.357	36,719	36,53 <u>5</u>	-0.000	36,538	
و, 964	91.5	. ·258	36.231	3n.45 <u>1</u>	30.341	<b>-0.000</b>	30.341	
964.3	81.7	• 05/16	27.794	23.9 9	24.82j	-0.000	23 <sub>.</sub> 851	
964.3	82.2	.0157	17.407	17.437	17.422	-0.000	17.422	
964.2	H5+H	. 133	14.451	14.521	14.485	<b>-</b> 0.000	14.486	1
964.3	b3.2	.01:9	11.734	11.722	11.728	<b>+0.00</b> 0	11.728	
964 ي	d3.7	.0070	7,323	7.271	7'.297	-0.000	7,297	

<sup>-!</sup>ARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM) 42 +

TABLE 80

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CLEAN CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE (TEST SPECIMEN S/N,020) INLET

3

7-8-76

PAGE:

TEST NUMBER SE PART F TEST DESCRIPTION PRESSURE 1,000 PSIA (NOMINAL)

NET DIFFERENTIAL PRESS TEST SPECIMEN INLET CONDITIONS \*\*\*\* PRESSURE TEMPER" TURE FLOW RATE \*\*\* \*\*\*\*\*\*\*\*\*\* \*\*\* ſ LITERS/ GNS GNS KG/SQ CM PSIA K@ZHK LRS/HR DIFFERENTIAL PSID KG/SQ CM DEG. K DEG. C DEG. F MIN \CFH SCFM 68.635 976.2 902 .5251 7.468 3.4.6 31.4 88.4 12.4 .4072 .462 2.004 976.2 12.076 .8490 68.635 304.4 , 31.3 88.3 20.1 6113 .728 1.434 3.165. .885 972.4 1.744 14,251 68.357 .0138 1.0512 304.3 31.1 88.0 24.6 3,840 Ĩ7.653 68.357 972.3 34.9 2.020 4,454 1.2411 3.4.1 87,7 28.5 •916n 1.026 68.357 972.5 10.5~ 85.R 78.0 0513 1.366 2469± 5.932 1.7036 24.231 303.6 68.357 و. 972 85.9 9257 1.648 3.240 7.156 2.1187 30.135 303.1 30.0 46.2 972,4 1.954 36.774 68.357 3.2.5 29.3 84.7 55.1 3.847 8.480 2.5854 .1304 68.078 9,898 968,3 43.943 301.9 8.7 83.7 64.6 .0355 80ج. و 4.490 3.0895 968.3 68.078 27.9 5.075 11.188 3,5235 50.116 301.0 82.2 73.3 .0400 2,577 2,859 57,259 67.800 964.5 27.4 . 11445 5.630 12.411 4.0257 300.5 81.3 81.0 \$7.385 67.800 964.3 5.629 299.9 24.8 80.2 81.1 . 1444 2,859 12.411 4.0345 964.3 67,800 299.9 26.7 80.1 77.5 .0392 2,524 4.971 jn.958 1.7444 24.811 67.800 964.5 8.85 84.3 . 352 2.264 4.455 9.828 3.0606 43.532 300.0 64.1 964.3 3,848 36,53B 67.800 80.5 54.9 1.954 8.484 2.5689 300.1 27.0 . 3344 . 1258 67.800 964.5 30,341 300.5 27.3 81.2 45.3 1.656 3.761 7.189 2.1332 67,800 964.5 ~ 23.851 2.641 5.823 1.6769 300.7 27.6 81.7 37.3 .0209 1.341 67.800 964.5 27.9 82.2 . 157 1.975 1.2249 17.422 301.0 27.9 4,360 1.064 67.800 964.3 1.673 1.0185 î4,486 301.4 28.2 82.8 23.5 .0133 .850 3.689 .699 67.800 964.3 11.728 301.6 28.4 83.2 19.3 .0109 1.379 3.034 .8246 67.B00 964.3 3.1.9 2p.7 83.7 12.2 +907A .450 .885 1 952 •5ì3a 7.297 \*\*\* \*\*\* \*\*\* \*\*\*\* \*\*\* 68.050 967,9 301.9 24.7 83.7

**PRINTING** 

2.5

.276

3.7

1 . 4

1.4

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 7/8/76

TEST NUMBER 11A PART A TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS
DIFFERENTIAL PRESSURE, TOTAL OF 4.9 mg OF
SYNTHETIC CONTAMINANT ADDED, TEST SPECIMEN
(S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL)
TEST SPECIMEN INLET CONDITIONS

FLOWMETER CONDITIONS

\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*

***	FLOWMLIER ONE	**	****	FLOWMETER TWO	****			• • •
FLOW RATE (ACFM)	PRESSURE (PSIA)	TEMP (DEA• F)	FLOW RATE (4CFM)	PRESSURE. (PSI4)	TFMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	ĀVĢ Flow Rāte (ĀČPM)
.87	49.9	74•7	.91	47.8	79•1	992.1	76 <b>.</b> 9	•0438
.78	42.9	74.4	.81	48,3	78.8	992.ī	76.6	. 0393
•69	49.7	74•6	•71	48+3	78.8	992.1	76.7	. ó345
•60	50.1	7 •9	•61	"8 <sub>•</sub> 9	78.9	992.1	76 <b>.</b> 9	.ogòl
.50	50.1	75.6	.50	49.3	79.4	992.₹	77 <b>.</b> 5	.0252
.41	<del>1</del> 9.5	7 +2	.40	48.9	79 <b>•7</b>	992.1	₹ <b>8</b> •Ô	.0200
•31	49.9	77:1	.31	49,3	88.4	792.1	78.7	. 0155
•27	<del>1</del> 9.9	77 <u>.</u> 8	• 56	49.3	8 •9	992.1	79.3	.ò13ī
•22	49.9	78•7	.51	49.5	91.3	992.1	80.0	.0106
.14	49.5	79.4	•13	49,3	81.7	7.598	8ñ.5	.0067
<u>•</u> 14	49.7	8 • 5	• j 3	49.3	ž.3	992.1	81.4	•0067
•23	42.3	8ក្+4	•22	48.9	82.5	992.1	81.4	.0110
•26	<u>49.9</u>	8 ° • 2	.25	49.5	82.5	992.1	81.4	.0136
.32	49.9	8ñ•0	.41	49.3	85.6	992.1	81.3	.õ157
•41	49.9	79.2	.41	49.3	R₽.5	992.1	8ñ.9	+ò2ŏ4-
.51	÷9.7	78 <u>•</u> 4	•51	48.7	82•1	992.1	8ñ.3	.õ251
.60	49.9	77÷6	•60	78.7	8i.6	995.1	79.6	• 0298
•69	42.5	75.8	.70	48.3	81.1	992•1	78.9	. ñ343
.78	49,5	75 • 9	•81	47.8	85.2	992 • <u>1</u>	78.ó	, ñ388
.87	50,1	75+2	.91	47.9	79.6	992.1	77.4	. 0439

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7/8/76

CONTAMINATED CONDITION-FLOW RATE VERSUS

DIFFERENTIAL PRESSURE, TOTAL OF 4.9 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL) TEST NUMBER 11A PART Á TEST DESCRIPTION

# TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*

• •	• •						
PRESSURE (PSIA)	(DĚG• F) Jemp Avg	AVG FLOW RATE (7CFM)	GROSS DIFF• PRESS PRIMARY (PSID)	GROSS DIFF. PRESS SECONDARY (PSIn)	AVG GROSS DIFF• PRESS (PSID)	TARE DIFF. PRESS (PSID)	NEŤ Ó DÍFF• PRESS (PSID)
992.1	76.9	.0438	56_858	57,449	57,153	-0.000	57, 153
992.1	76.6	. \393	49.599	51.189	49.894	-0.000	49.894
992.1	76•7	•0345	43,586	43.253	43.420	-0.000	43 • 42 Ó
1,566	76 <b>.</b> 9	.0301	37,179	36,922	37.050	-0.000	37.051
335 <b>-</b> 1	77.5	. <252	31.262	29,973	30.117	-0.000	30.118
992.1	78.0	.0200	23,333	23,339	23.186	-0.000	23.186
992 <b>.</b> †	78.7	<u>.</u> 0155	17.581	17.320	17.450	-0.000	Ĭ7.4Š0
992.1	79.3	.n131	14.576	14,477	14,492	-0.000	14,492
995•1	80.0	.01^6	11.569	11.384	11.476	-0.000	11.477
992.1	80.5	.0067	7.11,7	6.996	7.0=6	-0.000	7.057
992.1	81.4	.0067	6,991	6,996	6.994	-0.000	6,994
992.1	81.4	.0110	11,820	11.840	11.830	-0.000	ĭ1.830
992•1	81.4	.0130	14,200	14.2 6	14.218	-0.000	14.218
992.1	81.3	.0157	17.643	17,663	17.653	-0.000	Ĩ7.653
995 <sup>€</sup> Î	80.9	.0204	23.52/	23,497	23.509	-0.000	23.509
335°†	80.3	.0251	29,950	29.8=8	29.904	<b>~0.000</b> ,	29.904
992.1	79.6	.n298	36,432	36,290	36.361	-0.000	36,36i
992.ļ	78.9	. 343	42.964	42.792	42.878	<b>~0.000</b>	42.879
992.1	78.0	•0388	48.971	49.557	49.265	-0.000	49.266
992,1	77.4	.0439	56,983	57,449	57.216	-0.000	57,216

PAGE: 3 DATE: 7/8/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 11A PART A

T A TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 4.9 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL)

	***	***	*****	TEST S		ET CONDITION		***	****	****	NET DIFFERENTI	IL PRESS	
;	PRESSU	RE	****	TEMPER TURE	****	****	****	FLOW RATE	***	****			
	KĢ/ŞQ CM	PSIA	DEG. K	DEG. C	DEG. F	LITERS/ MIN	» CFM	SCFM	ĸē\HŘ eus	GNZ LBS/HR	ĶG/SQ CM Differentiāl:	PSAD	ı
	69.750	992.1	298 • 1	24.9	76.9	82.8	438	2.917	5•744	12.661	E870.4	97°, 153	
	69,750	885°Í	298.0	24.8	76.6	74.6	.0393	2.621	5:161	11.378	3.5079	49.894	
	69.750	992,1	298.0	24.8	76,7	65.1	0345	2,301	4.530	9.988	3.0527	05 <u>+</u> .E¥	
	69.750	992.1	298.1	25.0	76.9	56.4	.0301	2.005	3.945	8.703	2.6049	37,051	•
	69,750	885°∓	298.4	25.3	77.5	47.0	• 4525	1,677	3,302	7.280	2.1175	30.118	.F
	69.750	992,1	298,7	25.5	78.0	37.0	.0200	1,333	2,624	5,786	1.6361	23.186	น
	69.750	992.1	299.1	26.	78.7	28.6	•0155	1.029	2,027	4.468	1.2269	ĭÝ-\$50	
	69.750	992.1	299.5	26.7	79.3	24.1	.0121	.868	1.710	3∙770	1.0189	14,492	
	69.750	992.1	299.8	26.7	80.0	19.5	.0106	.703	1.385	3•054	.8069	11.277	
	69.750	992.1	300.1	27.0	80.5	12.1	•0067	.443	.872	1.922	•496Ī	7', 057'	
	69.750	992,1	300.6	27 <b>.</b> 5	81.4	11.9	.0067	.449	.86/	1.910	.4917	6.994	11
	69.750	995°Í	300.6	27,5	81.4	2ñ•0	.911n	.724	1.429	3.143	.8317	ĭ1.530	U
	69.750	992.1	300.6	27.4	81.4	23.7	.013%	.856	1.685	3+714	.9997	14.218	
	69.750	áa5•1	300.6	27.4	81.3	28.9	• 1157	1.038	2-045	4.508	1.2411	17.653	
	69,750	992,1	300.3	27.1	80.9	37.7	.0204	1,350	2.659	5.861	1.6528	23.509	
	69.750	992.1	300.0	26.8	80.3	46.7	.1251	1.664	j₌27 <u>5</u>	7.223	2.1025	29,904	
	69.750	1.566	299.6	26.4	79.6	55.6	. 298	1,976	3,891	8+577	2.5564	36,361	4
	69.750	885°†	299•2	26.1	78.9	64.5	.0343	2.276	4 <u>•</u> 48 ļ	9.878	3.0147	42.279	,
	69,750	992.1	298,7	25,6	78.0	73.0	.0388	2,577	5.075	īi.188	3,4637	49.266	•
	69.750 ****	992.1	298.4	25.2 *****	77.4	83+0	•0439	2.925	5.760	ĩ2•699	4.0227	57°576	
	69.750	992.1	299.3	26.2	79.1								
	0	• ñ -	.8	• <del>\$</del>	1.5	DEVIATION	s						

(ACFM) (PSIA) (DEG. F) (ACFM) (PSIA) (DEG. F) (PSIA) (DEG. F) (ACFM) (ACFM) (PSIA) (DEG. F) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (ACFM) (	,			11E PART B		TEST DESCRIPTIO	CONTAMINATED CONDI DIFFERENTIAL PRESS SYNTHETIC CONTAMIN (S/N 020) INLET PR	SURE, TOTAL OF SANT ADDED. T SESSURE 415 PS	4.9 mg OF EST SPECIME IA (NOMINAL
######################################	** <del>*</del> *****	******	**************************************	**** <del>*</del> ********	******	*****			
FLOW RATE   PRESSURE   TEMP   FLOW RATE   PRESSURE   TEMP   PRESSURE   TEMP   FLOW RATE   (PSIA)   (DES. F)   (DES. F)   (DES. F)   FLOW RATE   (ACFM)   (PSIA)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (DES. F)   (	******			*******	FLOWMETER TWO	*****			
.78         49.9         73.0         81         48.5         .75.7         417.4         74.7         .0937           .69         49.9         73.7         .71         .48.5         75.5         816.8         74.6         .0827           .50         49.9         73.4         .60         .48.7         .75.3         416.1         .74.3         .0713           .50         .50.1         .73.4         .50         .49.3         .75.3         416.1         .74.3         .1060           .41         .50.1         .73.6         .40         .49.3         .75.3         .415.5         .74.4         .1048           .31         .49.9         .73.6         .30         .49.5         .75.3         .415.5         .74.4         .1048           .31         .49.9         .73.6         .30         .49.3         .75.3         .415.5         .74.4         .1056           .32         .49.9         .73.6         .30         .49.3         .75.3         .415.5         .74.5         .4056           .32         .50.1         .73.7         .25         .49.9         .75.3         .415.5         .74.5         .4051           .15         .49.9				FLOW RATE	PRESSURE,	TEMP		TEMP	FLOW RATE
.69	.88	49.5	74.3	91	47.6	76.1	418.7	75•2	•1035
ABU         49.9         73.4         60         48.7         75.3         416.1         74.3         10713           LSU         50.1         73.4         50         49.3         75.3         416.1         74.3         10601           L41         50.1         73.6         40         49.3         75.3         415.5         74.4         10888           L31         49.9         73.6         30         49.3         75.3         415.5         74.4         10368           L31         49.9         73.6         30         49.3         75.3         415.5         74.4         10368           L32         49.9         73.6         30         49.3         75.3         415.5         74.4         10367           L22         50.1         73.7         25         49.9         75.3         415.5         74.5         10311           L22         50.1         73.8         121         49.9         75.3         415.5         74.5         10254           L15         49.9         73.9         14         49.9         75.3         416.1         74.6         10170           L15         49.5         74.4         14	70	42.9	73.8.	•81	48•3	.75.7	417.4	74.7	.0937
150         50.1         73.4         .50         49.3         75.3         416.1         74.3         .0601           241         50.1         73.6         .40         .49.3         75.3         415.5         74.4         .0368           331         49.9         73.6         .30         49.3         75.3         415.5         74.4         .0368           -29         50.1         73.7         .25         49.9         75.3         415.5         74.5         .6311           -22         50.1         73.8         .21         49.9         75.3         415.5         74.5         .0254           -15         49.9         73.9         .14         49.9         75.3         416.1         74.6         .0170           -12         49.5         74.4         .14         49.9         75.3         416.1         74.6         .0170           -12         49.5         74.4         .14         49.9         75.3         416.1         74.6         .0170           -12         49.5         74.4         .14         49.1         75.7         416.1         74.7         .0259           -27         49.9         73.9         .26<	69	49.9	, 73.7	•71		75.5	416.8	74.6	-0827
41       50.1       73.6       .40       49.3       75.3       415.5       74.4       .0468         31       49.9       73.6       .30       49.3       75.3       415.5       74.4       .0368         .31       49.9       73.6       .30       49.3       75.3       415.5       74.4       .0367         .22       50.1       73.7       .25       49.9       75.3       415.5       74.5       .0254         .15       49.9       73.9       .14       49.9       75.3       416.1       74.6       .0170         .12       49.5       74.4       .14       49.1       75.7       416.1       74.6       .0170         .12       49.5       74.4       .14       49.1       75.7       416.1       74.6       .0170         .12       49.5       74.4       .14       49.1       75.7       416.1       74.6       .0168         .22       49.5       74.4       .14       49.3       75.2       416.1       74.7       £.0259         .27       49.9       73.9       .26       49.5       75.2       416.1       74.5       .0315         .32       50.1 <td><u></u></td> <td>49,9</td> <td> 73.4</td> <td>. •60</td> <td> 48*7</td> <td>75.3</td> <td>416-1</td> <td>74.3</td> <td>.0713</td>	<u></u>	49,9	73.4	. •60	48*7	75.3	416-1	74.3	.0713
31       49.9       73.6       ,30       49.5       75.3       415.5       74.4       ,0368         -31       49.9       73.6       .30       49.3       75.3       415.5       74.4       .0367         -29       50.1       73.7       .25       49.9       75.3       415.5       74.5       .6311         -22       50.1       73.8       .21       49.9       75.3       415.5       74.5       .0254         .15       49.9       73.9       .14       49.9       75.3       416.1       74.6       .0170         .15       49.5       74.4       .14       49.9       75.7       416.1       74.6       .0170         .15       49.5       74.4       .14       49.9       75.7       416.1       74.6       .0170         .12       49.5       74.4       .14       49.9       75.7       416.1       74.7       .0259         .27       49.9       73.9       .26       49.5       75.2       416.1       74.5       .0315         .32       50.1       73.8       .31       49.7       75.2       415.5       74.4       .0889         .51       50.1 <td><u>.5</u>0,</td> <td> 50.1</td> <td>73•4</td> <td>•50</td> <td>. 49•3</td> <td>75.3</td> <td>416.1</td> <td>74.3</td> <td>.0601</td>	<u>.5</u> 0,	50.1	73•4	•50	. 49•3	75.3	416.1	74.3	.0601
.31       49.9       73.6       .30       49.3       75.3       415.5       78.4       .0367         .69       50.1       73.7       .25       49.9       75.3       415.5       74.5       .0311         .22       .50.1       73.8       .21       49.9       75.3       415.5       74.5       .0254         .15       .49.9       73.9       .14       49.9       75.3       416.1       74.6       .0170         .12       .49.5       .74.4       .14       49.1       .75.7       .416.1       .75.0       .0168         .22       .49.5       .74.1       .21       .49.3       .75.3       .416.1       .74.7       .0259         .27       .49.9       .73.9       .26       .49.5       .75.2       .416.1       .74.5       .0315         .32       .50.1       .73.8       .31       .49.7       .75.2       .415.5       .74.5       .0379         .41       .49.9       .73.7       .91       .49.3       .75.2       .415.5       .74.4       .0489         .51       .50.1       .73.6       .50       .49.3       .75.2       .415.5       .74.4       .0604 <tr< td=""><td>_ 41</td><td> 50.1 .</td><td> 73:6</td><td>-4.0 .</td><td>49.3</td><td>75.3</td><td>415.5</td><td>74.4</td><td>-0484</td></tr<>	_ 41	50.1 .	73:6	-4.0 .	49.3	75.3	415.5	74.4	-0484
.89       50.1       73.7       .25       49.9       75.3       415.5       74.5       .0311         .22       .50.1       .73.8       .21       49.9       .75.3       415.5       74.5       .0254         .15       .49.9       .73.9       .14       49.9       .75.3       416.1       .74.6       .0170         .12       .49.5       .74.4       .14       .49.1       .75.7       .416.1       .74.6       .0170         .22       .49.5       .74.4       .14       .49.1       .75.7       .416.1       .74.7       .5.0259         .27       .49.9       .73.9       .26       .49.5       .75.2       .416.1       .74.5       .0315         .32       .50.1       .73.8       .31       .49.7       .75.2       .415.5       .74.5       .0379         .41       .49.9       .73.7       .41       .49.3       .75.2       .415.5       .74.4       .0489         .51       .50.1       .73.6       .50       .49.3       .75.2       .415.5       .74.4       .0604         .60       .49.9       .73.6       .61       .48.7       .75.0       .413.5       .74.4       .0719	.31	<u> 49,9</u>			49.5	75.3	415.5	74.4	0368_
.22 50.1 73.8 .21 49.9 75.3 415.5 74.5 .0254 .15 49.9 75.9 .14 49.9 75.3 416.1 74.6 .0170 .15 49.5 74.4 .14 49.1 75.7 416.1 75.0 .0168 .22 49.5 74.1 .21 49.3 75.3 416.1 74.7 \$ .0259 .27 49.9 73.9 .26 49.5 75.2 416.1 74.5 .0315 .32 50.1 73.8 .31 49.7 75.2 415.5 74.5 .0379 .41 49.9 73.7 .41 49.3 75.2 415.5 74.4 .0489 .51 50.1 73.6 .50 49.3 75.2 415.5 74.4 .0489 .51 50.1 73.6 .50 49.3 75.2 415.5 74.4 .0604 .60 49.9 73.6 .50 49.3 75.2 415.5 74.4 .0609	31	49.9	73+6	•30	49.3	75.3	415.5	74-4	
.15.       49.9       73.9       .14       49.9       75.3       416.1       74.6       .0170         .12.       49.5       74.4       .14       49.1       75.7       416.1       75.0       .0168         .22.       49.5       74.1       .21       49.3       75.3       416.1       74.7       .0259         .27       49.9       73.9       .26       49.5       75.2       416.1       74.5       .0315         .32       50.1       73.8       .31       49.7       75.2       415.5       74.5       .0379         .41       49.9       73.7       .41       49.3       75.2       415.5       74.4       .0489         .51       .50.1       .73.6       .50       49.3       .75.2       415.5       74.4       .0604         .60       49.9       .73.6       .61       48.7       .75.2       414.2       .74.4       .0719         .69       49.7       .73.6       .61       48.7       .75.0       413.5       .74.3       .0830	- ∙ <u>₹</u> ō	50.1	73•7	•25 _	49.9	75.3	415.5	74.5	0311_
•15       49.5       74.4       •14       49.1       75.7       416.1       75.0       •0168         •22       49.5       74.1       •21       49.3       75.3       416.1       74.7       \$.0259         •27       49.9       73.9       •26       49.5       75.2       416.1       74.5       •0315         •32       50.1       73.8       •31       49.7       75.2       415.5       74.5       •0379         •41       49.9       73.7       •41       49.3       75.2       415.5       74.4       •0489         •51       50.1       73.6       •50       49.3       75.2       415.5       74.4       •0604         •60       49.9       73.6       •61       48.7       75.2       414.2       74.4       •0719         •69       49.7       73.6       •61       48.7       75.0       413.5       74.3       •0830	22	50.1.	73.8	21	49.9	75.3	415.5	74.5	.0254
.22       49.5       74.1       .21       49.3       75.3       416.1       74.7       \$ .0259         .27       49.9       73.9       .26       49.5       75.2       416.1       74.5       .0315         .32       50.1       73.8       .31       49.7       75.2       415.5       74.5       .0379         .41       49.9       73.7       .41       49.3       75.2       415.5       74.4       .0489         .51       .50.1       73.6       .50       49.3       75.2       415.5       74.4       .0604         .60       49.9       73.6       .61       48.7       75.2       414.2       74.4       .0719         .69       49.7       73.6       .71       48.3       75.0       413.5       74.3       .0830	<u>.</u> 15.	49.9	73•9		49:9	75.3	416-1	74.6	•0170
	• <u>15</u> .	49.5	74•4	. •14	49:1	75.7	41 <u>6•1</u>	75.0	•0168
.32     50.1     73.8     .31     49.7     75.2     415.5     74.5     .0379       .41     49.9     73.7     .41     49.3     75.2     415.5     74.4     .0489       .51     .50.1     .73.6     .50     49.3     75.2     415.5     74.4     .0604       .60     49.9     .73.6     .61     48.7     75.2     414.2     74.4     .0719       .69     49.7     .73.6     .71     48.3     75.0     413.5     74.3     .0830	2걸	49.5	74:1	•21	49.3	75.3	416.1	74.7	£ •0259
.41     49.9     73.7     .41     49.3     75.2     415.5     74.4     .0489       .51     .50.1     .73.6     .50     49.3     .75.2     415.5     .74.4     .0604       .60     .49.9     .73.6     .61     .48.7     .75.2     .414.2     .74.4     .0719       .69     .49.7     .73.6     .71     .48.3     .75.0     .413.5     .74.3     .0830		49.9	73•9 .	•26	_ 49•5 _	<u> 75.2</u>	416.1	74.5	.0315
.51     .50.1     .73.6     .50     49.3     .75.2     415.5     .74.4     .0604       .60     49.9     .73.6     .61     48.7     .75.2     414.2     .74.4     .0719       .69     49.7     .73.6     .71     48.3     .75.0     413.5     .74.3     .0830	_ ,32	. 50.1	73•8	+31	. 49•7		415.5	74.5	- 0379
.60 49.9 73.6 .61 48.7 75.2 414.2 74.4 .0719 .69 49.7 73.6 .71 48.3 75.0 413.5 74.3 .0830	.41	49.9	<u>73•7</u>	: 41	49•3	75•2	415.5	74.4	•0489
69 49.7. 73.6 •71 48.3 75.0 413.5 74.3 •0830		50 <b>_1</b> _	. 73.6	•50	49•3 <u> </u>		415.5	74.4	•0604
7,000		* *	.73 <u>•</u> 6	•61		75.2	414.2	74.4	•0719
<u>.78 49.5 73.7 81 47.9 75.0 412.9 74.4 .0938</u>			73•6	•.71				74.3	•0830
	<u>7</u> ë	49.5	73•7	•81	47.9	75.0	412.9	74.4	• 0938

	## I			FLOW RATE VERSUS DI	PEEDENITAL PRESCI	PAGE: 3 URE DATE: 7/8/3	76	•	
·			a4	FLOW RATE VERSUS DI	FFERENITAL FRESS			,	
		-	EST_NUMBER 118	PART_B	TEST DESCRI	CONTAMINATE  PTION DIFFERENTIAL	D CONDITION-FLOW F L PRESSURE, TOTAL (	RATE VERSUS OF 4.9 mg OF	
						SYNTHETIC CO	ONTAMINANT ADDED.	TEST SPECIME	
• .		ECIMEN INLET CON		<b></b>		(S/N_UZU)_LI	KLET PRESSURE 413	PSIA (GIMINAI	·/
•	** <u>**********</u>	<u>****</u> *****	************						
<b>U</b> -		AVG	AVG	DIFF• PRESS	GROSS DIFF. PRESS	AVG GROSS	TARE	NET	<del></del> ;-
	PRESSURE	TEMP	ELOW RATE	PRIMARY	SECONDARY	DIFF. PRESS	DIFF. PRESS	DIFF. PRES	
	(PSIA)	(DEG. F)	(ACFM)	(PSID)	(PSID)	(PSID)	(PSID)	(PSID)	¥
	418.7	75.2	•1035	168.453	168-453	168.453	•002	168.451	•
•	417.4	74.7	.0937	143.169	143.169	143.169	•001	143.167	
	416.8	74.6	.0827	119.465	119.465	119.465	.001	119.464	
	416.1	74.3	•0713	97.974	97.974	97.974	•001	97.973	
4	416•1	74.3	.0601	77.882	78.695	78.289	•000	78.287	L
***	415.5	74.4	0484	59.520	60 • 049	59.784	•000	59.783	P
	415.5	74.4	.0368	-0.001	•000	· -0.000	•000	-0.002	<u>\$</u> -
	415.5	74.4	.0367	44.043	43.788	43.916	•000	43.914	
• • • •	415.5	74.5	.0311	36.172	35.894	36.033	•000	36.032	
	415.5	74.5	.0254	28+969	28.594	28.781	•000	28.780	ı
,1	416.1	74.6	.0170	18.699	18.448	18.574	•000	18.572	<del>'</del> -
	416-1	75.0	.0168	18.201	18.162	18.181	•000	18.180	<del></del>
	416.1	74.7	.0259	29.404	29.225	29.315	•000	29.313	
- "	416.1	74.5	.0315	36.793	36.527	36.660	•000	36.658	· ,
	415.5	74•5	•0379	45.405	45.058	45.232	•000	45.230	,
_	415.5	74•4	.0489	60.021	60.681	60.351	•000	60.349	
H	415.5	74.4	.0604	78.006	78.695	78.351	•000	78.349	
,	414.2	74.4	.0719	98.922	98+922	98.922	•001	98.921	1
	413.5	74.3	.0830	120.414	120.414	120.414	•001	120.412	ो
	412.9	74.4	•0938 <sup>~</sup>	143.801	143.801	143.801	•001	143.799	1,
	~			•	A	MANUAL B. A. SCHOOL SEC. 1884			
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	* 184 * *				**** ***			······································	

en a essoure			TABLE 8: FLOW RATE VERSUS DI	2 IFFERENTIAL PRESSU	PAGE: 4 DATE: 7/8/7	6	
		ST NUMBER 118	PART_B	. TEST_DESCRIE	CONTAMINATED DIFFERENTIAL SYNTHETIC CO (S/N 020) IN	CONDITION-FLOW R PRESSURE. TOTAL C NIAMINANT ADDED. LET PRESSURE 415	ATE VERSUS F 4.9 mg OF TEST SPECIMEN PSIA (NOMINAL)
TEST SPE *********	CIMFN INLET COND	[TIONS *******	4 1 4 4 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7				
			GROSS	GROSS			ì
PRESSURE	AVG TEMP (DEG• F)	AVG <u>Flow Rate</u> (ACFM)	DIFF. PRESS PRIMARY (PSID)	DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF• PRESS (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)
412.9	74.3	•1055	173-509	173-509	173.509	•002	173.508
							ì
	TARE DIFF. PRESS	5 = -3.40000E-0	5 + -4.44000E-04 (A	ACFM) + 1.50933E-	01 (ACFM)**2 +	0 (ACFM)	**3
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TABLE 82.
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 5

DATE:

<del>-7/8/76</del>

CONTAMINATED CONDITION-FLOW-RATE-VERSUS DIFFERNTIAL PRESSURE TOTAL OF 4.9 mg. OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL) TEST NUMBER 11B \_ PART, B TEST\_DESCRIPTION TEST SPECIMEN INLET CONDITIONS NET DIFFERENTIAL PR PRESSURE ....TEMPERATURE FLOW RATE \*\*\*\*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\*\*\*\*\*\*\* KG/SQ CM GN2 LITERS/ GN2 PSID DIFFERENTIAL KG/SQ\_CM PSIA DEG. K DEG. C DEG. F \_\_\_\_MIN \_\_\_ACEM SCFM KG/HR LBS/HR 29.438 418.7 297.2 75.2 82.7 .1035 2.920 5.750 11.8433 168.451 24.0 12.676 29,397 143.167 417.4 296.9 23.7 74.7 . ..... .74.7 .\_\_.0937\_\_\_ 2.636 5.190 11.442 10.0657 119.464 29.302 . 416.8 296.8 23.7 74.6 \_ .65.6 .0827.....2.324 4.577 10.090 8.3991 29.226 416.1 296.7 23,5 . .56.1 .. \_.0713 ... 3.940 8.686 6.8882 97.973. 74.3 2.001 29.256 416.1 296.7 1.687 3.322 7 - 324 5.5041 78.287 23.5 59.783 296.7 23.6 2.673 5-893 4-2031 43.914 29,210 415,5 74.4 28.6 0367 1.029 2.026 4.468 296.7 \_\_\_23.6 3.0875 29.210 24.2 .0311 .872 36,032 415.5 296.8 23.6 1.716 3.784 2.5333 \_\_19.7 \_\_\_\_.0254 \_\_\_.712 296.8 1.402 3.090 2.0234 28.780 . 29-210 \_\_\_415.5 ... 23.6 \_.478 18.572 29.256 416.1 296.8 .. 23.7 13.0 .....0170..... . . . 941 \_ \_\_\_ 2 • 075 1.3057 18.180 29.256 416 • 1 297.1 23.9 75.0 12.8 .0168 .472 •930 2•050 1.2782 29,256\_ 416.1 296.9 23.7 74.7 20.1 .0259 .726 1.430 3 - 152 29.313 2.0609 36:658 29.256 416 • 1 296.8 23.6 24,5 74.5 .0315 .884 3.836 2.5773 1.063 29.210 415.5 296.8 45.230° 23.6 74.5 29.7 .0379 2.094 4.616 3.1800 60.349 29.210 415.5 296.7 23.6 74.4 38.2 .0489 1.369 2.696 5.944 4.2430 78.349 29.210 ....415.5 296.7 3.55 74.4 47.4 .0604 1.693 3.333 7 • 348 5.5085 98.921 29,119 414.2 296.7 23.6 74.4 56.5 .0719 2.009 . 3 957 8.723 6.9548 29.073 413.5 296.7 23.5 74.3 65.4 .0830 2.317 4.562 10.057 8.4658 120.421 29.028 412.9 296.7 23.5 74.4 73.9 .0938\_\_\_\_ 2.614 143.799 5-148 11.349 10-1101

} 			<u></u>	ST NUMBER 11	B <u>P</u> ART I	3	TEST DE	SCRIPTION	DIFFERENTI	AL PRESSURE	N-FLOW RATE VERS TOTAL OF 4.9 mg ADDED. TEST SE URE 415 PSIA (NO	TO S
·				TEST S	PEČÍMEN INL	T CONDITIONS					NET DIFFERENT	IAL
	***********		**** <del>*</del> ** <u>*</u> *			* <u>****</u> ****	*********	*****	******	*****	******	***
l <del>}</del>	PRESSUR	3E		<u>TEMPERATURE</u> *********				FLOW RATE				
-	******		*****	**************************************	**************************************		******	***	*****			
	ĸē∖zō cw	PSIA	DEG. K	DEG. C	DEG. F	LITERS/ MIN	ACEM	SCFM	GN2 KG/HR	GN2 LBS/HR	KG/SQ CM DIFFERENTIAL	
	29.028 ****	412•9 *****	296.6 ****	23.5 *****	<u>74.3</u> *****	83.0	1055	2.939	5•788	12.760	12.1988	17
•	29.217	415.6	296.8	23.6	74.5		-					
Ð	.064	9	.1	•1	.2	DEVIATIONS					· · · · · · · · · · · · · · · · · · ·	
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	x <b>DELIVERATE SEE</b> -PPF		•		,	<del></del>						
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	Million on the same shadowsky to be			_								
	* * * *										,,	
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Q- 												

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 7/8/76

TEST NUMBER 110

PART C

TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE TOTAL OF 11.3 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET ERESSURE 1000PSTA (SOMINALIONS

FLOWMETER CONDITIONS

\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*

FLOWNLIER ONE			****	FLOWMETER TWO	***			440	
FLOW RATE	PRESSURE (PSIA)	TFMP (DEG: F)	FLOW RATE (ACFM)	PRESSURE. (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	AVG FLOW RATE (ACFM)	
.86	42.7	75.7	•91	47.6	78+7	1004.0	75.7	.0428	
.78	4¥.4	71.9	•81	49.1	77.7	1 04.0	74.8	• 0389	
•69	20.1	, 7ì•7	•71	48.7	77.	1.04.0	74.4	,0343	
.60	49.9	71.9	•61	48.7	77.3	1004.0	74.6	.0298	
.50	51.1	72.2	•5u	4 <sup>9</sup> • 1	77•3	1600.0	74.8	.0250	,
•41	56.2	73•4	•41	49.5	77.7	100.0	75.3	.0204	
•31	ņ <sub>z</sub> 1	79.7	. Ţ0	49.5	78.2	1000.0	75.9	.0153	
• 26	77.9	74.2	.26	49.7	78.4	1400 • n	76.3	.0130	
•22	47.5	75•	.21	49.1	78.8	1.00.0	76.9	.0105	
,15	47.5	76•1	.14	49.7	79.6	1 04.0	77.9	.0070	
•15	24.S	77.8	•14	49.9	60.7	1004.0	79.2	.0070	
.23	45.3 -	77•A	• 22	47.9	8 .9	1.04.0	79.4	.0107	
.26	47.5	78 • 0	.26	49,1	B1+1	1 04.7	79.6	, 0128	
.32	49.9	77•9	•31	49.3	1.1	1 04.0	79.5	.0155	
.41	47.5	77 • 6	.40	48.9	91.1	1 04.0	79.3	.0199	
<b>.</b> 50	# <b>½</b> .9	76-8	, •50	49.1	Bn•6	1.04.0	78.7	.024B	
.60	2(.1	75.8	•60	49.1	90 • t	1"00.0	77.9	.0297	,
.69	÷₹•5	74.7	.71	48.7	79.7	1000.0	76.9	.0342	
.78	āà"a	74.0	.81	48.3	78.7	1000.0	76.3	.0388	
.87	47.7	72:4	.91	47.6	78.t	1000.0	75.7	.0433	

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7/8/76

TEST NUMBER 110 PART C TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 11.3 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000PSIA (NOMINAL)

- 格拉拉拉特拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉拉	ŢĿST	PECTMEN	INLET	CONDITIONS

PRESSUKE (PSIA)	AVG lemp (DEG• F)	nVG Flow Rate (acfm)	AROSS DIFF• PRESS PRĪMARY (PSID)	GROSS DIFF. PRESS SECOMDARY (PSIn)	AVG GRUSE DIFF PREES (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF• PRESS (PSID)
1004.0	15.7	.0428	55,940	56,817	56 <b>•</b> 379	<b>*0.000</b>	56,379
1004.0	14.8	389	49,683	50,544	50.094	-0.000	50+094
1004.9	14.4	• r 3 <u>4</u> 3	43.99	47.599	43.754	-0.000	43.754
1004.0	14.6	£4298	37.274	36,92	37.098	-0.000	37.098
1000.0	14.8	. n250	30,32	29,973	30.145	-0.000	30.147
1000.0	(5∙≋	.0274	23,971	22.611	23.791	-0.000	23.791
1000-0	75.9	.9153	17,425	17,2 6	17.315	-0.000	17,316
1000.0	16.3	,0130	14.52	14,243	14.405	-0.000	14.407
1000.0	(6.9	.01'5	11.488	11,27,	11.379	<b>~</b> 0.000	11.379
1004.0	17.9	,0570	7.463	7.438	7.400	-0.000	7.400
1004.0	19.2	.0070	7,463	7.451	7.457	<b>→0.000</b>	7.457
1004.4	19.4	.01 7	11.674	11.726	11.700	-0.000	11.700
1004.0	19.6	·r128	14.272	14.293	14.283	≈0.000	14.283
1004.9	19.5	.0155	17.611	17.616	17,6r <u>ë</u>	⇒0 • 0 0 0	17.608
1004.0	79.3	• • 1 9 9	23,294	23.26я	23.280	-0.000	23.280
1004.4	18.7	. (.248	29,951	87.8.85	29.904	-0.000	29,905
1000.9	17+9	.6297	36,844	36.75r	36.797	-0.000	36.797
1000.5	16.9	,, 342	43,54)	43,426	43.482	-0.000	43.484
1000.y	(6•3	*"388	49.433	5 .189	49.811	-0.000	49.811
1000 • 6	/5.7	.^433	56,942	57,764	57 . 35 .	-0.000	57,353

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION

PAGE: 3 DATE: 7/8/76

5,141

5-744

11.334

12-664

49.511

57.353

3,5021

4.0323

TEST NUMBER 110 PART C

70.307

70.307

70.461

•138

\*\*\*

1000.0

1000.0

1005.4

6.1

\*\*\*

297.B

297.4

化存存存存

208.1

• 9

24.6

24.3

25.4

• 9

化化化物

76,3

75.7

77,0

1.6

\*\*\*

74.1

82.6

DEVIATIONS

. u388

.0433

2.611

2.917

TEST SPECIMEN INLET CONDITIONS

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 11.3 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL)

NET DIFFERENTIAL PRESS \*\*\* \*\*\*\*\* PRESSURE IEMPER . TURE FLOW RATE \*\*\* \*\*\*\*\* \$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$ LIT-RS/ UND GNZ KG/SQ CM KG/SO CM P514 DEG. K **SCFM** DIFFERENTIAL PSLO UEG. C DEG. F MIN 1CFW KG/HK LBS/HR 70.586 297.4 5,694 1004.0 74.3 75,7 2.892 12.554 3.9638 56.379 82.1 • 426 70.586 1004.0 23.8 >96.9 74.8 74.7 . 389 2.633 5 J 8 5 3.5219 50.094 11 432 70.586 1004. 296.7 74.4 65.7 . . 343 4.573 43./54 23.6 2.323 10.n83 3.0762 70.586 1004.. 296.₽ ¢3.1 • 298 3.76 37.098 74.6 56.6 2.015 8.745 2,6083 70.307 1000.. 23.5 -96.9 74.8 47.2 ·1251 1.655 3:317 7.317 2.1195 30.147 1.375 70.307 1006.0 297.2 75.3 2.70! 23, [91 24.1 38.3 .0204 5,968 1.6727 70.307 297.6 1000. 24.4 75.9 28.7 )153 1.030 2 .: 20 4.472 1.2174 17, 216 70.307 1000.0 -97.8 74.6 76,3 .013 .871 1./15 3.781 1.0129 14.507 74.2 70.307 1000.0 298.1 24.9 76.9 19.4 J105 .7.2 1.484 3.048 .8000 11.479 70.586 1004. 298.6 25.5 77.9 12.8 .471 .92! • 07 2+043 .5203 7.200 70.586 1004.0 199.4 .473 •331 26.2 79.2 12.9 .407 2.053 .5243 7.457 70.586 1004. 299.5 26.3 79,4 19.8 .715 1.407 .8226 11.700 .0107 3.106 70,586 1004... 299.6 26.4 79.6 23.8 .858 1.689 3.723 • 128 1.0042 14.283 70.586 1004-1 299.6 79.5 6.4 28.8 • 1155 1.039 2:140 1.2380 17.208 4.510 70.586 1004.0 >99.4 26.3 79.3 37.2 199 1,335 2.627 5.796 1.6367 23.280 70.586 299.1 25.9 1004.7 78.7 46.7 .0248 1.664 3.27 ( 7.224 2.1025 29 905 70.307 1000. 298.7 25.5 77,9 . 297 56.2 1.994 3.425 B • 654 2.587į 36.797 1000.0 70.307 .98.1 75.3 76.9 65.0 134 2.298 4.525 9,976 3.0572 43.484

:

.69

.78

.87

# TABLE 84 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 110 > PART D

FLOWMETER CONDITIONS 

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8] ៖ [

87•1

Do.S

5..2

49.9

.71

.81

91

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE versus DIFFERENTIAL PRESSURE. TOTAL OF 11.3 mg OF SYNTHETIC CONTAMINANT ADDED. TEST

409.6

418.7

418.1

81.9

81.8

81.8

.0847

.0937

·1041

PAGE: 1

DATE: 7-8-76

FLOWM: 1EH ONE			*****	FLOWMETER TWO	***				
	FLOW RATE (ACFM)	PŘESSURE (PŠÍA)	ţEMP (DEG• F)	FLOW RATE (ACFM)	PRESSURE, (PSIA)	TEMP (DEG. F)	PRESSURE (PSI4)	AVG TEMP (DEG. F)	ĀVĠ FĻOW RATE (ACFM)
	.88	45.2	୩ନି•୍ମ	•92	47.4	6 <b>2</b> •2	412.9	ė1.5	•1051
	.78	٥ų <b>,</b> 4	ลกั <b>.9</b>	.81	48,7	85*5	412.2	81,6	.0957
	.69	5v.2	8ñ • 9	• 7¢	48.9	82.3	411.6	81.6	• ĝ835
	•60	50.1	გ∄ • 9	•6l	49• Ī	80.4	410.9	81.7	•0730
	•51	44.9	คก์ • 9	.51	48,9	82.5	4io,9	81.7	.0610
	• 41	⊃v 4	3409	•41	49,9	R <b>⊅</b> •5	410,9	81.7	. 5499
	•32	49.9	AT+2	•31	49.5	82.6	414.9	81.9	• ö379·
	•27	49.9	81 <u>.</u> 4	• <del>š</del> 6	49.3	85 <b>.</b> 8	4Ĭì.6	82.1	•ó3Ĩ5
	•22	ր*8	eī.a	.21	49.7	83 <b>.</b> n	411.6	82.4	.025B
	<b>.</b> 15	50 <sub>-</sub> 1	92•Î	• 13	49.9	#3 <b>*</b> 3	411.6	82.7	•ŏ17ō
	•15	49.5	8.94	•13	49.3	83.5	412.5	82.9	.0168
	<b>,</b> 21	50.2	82.5	•50	49,9	83.7	412.2	83.1	•ó25 <b>4</b>
	•2Ž	49,9	ฅอ๋•ฺอ๋	• ∌6	49.5	43.5	411,6	82.8	• 0319
	•32	49.5	ลโ•ฺร	• 71	48.9	83+3	411.6	82.6	.0374
	•41	47.9	81.5	.40	49•ï	93.5	410.9	82.3	• 0492
	•51	45.a	9 <u>7</u> •3	•50	49•Ĭ	93 <b>.</b> q	414.9	82.2	• 06 09
	<b>.6</b> 0	49.7	8i • 1	•60	48.5	8>+8	410.3	82.0	.07žl

48.7

48.5

47.8

82.7

82.5

85.4

PAGE: 2 TABLE 84 FLOW RATE VERSUS DIFFERENTIAL PRESSURE DATE: 7-8-76

CONTAMINATED CONDITION - FLOW RATE versus DIFFERENTIAL PRESSURE, TOTAL OF 11.3 mg OF SYNTHETIC CONTAMINANT ADDED. TEST TEST DESCRIPTION TEST NUMBER 11D PART D SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL).

	ECTWEN INFEL CON		o.bom.m.	(5) 11 020)	INDEE INDEE OF	m	,,		
PRESSURE	aVG ŢEMP	ÁVG FloW_R∆TE	GROSS DIFF. PRESS PRIMARY	GROSS DIFF. PRESS SECONDARY	AVG GROSS DIFF. PRESS	DIFF.	ARE PRESS	NET DIFF PRES	S

PRESSUKE	AVG TEMP (DEG. F)	ÁVG FLOW RATE ((CFM)	GROSS DIFF. PRESS PRIMARY (PSID)	GROSS DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	NEŤ DIFF; PRESS (PSID)	
412.7	81.5	,1o51	183,709	183,709	183.709	\$00.	183.706	
412.4	81•6	• :957	155.616	155.616	155,616	•001	155.615	
411.0	81.6	• 0835	127.208	127.208	127.208	.001	127.206	
410.9	81.7	.0730	105_428	1 15 428	105.428	.001	105,426	
410.7	81.7	.0610	82,199	83.716	8 <b>2.</b> 6n8	.001	82,606	
410.5	21.7	.0449	63,533	64.393	63.963	.000	63.961	J
410.9	41.9	.^379	46,785	46.597	46,691	.000	46,689	
411.9	42.1	.n315	38,144	37,842	37.943	.000	37,942	
411.0	&2•4	•×558	3n.148	29,915	30.032	•000	30.030	
411.0	82.7 ·	.0170	19,151	18,863	19.00/	.000	Ĩ9.000	
412.4	82.9	.0168	18.707	18.749	18.729	•000	ï8.726	
412.4	#3• <u>1</u>	.:254	29,654	.29,456	29.555	• 000	29.554	ą
411.9	85*8	.0319	38.414	38,310	38,358	.000	38.357	
411.0	92.6	.9374	46,232 .	46.020	46.126	•000	46.124	
419.9	92∙3	.492	62,657	63,446	63.452	•000	63.050	
410.7	82.2	•0609	446.ح	83,332	87.889	.000	82.887	
410.5	82.0	.0721	103.849	103,849	103.849	.001	103.848	
409.0	81.9	.~847	129,733	129,733	129.733	.001	129.731	,t
418.	81.8	.0937	149,934	149.934	149.934	.001	149.933	
418.1	⊲1.8	.1041	178,659	178,659	178,659	•002	Ĩ78,657	

JARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM) \*\*2 + 0 (ACFM) \*\*3

# TABLE 84 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3

DATE: 7-8-76

TEST DESCRIPTION TEST NUMBER 110 PART D

CONTAMINATED CONDITION - FLOW RATE versus
DIFFERENTIAL PRESSURE. TOTAL OF 11.3 mg
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL).
NET DIFFERENTIAL PRESS 

PRESSURE		ГЕМРЕК (TURE			FLOW RATE				****	•	•		
	Kē\sa Cw	P\$14	DEG. K	ĐEG. C	DEĢ, F	LIT#RS/ MIN	4CFM	SCFM	ĸĞ∖Hǩ Gu≶	GN2	KG/SQ CM DIFFERENTIĀL:	PSĪQ	,
	29.028	412.7	3 <u>00.</u> 7	27.5	87.5	81.7	•1951	2.890	5.690	12.544	12.9759	183.70t	
	28.982	412.4	300,7	>7.5	81.6	74.3	.0957	2.626	5 <u>•</u> 171	11.400	10.9408	155,61	
	28.937	411,0	300.7	27.6	81.6	64.6	.0835	2,288	4.504	9.930	8,9435	127.20+	
1	58*891	410.7	300.7	27.6	81.7	56+1	•"73c	1.996	3.555	8.663	7.4122	105.42	
	28.891	410 • ۶	8,005	»7 <b>.</b> 6	81.7	46.6	.4610	1,668	3•284	7•239	5.8078	82, <b>6</b> 01	4
	28.891	410.9	300.8	27.6	81.7	38.1	.:499	1.366	5*68Ă	5.928	4,4969	63,96;	J
	28,891	410•₹	300.9.	27.7	81.9	28.8	.0379	1.036	2,032	4.496	3,2826	46,685	
	28.937	411.0	301.0	27.8	82.1	24.9	.0715	.864	1.700	3.749	2,6676	37.946	
	28.937	411.9	3,1,2	28.0	82,4	19.6	. 258	.707	1,392	3∙ე68	2,1113	30 <b>.</b> 03r	
4	28.937	411.9	3,1,3	28.2	82.7	12.7	•3176	.466	•91[	2.452	1.3359	19.00°	
	28.982	41244	301.5	2A.3	82.9	12.5	.0168	.460	• <u>9</u> 0 <u>0</u>	í.998	1.3166	18.72	u
	28,982	412,4	301.5	28,4	83,j	19.2	.0254	,696	1,370	3.021	2+0778	29.55	٠
	28.937	411,9	381.4	29.2	82.8	24.2	. 319	.872	1:715	3.787	2.6967	38,35"	
	28.937	411:2	3-1-3	28•1	82.6	28.5	. 0374	1.022	2014	4 • 436	3.2429	46.121	
	28.891	410.9	301.1	38.0	85.3	3 <b>7∙3</b>	.0495	1,343	2:647	5.830	4.4329	63,05	
٠	28,891	410,7	301.0	27.9	82.2	46,6	.0609	1.654	3.276	7.223	5;8276	85.68.	
	28.845	41025	300.9	27.8	82.5	55.1	• ::721	1.967	3.87€	8.537	7.3012	103.841	ri
	28.800	409 • 0	300.9	27.7	81.9	65.0	.0847	p.308	4.544	10.018	9.1210	129.73.	Į,
	29,438	416.	300.8	27.6	81.8	73.8	.0937	2.612	5,144	11.339	10.5413	149,930	
	29•393 ****	418.1 ****	300.8 ****	27.6 *****	81.8 *****	81.9	-1941	2.897	5•?n4	ĩ2•575	12.5609	178,65	
	28,971	412.1	301.0	27.8	82.1								
	•098	1.4	•2	• 2	• 4	DEVTATIONS	S						

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 11E PART F TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE Versus
DIFFERENTIAL PRESSURE. TOTAL OF 16.7 mg
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N.020) INLET FRESSURE 1000 PSIA (NOMINAL).
TEST SPECIMEN INLET CONDITIONS

PAGE: 1

7-8-76

DATE

FLOWNEIER ONE		444 <del>44</del> 4444	FLOUMETER TWO	***		,	•		
FLOW RATE (ACFM)	PRESSURE (PSIA)	TENP	FLOW RATE (4CFM)	PRESSURE, (PSI4)	TEMP (NEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	ĀVĢ Flow Rāte (ācfm)	נו
.86	50.1	67•3	.91	47.9	<del>7</del> 5,8	992.1	70.0	.0437	
.78	50.4	64+R	"Al	48.5	72.2	992,1	69.5	. 6397	
•68	20.00	66+5	•70	48.9	71,8	992.1	69.2	•6344	
.60	5 Ú • 4	66+8	• 60	49.3	7i.8	992.1	69.3	.0302	•
•50	÷2.5	67.2	• 5:	48.7	71.9	992.i	- 69.6	. 0249·	1
•41	49.9	67.8	.40	49.3	7ż. >	992.1	70.0	. 6264	•
<b>•31</b>	49-1	68 • 7	<b>∗3</b> ⁴	48.7	72.8	992.i	70.7	.0151	
•27	50.2	69+5	• >6	49.9	73,2	992. 1	71.3	,ól33	
•22	50.5	75.2	.21	49,9	73.5	992.7	71.6	.0107	•
•15	49.9	7֥9	•14	49.9	74.	992.1	72.4	", ècŶZ ""	
.15	42.7	75•5	•14	49.5	74.7	995.1	73.4	.007Ź	~ †
•52	44.2	72.2	.21	49.1	74.9	992.7	<b>73.5</b>	,6167	,
.27	<del>1</del> 9.5	72.1	• 56	49.3	75.	992.1	73.6		-
.32	50°5	7Ĩ <u>•</u> 9	•31	79.9	75.1	992.7	73.5	;61\$7' ″	•
•41	₽Ų•I	7ī••	.41	49.5	<b>75.</b> 0	992. 1	73.2	, ēžē4	
<u>,</u> 51	<u> </u>	77.27	•51	48.5	74.7	992.7	72,T	, 0880	
•60	49.5	69+7	•60	E.8%	74.1	992.1	71.9	. ô <b>29</b> 6 ` ~	
•69	49°3	69 • 0	.71	48.5	73.6	988.7	71.3	FAEō.	. 1
•78	49.5	63+2	•81	47.6	73. i	988.1	70.6	. 6 <b>39</b> 6	
.87	45.2	67 • 5	•91	47.4	72.3	988.į	69.9	.0436	

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TABLE 85 PAGE: 2 DATE: 7-8-76

CONTAMINATED CONDITION - FLOW RATE versus TEST DESCRIPTION TEST NUMBER 11E PART E DIFFERENTIAL PRESSURE. TOTAL OF 16 7 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL).

TEST SPECIMEN INLET CONDITIONS

PRESSUME (PSIA)	AVG IEMP (DEG. F)	AVG Flow Rate (XCFM)	GROSS DIFF. PRESS PRIMARY (PSID)	GROSS DIFF• PRESS SECONDARY (PSID)	AVG GROSS DIFF: PRESS (PSIÙ)	TARE DIFF. PRESS (PSIO)	NEŤ DÍFF, PRESS (PSIÔ)	7
992,1	70.0	.0437	58,641	59.417	59.029	-0.000	59. <u>0</u> 29	
992.1	69.5	. 397	51.874	52.464	52.169	-0.000	52.169	
992.1	.9•8	344	44.799	44.:20	44.659	-0.000	44.659	
992,1	69.3	.03(2	38,372	38,163	38.217	<b>-0.000</b>	38,217	_
992.1	69.6	.:249	30.57:	30.240	30,405	-0.000	30.406	
992.1	70.0	.0204	24.244	23.927	24.086	-0.000	Ż4.086	1
992.1	70.7	.0151	17.409	17.17a	17.290	<b>→0.000</b> '	Ĩ7.290	
992.1	71.3	.:133	15,146	14.826	14.935	-0.000	14.936	
992.1	-1.A	.0187	11.933	11.7 i	11.837	<b>~0.00</b> 0	11.837	
992.1	72.4	.0172	7.821	7,632	7.726	-0.000	7.727 ,	
992.1	73.4	.0472	7,696	7.632	7.664	-9.000	7.664	
992.1	73.⊭	.0107	11.684	11,683	11.684	-0.000	11.684	!
992.1	73.6	.0130	14.672	14.654	14.663	<b>-</b> 0.000	14 <sub>6</sub> 663	
992.1	73.5	. 157	17.969	17.914	17.941	-0.000	17.942	
992.1	73.2	.0206	24.3n6	24,214	24,260	-0.000	24,260	
992.1	72.7	•025n	30.694	34,527	30.611	-0.000	30.611	
992.1	71.9	<u>.</u> ^296	37.444	37,199	37,321	⇔n.000	37.322	
988.1	71.3	<u></u> ^348	45 <sub>1</sub> 169	44.866	45.018	<b>~0.000</b>	45.018	į
988.1	70.6	•n390	50.621	51.199	50.910	-0.000	50.910	
988.1	p9.9	. '436	56.391	59.417	58.904	-0.000	58.904	

TARE DIFF. PRESS = -1.64000E-04 + -1.26930F-02 (ACFM) + 2.48070E-01 (ACFM) +2 +

n (ACFM) \*\*3

TABLE 85 FLOW RATE VERSUS OFFFERENTIAL PRESSURE

PAGE: 3

DATE 7~8-76

CONTAMINATED CONDITION - FLOW RATE versus
DIFFERENTIAL PRESSURE. TOTAL OF 16 7 mg
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NCMINAL).
NET DIFFERENTIAL PRESS TEST NUMBER 11E PART F TEST DESCRIPTION TEST SPECIMEN INLET COUNTIONS

	***	**	****	*****	****	****	****	***	**	***	***	****	
1	PRESSU		TE::PERATURE		FLOW								
	KĢ/SQ CM	PSIL	OFG. K	DEG. C	DEG. F	LITERS/ MIN	>CF#	SCFM	ĸĞ∖HŘ ens	GN2, L95/HR	KG/SQ CM DIFFERENTIĀL	PSĮD	;
	69.750	1.566	294.3	71.1	70.0	83.9	.0437	>.949	5.806	12.800	4.150ž	59,029	
	69,750	495.1	294.0	29.8	69,5	75.9	.0397	2,680	5,279	11.632	3,6678	52,169	
	69.750	992.1	293.8	27	69,2	65.8	. 344	2.325	4.579	10.095	3,1399	44,659	
٠	69.750	992.1	293.9	±0.7	69.3	57.5	.0305	2.041	4:012	8.859	2.6869	jā.217	
	69,750	992.1	294.0	20.9	69,6	47.1	.0249	1.680	3•ិ3បិត្ត	7,293	2,1377	30.206	.1
	69.750	992.1	294.3	21.1	70.0	38.3	.1204	1.375	2,70!	5.969	1.6934	24.086	
	69.750	992.1	294.7	21.5	70.7	28,3	.3151	1.017	5.00%	4.414	1.2156	17°590	
	69.750	992.1	295.	8. 15	7î,3	24.9	• 133	.896	1.764	3.889	1.0501	14.936	
	69.750	995.1	295. 3	22.1	7i.8	19.9	•0117	.723	1.423	3.137	.8322	īi.837	
ŀ	69.750	992.1	295,6	77.5	72.4	13.2	•0072	.486	•95 <u>5</u>	2.109	.5432	7.727	
	69.750	992.1	296.2	23.	73.4	13+1	• 072	.482	.949	2.093	.5389	7,664	31
	69.750	992.1	296.2	23.1	73.5	19.7	.0107	.715	1.405	3.104	.8 <u>2</u> 15	11.684	y
	69.750	992,1	296,2	23.1	73,6	24.3	.0136	.875	1•?z?	3.796	1.0309	14.963	
	69.750	992,1	294.2	23.0	73,<	29.3	.0157	1.055	2.075	4.580	1.2614	17.942	
	69.750	992.1	296.0	22.9	73.2	38.6	.0206	1.381	2.719	5.993	1.7657	24 <b>.</b> 260	
I	69.750	992.1	295.8	22.6	72.7	47.2	. 1250	1.681	3.310	7.298	2.1522	30.211	
	69.750	992.1	295.3	2.48	71.9	56∙1	•0296	1,989	3,915	8.634	2.6240	37,322	
	69,471	1,886	295.0	27.8	71.3	66+4	•134A	2,333	4,594	j̃∩•128	3.1651	45,018	,
	69.471	988•1	294.6	21.4	70.6	74.7	•a39n	2,617	5,153	ī1•36a	3.5794	50.210	
	69.471 ****	988.1	294•2 ****	2j.1 *****	69 <b>.</b> 9	83.5	•0436	2,932	5.2773	i2•728	4.1414	58,904	
	69.708	991.5	295.0	21.9	71.4								
	.071	1.0	•8	•8	1.4	DEVIATIONS	S						

.79

.88

Dr. 2

51.2

79.1

79.4

TABLE 86 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST MUMBER 11F PART F

.81

•91

FLOWMETER COMMITIONS 

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS 

PAGE: 1 DATE: 7-8-76

	•								•	
;	****	FLOWNLIER ONF		****	FLO METER THO				_	
	FLOW RATE	PRESSURE (PSIA)	TFMP (DEG• F)	FLOW RATE (ACFM)	PRESSURE. (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	ĀVĢ FLOW RĀTĒ (ACFM)	Ì
	•88•	49,5	77•4	•91	47.5	7,,9	4 <b>ï2.</b> ñ	78.1	.1050	
	<b>.</b> 79	51,4	77+5	•81	48.7	79.	4Ĩ1 <b>.</b> 3	78.2	• õ̃959	
	• 70	1,30	77.5	•71	^8 <b>.</b> 5	79.1	410.7	78.3	.0842	
ţ	,61	45.8	77.7	.61	48.7	79.3	410.7	· 78.5	•õ734	-
	•51	51.5	77•7	•51	49.2	79.4	41n.7	· 78.6	• ó6 ī5	٠;
	•41	>0.1	77.9	.40	49.4	79.6	410.7	78.8	. ā496·	
	•31	⇒6 <sub>+</sub> 1	78•2	•31	49.8	79.7	410.7	79.0	.0375	
	.26	ph*1	78•4	•25	49.B	79.9	410.7	79,1	.0313	
	•21	50.4	79.6	,20	50.0	9n.2	410.7	79,4	• ő255	
	•15	5,,1	79•9	.13	49.R	e: •2	411.3	79.6	-0170	
	<u>.</u> 15	44.1	79•4	•13	48.8	80.7	412.0	80.1	.0166	J
	•ss	5¢.1	79+4	.21	49.8	80.8	412.0	80.1	• 0258	,
	• 27	49.9	70.4	. 26	49.4	A4.8	411.3	80.1	.0321	
	•35	47.7	79.2	•31	49•2	₽÷•8	411.3	80.0	.0380	
	•42	50.1	79 <u>*</u> 1	•41	49.~	8^.7	411.7	79.9	.0496	
ŀ	•51	=U+1	79•0	•51	49•0	86.7	410.7	79.9	•06Î7`	
	•60	<b>⊅</b> 0,4	7B+9	•6)	49.2	88.7	41n.n	79.8	. 6730	í
	• 70	44.5	79.	•71	48.2	8n.7	410.0	79.9	.0838	,

48.5

413.3

80.7

8.06

410.0

419.1

79.9

80.1

.0959

1052

PAGE 2 TABLE 86 DATE 7-8-76 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION - FLOW RATE VERSUS TEST DESCRIPTION DIFFERENTIAL PRESSURE. TOTAL OF 16.7 mg TEST NUMBER 11F PART F OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL).

TEST SPECIMEN INLET COMPLITIONS \*\*\*\*\* aRMSS OIFF. PRESS ลู่สารรร NEŤ ΔVG GHOS≥ TARE DIFF. PRESS ΛVG , VG DIFF. PRESS DIFF. PRESS DIFF. PRESS SECONDARY PRIMARY ļţ PRESSURE TEMP FLOW ROTE (PSIN) (PŠIÚ) (PSID) (PSID) (pSI0) ( · CFM) (DEG. F) (PSIA) 189,495 189.496 -002 189.496 189,496 78.1 . 1950 412.0 160.455 .001 160.456 160,456 .0959 160.456 78.0 411.5 132.046 132.048 .001 132,048 132, 148 .0842 78.3 410.5 108.372 108.374 .001 . 1.734 148.374 1-8.374 78.5 410. 84.706 84.717 .001 64. 199 95.: 15 .0615 8.6 410. 64.178 64.49R 64.184 .000 63.862 .n496 78.8 410. 46.445 46.447 46.3 A .000 ..375 46.595 79.1 410.7 37.670 37,672 .000 37.544 .0313 37,800 410. 79.1 29.586 29.585 .000 29.435 29.74 410:5 79.4 . 225 19.001 .000 19.000 18.8 9 .0170 19,174 79.6 411.3 18.546 18,547 .000 15.543 .0166 18,552 50.1 412.0 Ή 30.210 30.211 .000 30.298 3 .. . 125 . 4258 412.0 86.1 38.832 18.753 38.834 .000 38,915 86.1 .43.1 411.5 47.370 47.372 47,512 47,232 .000 ζ. .0380 411.3 80.0 64,461 64,463 .000 64. 14 . 1496 64,112 79.9 411.2 85.391 85.392 .001 85.647 85,138 79.9 .4617 410.7 107.425 107.427 .001 107.407 107,427 .0730 410.0 79.8 d 131,099 131,101 .001 131,101 .0838 131,101 79.9 410.0 161.402 161.403 •001 161.443 . 1959 161.443 79.0 410.0 188.232 •002

188.234

188 . 234

LARE DIFF, PRESD = -3.40000E-05 + -4.44006E-04 (ACFM) + 1.50933E-01 (ACFM) 442 +

188.234

80.1

419.1

-1052

(ACFM) ##3

TABLE 86 PAGE: 3
DATE: 7-8-76

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 11F PART F

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 16 7 mg OF SYNTHETIC CONTAMINANT ADDED. TEST

								•			•	
PRESSU		***	leyPER.TURE	****	*****	FLOW RATE	FLOW RATE					
Kē∕ēơ ¢w	PS1,	DEG. K	DEG. A	DEG. F	LIT#RS/ MIN	4CFM	SCFM	KÖ\HK PINS	GN, S,HR	KG/SQ CM DIFFERENTIÄL	PSÁD	
28 963	412.	298.8	25.6	78,1	82*0	.105-	2.899	5.107	12:586	13.3228	189.495	
28,918	411.5	29A.B	25.7	78.2	74.5	• 1959	2,642	5 . 20 3	11.470	11.2811	160.455	
28.872	41!	298,9	25.7	78.3	65.4	. 642	2,317	4.56¢	10.657	9.2838	132.046	
28.872	410./	299.4	25.6	78,5	56.5	./734	>.619	3.975	8.762	7.6193	108.372	
28.872	410.	299.0	25,9	78.6	47.1	. 615	1.690	3.325	7.337	5.9554	84.706	ţ
28 872	410.5	299.1	25.	78.8	37.8	. 496	1.362	5+683	5.914	4.5122	64.178	•
28,872	410.1	299.3	26.1	79.6	28,5	1375ء	1.030	2+12%	4,473	3,2654	46,445	
28.872	41 . • !	299.3	26.2	79.1	23.7	. 313	.861	1.695	3.736	2.6485	37,670	
28.872	410-1	299.5	26 <b>.</b> 3	79.4	19.>	.0>55	.700	1.379	3.041	2.0801	29 <b>.</b> 586	
28,918	411,3	299.6	26.4	79.6	12.7	.n17e	.469	•923	2.n34	1,3358	19.000	
28.963	412.	299.9	26,7	88.1	12.3	. 166	.456	•ឧଚନ	1.981	1.3039	18.546	ı
28.963	412.4	299.9	24.7	80.1	19.6	1258	.710	1,495	3 • 981	2.1240	30.510	•
28.918	411.5	299.9	26.7	80.1	24.4	321	.882	- 1:735	3.830	2.7302	38.632	
58° 318	411.3	299 <sub>.</sub> B	24.7	80.0	2A.9	,0390	1.044	2.155	4.531	3,3305	47,370	
28.918	411.2	299.8	25.6	79.9	37.8	496	1,363	5•683	5.915	4.5321	64.461	
28 • 872	410 - !	299.8	26.6	79.9	47.2	• 617	1.691	3,336	7 • 341	6.0035	85.391	
28.826	410.4	299.7	26.6	79.8	56•0	1F70.	1,999	3± <sup>9</sup> 3∫	8.679	7.5527	107.425	11
28,826	410.0	299_8	26.6	79.9	64.8	<b>.</b> #839	2,295	4.5 <u>2</u> J	9.964	9.2172	131,099	
28.826	410.	299.8	- 26.6	79.9	74-1	• 959	2.627	5•174	11+463	11.3477	161.402	
29•466 ****	419.1 ****	299 <b>.</b> 9	26.7 *****	80.1 *****	82.2	.1)52	2,943	5•794	12.774	13.2340	188.432.	
28,920	411.5	299,5	26,3	79,4								
•068	1 • y	• 4	• 4	•6	DEVIATIONS							

# TABLE 87 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 7-8-76

TEST NUMBER 116 PART G

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 24.1 mg

FLOWMETER CONDITIONS

****	FLOWNEIER ONE		***	FLOWMETER TWO	****			AVG AVG TEMP FLOW RATE (DEG. F) (ACFM)	;
ELOW RATE	PRESSURE (PSTA)	TEMP (DEG: F)	FLOW RATE (ACFM)	PRESSURE, (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	TEMP		
.86	49.7	<b>75</b> ∙8	•91	47.6	81,5	1904.0	78.7	.0429	
.78	49,9	75•4	18.	48.1	ei	1 104.0	78.2	.ô38B	
.69	47.5	75• -	•71	47.9	8ċ•6	1 104.0	77.9	•0339	
.60	45.2	75.3	.60	48.3	8n_6	1000.5	78.0	.0295	
•51	50.1	75.6	•51	49.1	3ñ•6	1400.0	78.1	.0251	1.
<b>.41</b>	42.5	76-1	41	48.9	8n.8	1000.5	78.5	.02ó2	- '
•31	49.7	76.7	•30	49.3	Sien	1000.0	7B.9	•0153	
•27	49.5	77 <u>*</u> 3	• 26	49.Ĩ	ā1+3	1000.0	79.3	.0130	
•22	49.7	78+n	.21	49,3	87.7	1900.0	79.8	.0107	
•15	45.2	78+6	•13	49.3	<b>45•</b> 4	1 100.0	80.3	.0070	
.15	49.1	79,9	•13	48.7	8-6	1000.0	81.2	.0069	t
.23	49.1	79.8	*55	48.7	85 <b>∙</b> 6	1000.0	81.2	.0108	•
.27	42.9	79•6	• 56	49.7	95° e	1:00.0	81.1	.0133	
•35	42,7	70:4	•31	£9.3	82.6	1000.5	81.0	.0156	
.41	49,5	78.8	.41	48.7	82.4	1000.0	80.6	.ożō1	
•50	49.1	78• <u>1</u>	•5U	48.3	82.2	1000.n	80.1.	.0246	
.60	42.7	25.57	•60	;8.5	81.7	1000.0	79.5	.0295	ı
,69	42.7	76.0	.71	48.3	ត <sub>្</sub> ន	1000.0	78.4	.0343	•
.78	50.2	74.9	•81	48.5	79.8	996.ā	77.4	•õ39 <b>4</b>	
.87	49.7	74.0	,91	47.6	78.9	996.0	76.5	.0435	

TABLE 87 PAGE: 2
DATE: 7-8-76

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 24.1 mg
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN INLET CONDITIONS

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 24.1 mg
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 020) INPUT PRESSURE 1000 PSIA (NOMINAL).

\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*

PRESSUKE (PSIA)	TEMP (UėG• F)	AVG FLOW RATE (+CFM)	ARCSS DIFF. PRESS PRIMARY (ASIQ)	GRASS DIFF• PRESS SECONDARY (PSIÁ)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	NEŤ DIFF• PRESS (PSID)
1004.0	78,7	.0429	59,694	60,214	59,954	-0.000	59,954
1004.y	78.2	• • 388	52,559	53,279	52.919	<b>-0.00</b>	52.919
1004.ÿ	77 <u>•</u> 9	.0339	45.697	45,329	45 • 468	-0.000	45.468
1000-0	7a.ງ	<b>1</b> 0295	38,519	36,254	38,385	-0.000	38,382
1000•0	78.1	.^251	31.77	31,482	31.650	-0.000	31.627
1000.9	78 <u>.</u> ¤	.0202	24.524	24.211	- 24.367	<b>⇔0.000</b>	24.367
1000.9	78,9	,1153	17_947	17,698	17.822	-0.000	17,822
1000.0	79.3	.1134	14.84	14.617	14.729	-0.000	14.729
1000.2	/9•₿	.0107	12,1-7	11,939	12.053	-0.000	12.053
1000.9	80.3	.0070	7,562	7,442	7.502	-0.000	7,502
1000.0	41.2	•nn69	7.438	7,385	7.411	<b>~</b> 0.000	7.412
1000.0	1.Z	.0198	12,10	12,110	12.107	-0.000	12.108
1000.0	81.1	.n133	15,151	15,188	15.169	-0.000	is.170
1000.0	81.0	. ñ156	18,195	18,154	18.175	-0.000	18.175
1000.0	ರ0.6	.0201	24,276	24,211	24.243	-0.000	24,243
1000.9	80.1	.ñ246	30,842	30.737	30.790	<b>-0.000</b>	30.790
1000.0	79.5	•0295	3A <sub>4</sub> 448	38,25%	38.351	<b>~0.00</b> 0	38.351
1000.0	78.4	.n343	46,938	45,789	45,914	<b>~</b> 0.000	45.914
996.0	77.4	• n394	53.185	54.224	53.7 <sub>0</sub> 5	-0.000	53.705
áae*n	76.5	.0435	60,570	61,475	61.023	~0.000	61.023

LARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM) +2 +

n (ACFM) \*\*3

TABLE 87 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 7-8-76

TEST NUMBER 116

PART G TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 24.1 mg
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 020) INPUT PRESSURE 1000 PSIA (NOMINAL).
NET DIFFERENTIAL PRESS TEST SPECIMEN INLET CONDITIONS

	******	****	*****	***	****	****	****	****	***	****	ត្តស៊ីនិទីទសិតស៊ីតំទំនង់ដឹ	ត់និន់ង់ង់នទឹងនិះ **
į	PRESS	URE	****	TEMPERÄTURL	***	****	***	FLOW RATE	****	****		
	KG/SQ CM	PSIA	DEG. K	ĢEG. C	DEG. F	LITERS/ MIN	\CFM	ScFM	κā∖н∺ ēиS	GN2	KG/SQ CM Differentiäl	PSAD -
	70.586	1004.9	299•1	25.9	78.7	87.9	• 7429	2,882	5,674	72.5n9	4.2152	59, 254
	70,586	1004.4	8,862	25.7	78.2	74.0	.u388	2,611	5,141	11.334	3,7206	52 <b>.</b> 919"
	70 <u>•</u> 586	1004•0	298.7	25.5	77.9	64.4	• •339	2.282	4+494	9•9ñ7	3.1967	45.468
1	70.307	1000,0	298.7	25.5	78.Ó	55.5	• 1295	1.975	3.88%	8.574	/ 2.6985	~38.38ē
	70.307	1000.0	298.8	25,6	78,1	47.1	.0251	1,681	3,30%	7.295	2,2236	31.927
	70.307	1000+0	299.0	25.8	78.5	37.6	•0202	1.351	5•̃ <u>6</u> €1	5.866	1.7132	24.367 "
	70.307	1000.0	299.2	26.0	78,9	28.4	.0153	1.024	2.01(	4.446	F.2530	17.522
	70,307	1000±0	299.4	26.3	79.3	24.0	.0139	.866	1=709	3.761	1.0356	14.729
	70.307	1000.0	299.7	26,4	79.8	19.7	.0107	.718	1,413	3.116	.8474	12.053
l	70.307	1000.0	300.0	26. <sup>8</sup>	8 <sub>0•3</sub>	12.6	.007a	.466	<u>•</u> 91	2, 521	.5275	7.502
	70•307	1000,0	300.5	27.4	81.2	12.4	• 1069	.458	•90 I	ĭ•986	.5211	7.412
	70.307	1000.0	300.5	27.3	81.2	19.9	.0108	.721	1,421	3+Í32	.851ž	îż.loB
	70.307	1000,0	300.4	27.3	81.1	24.5	•4133	.883	1,737	3.833	1.0665	T5. 170
	70,307	1000.9	300.4	27.2	81.0	28.8	.0156	1.037	2.044	ă.501	1.2778	18,175
	70,307	1000.0	300.1	27.0	80.6	37.3	.0201	1,341	2.640	5.820	1.7545	54.543
1	70.307	1000.0	299.9	26.7	80.1	46+0	.0246	1.640	3.229	7+119	2,1547	30-150
	70.307	1000 • 0	299.5	26.4	79.5	55+6	• '295	1.974	3•88₫	8.571	ž.6964	38,351
	70,307	1000.0	298.9	25.8	78.4	65.0	.0343	2.299	4•25]	9.98î	3.2281	45 <u>-</u> 214
	70,029	996≛4	298.4	25.2	77.4	74.7	•J394	2.635	5.189	īi•44ō	3,7758****	53.705
	70 <u>+</u> 029	996 <u>.</u> 0	29 <b>7.</b> 9	24.7 *****	76.5	8 <sub>2.</sub> 5	•0435	2.910	5• <u>1</u> 30	îp <u>•</u> 634	4.2903	91.053
	70,321	1000.€	299.4	26.2	79.2							
	•079	ļ.1	•7	•7	1.2	DEVIATIONS	5					

PAGE: 1 DATE: 7/8/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 11H PART H

TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS F DIFFERENTIAL PRESSURE, TOTAL OF 24.1 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

# .

*****	FLOWMETER ONE	***	****	FLOWMETER TWO	***			÷
FLOW RATE	PRESSURE (PSIA)	TEMP (DER: F)	FLOW RATE (ACEM)	PRESSURE.	TEMP (DEG. F)	TRESSURE (PSIZ)	AVG TEMP (deg. f)	ĀVG Flow Rāte (ācēm)
•88	49.7	77.9	• 92	47.5	79•4	418.1	78.6	1645
.78	50.4	77.8	.81	48.7	79.3	417.4	78.5	.0941
•70	51 4	77.7	•71	49.0	79.3	416.A	78.5	. ê836
•60	50.1	77.6	.60	ر و و د	79.4	416.8	78.5	.07Ī8
•51	47°2	77°.8	.51	48.7	79.6	416.8	78.7	.0597
.41	49.9	78 <u>•</u> 0	• 40	49.2	79.8	414.8	78.9	•₫486
.32	49.7	78.3	.31	49,2	80.0	416,8	79.2	, ĝ369
•27	p₁ .1	79•5	• 56	49.8	86.1	416.8	79.3	. ô3 <b>ī</b> 6
•22	50.4	7 <b>8</b> •8	•21	50•>	8r•3	4₹6.8	79.6	. ō 256
•15	49,5	79+1	.14	49.0	8p.6	416.8	79.8	.ólŤī
•15	42.1	79 • 7	• 14	48.8	81.	417.4	80.3	.0169
+55	49.9	79.7	4.51	49.4	8j•1	417.4	80.4	0251
•56	44.9	79•8	. 55	49.4	81.2	417.4	80.5	• 03 05·
+32	49.7	79.6	•31	49.5	Bĵ.º	417.4	80.4	. 6368
•42	47.7	70.5	•41	49.0	81.1	417.4	, 8ñ•3	. 0457
•51	49.5	79+2	•51	48.7	81.1	416.я	80.1	. 6597
<u>.</u> 60	2.04	79 • 2	•60	29±0	ยกิ.9	416.1	80.0	.áŤĨ9
.69	42.7	79.2	.70	48.3	80,9	415.5	80.0	.0823
•79	49.9	79•2	•81	48•3	A + B	415.5	80.0	. 0942
.88	a^*5	79.2	,91	48.3	81.7	415.5	ŏ,08	.1062

PAGE: 2 DATE: 7/8/76

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION-PLOW RATE VERSUS
DIFFERENTIAL PRESSURE TOTAL OF 24.1 mg OF
PTION SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN
(S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

TEST NUMBER 11H PART

11H PART À TEST DESCRIPTION

TEST SPECIMEN INLET CONDITIONS

PRESSUME (PSJA)	pVG Temp (Deg <sub>e</sub> f)	ÄVG FLOW RATE (RCFM)	GROSS DIFF. PRESS PRIMARY (PSIA)	GRASS DIFF. PRESS SECONDARY (PSIQ)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	DĪFF• PRESS (PSID)	11
418,1	78.6	.1045	198_019	198,019	198.019	•005	198.017	
417.2	78.5	.~941	163.928	163,928	163.928	.001	163,927	
416. <sup>8</sup>	78.5	• 9836	135.835	135.835	135.835	.001	ī35.834	
416.9	78.5	.0718	109.636	109,636	109.636	.001	109.635	
416.8	78.7	.~597	84.458	85. 15	84.737	•000	84.735	
416 ق	78 <u>+</u> 9	.0386	64.576	65.445	65.010	.000	65.009	1
416.5	19.2	, ĝ369	47.327	46.827	47.077	.000	47.075	
416,5	79.3	,9316	39,162	38,648	38.905	.000	38,903	
416.5	79.6	• ^256	30.698	35.317	30.463	•000	30.461	
416.8	79.8	.0171	19,4>3	19,7.6	19.314	.000	19,313	
417.4	£.0p	.0169	19.174	19. 192	19,133	•000	ĩ9.ĩại	
417•4	dn.4	,3251	29.8 -2	29.743	29.772	.000	29.771	ţ.
417.4	80.5	.0305	37,490	37,389	37.436	.000	37,435	
41,7 • <u>4</u>	00.4	,n368	46.894	46,654	46.774	.000	46.773	
417 <sub>2</sub> 4	8v•3	,3487	64.326	65,129	64.727	•000 -	64.726	
416.8	50.1	.0597	84.335	85 <b>.33</b> î	84,633	.000	84.831	
416.4	B0•0	.0719	109.636	109,636	109.636	.001	109.635	- •
415.5	<b>40 • 0</b>	, AB23	133_626	133,626	133.626	•001	133.624	4
415.0	80.0	.0942	164.244	164.244	164.244	.001	164.242	
415.5	90.0	,1062	203.700	203,700	203.700	\$00	203.699	••

PART H

74.6

•6

DEVIATIONS

26.4

. 4

TEST NUMBER 11H

416.8

.5

299.6

29.304

.035

#### FLOW PATE VERSUS DIFFERENTIAL PRESSURE

TEST DESCRIPTION

PAGE: 3 DATE: 7/8/76

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 24.1 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

NET DIFFERENTIAL PRESS TEST SPECIMEN INLET CONDITIONS \*\*\* PRESSURE TEMPERATURE FLOW RATE \*\*\* \*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\*\*\*\*\* LITERS/ GN۶ GN2 KG/SQ CM KG/SQ CM PSIA SCFM K@\HK LRS/HR DIFFERENTIAL PSID. DEG. K DEG\_ C DEG\_ F MIN ACFM 29.393 418.1 5,757 299.1 25.9 78.6 82.6 .1 .45 2.923 ī2,688 13.9228 198,017 j9.347 417.4 299,4 78.5 163.927 25.8 74.3 .0941 2,631 5<u>.</u>180 11.419 11.5252 4.590 29.302 416.0 299.1 25.8 78.5 9.5501 135,534 65.6 .0836 2.334 īn.132 29.302 416.5 299. 25.8 78.5 56.2 3.944 8.696 7.7081 169.635 ...718 2.003 29.302 416.5 299.1 2-.9 78.7 46.6 . 597 1.666 3.281 7.233 5.9575 84.735 29.302 416.0 299.2 26.1 78.9 37.7 .0486 1.356 2,670 5.887 4.5706 65,009 29,302 416.5 299.4 47', 075' 26.2 79.2 28.5 . 1369 1.928. 2 . #22 4.463 3.3097 29,302 416.0 299.5 79.3 38.203 26.3 .880 1.734 24.3 .0316 3.819 2.7352 29.302 416,0 299.6 26.4 79.6 19.6 30.461 .0256 .712 1.402 3.693 2.1416 29.302 416.0 299.7 26.6 79.8 476 .93/ 1.3578 19.313 15.8 . 171 2.066 29.347 417.4 .925 Ĩ9.131 300.0 26.8 80.3 12.8 .0169 470 >•ã40 1.3451 29.347 417.4 699 26.9 80.4 1.377 29.771 300.1 19.3 .0251 3.035 2.0931 29,347 417.4 26.9 300.1 8. .5 23.4 37.435 .0305 .85ຄ 1.074 3.691 2.6319 29.347 417.4 300.0 26.9 80.4 28.4 **.**0368 1.026 2:020 3.2884 46,773 4.452 29.347 417.4 300.0 26.8 80.3 37.7 4)487 1.356 64.726 2.670 5.886 4.5507 29.30Z 416,0 299.9 26.7 80.1 46.5 .8597 1.662 3.274 7.214 5.9642 84.531 29,256 416.1 299.9 7.45 80.4 55.9 719 1.998 3,935 8.674 109.635 7.7081 29.210 80.0 415.D 299.9 26.7 2.283 4.490 64.3 . 829 9.912 9.3947 133.624 29.210 415.5 299.h 26.7 80.0 73.8 .11942 5.144 2.613 11.341 11.5474 164,242 415.5 29.210 299.8 26.7 80.0 **83.3** .1062 2.947 5.803 12.794 14.3215 203.099 \*\*\* \*\* \*\*\* \*##### \*\*\*

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 7/8/76

TEST NUMBER 111

PART T

TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE TOTAL OF 38.9 mg OF SYNTYETIC ECRTANICANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL)

TEST SPECIMEN INLET CONDITIONS FLOWMETER CONDITIONS 

FLOWMETER TWO					FLOWNC]ER ONE 44444444444444444444444444444444444							
TFM:			PRESSURE (PSIA)			FL~W RA (*CFH	<b>)</b>	TFMp (DEG: F)		ESSURE	LOW RATE	
93.	į	46.9	46.9	46,		•91		77.5		49.1	.87	
81.49	,	48.7	48.7	48,		•#1		76•4		<b>50,4</b>	.78	1
81.4		49.0	49.0	49.		•71		76+7		50.4	•69	
₽Ţ.	ł	49.0	49.0	49.		.61		76.6		20.S	<b>.</b> 60	•
81.4	ı	49.1	49. 1	49,		•51		77.7		49.9	•51	•
85.2	į.	48.8	48.8	48,		.40		77.8		44,5	•41	,
52.6	,	49.4	49.4	49.		•3)		73•5		49.9	•32	4
87.5	į	49.8	49.8	49.		. 26		79+3		54.7	•27	
B3.2		49.0	49.0	49.		.80		79.9		47.5	.21	1
P3.7		49.6	49.5	49.		-14		8**7		49.5	•15	
94.		49.8	49.8	49.		-14		A1.8		54.1	.15	
84.4		48.7	48.7	48.		.21	•	βĩ•ន		46.9	•55	,
P4.4	ı	49,4	49,4	49,		.25		8 -6		49.7	•26	•
84.4	ı	49.6	49.6	<sub>4</sub> 9.		•31		81.3		50.1	.32	•
84.1		49.4	49.4	49.		.40		85.6		50.1	.41	
83.9		49.7	49.7	49.		•50		70 . 9		44.9	•50	•
87.4		49.0	49.0	49.		•60		<b>7</b> 7•1		50€2	.60	•
82.7		48.5	48.5	48.		.71		70.2		49.9	<b>,</b> 69	•
F7.		48.7	48.7	48.		•81		77•3		4 و د	•78	•
°i.3		47.7	47.7	47,		.91		76.5		49.9	.87	•

PAGE: 2 DATE: 7/8/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER III PIRT T

TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 38.9 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 FSIA (NOMINAL)

TEST SPECIMEN INLET CONSITIONS

1

PRESSURE (PSIA)	AVG Tenp (DEG. F)	VG FLOW RATE (*CFM)	GROSS DIFF. PRESS PRIM. BY (PSIO)	Rrss DIFF. PRESS SECONDARY (PSID)	∧VG GRUSS DIFF• PRESS (PSID)	TARE Diff. PRESS (PSID)	NEŤ DIFF• PRESS (PSID)	ï
1000.9	80.3	.0426		62,106	62.106	~0.000	62.106	
996.0	79.2	347	55.829	56.116	55,972	<b>∞</b> 0.000	55,973	
996•0	78 <b>•</b> 9	•n349	48.747	47.919	48,333	-0.000	48.334	
996.Ų	79.1	.ევა1	40.640	40,259	40.453	<b>#0.00</b> 0	40.454	
996.∪	79.5	• ~ 2151	32.718	32,343	32.550	-0.000	32.551	-
996.0	80.n	insn.	24.206	24.871	25.139	-0.000	25.039	IJ
996.0	80.6	.n155	18_863	18,577	18,720	-0.000	18.720	
996.0	৪1∙1	. 133	15,687	լ5,435	15.561	-0.000	15.561	
996•0	81.6	*011'	11.886	11.724	11.805	-0.000	11.806	
3à4°ñ	95.5	.0073	8.016	7.907	7.963	<b>⇔0.000</b>	7,963	
996.0	B3+1	.ñn74	8.08 ೪	8,478	8.079	-0.000	8.079	
996.0	83.1	.0107	12.25'	12,239	12.249	-0.000	Ĩ2.250	y
996. ب	83.0	.0128	14,940	14.921	14.930	-0.000	14.931	
996.0	88.9	• 155	18.552	18.52-	18.536	-0.000	18,536	
996. <u>v</u>	82.4	£0203	25,276	25,110	25.153	-0.000	25,153	
996.0	<b>₩1</b> •9	• <sup>1</sup> 24g	32.222	32,43n	32.130	-0.000	32.130	
996.0	51.2	•1759	40,21:	39,971	40.093	-0.000	40.093	
996.ų	80 <b>.</b> 5	.0344	47.821	46,973	47.397	-0.000	47.397	4
996.0	79+6	••396	55.7:4	56,116	55.910	-0.000	55.91ó	
996.0	78.9	• ^436	63.728	63.997	63.663	<b>~0.00</b> 0	63+663	

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 7/8/76

CONTAMINATED CONDITION-FLOW RATE VERSUS

TEST DESCRIPTION

DIFFERENTIAL PRESSURE, TOTAL OF 38.9 mg OF
SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN
(S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL)

TEST SPECIMEN INLET CONDITIONS NET DIFFERENTIAL! PRESS PRESSURE TEMPER , TURE FLOW RATE \*\*\* \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* \*\*\*\* ¥ GNS LITERS/ GN2 KG/SQ CM KG,SQ CM PSIA **ACF**<sup>V</sup> KG/HK DIFFERENTIAL' PSID DEG. K DEG. C DEG. F MIN **SCFM** LBS/HR 70.307 1000.0 31.054 300.0 26.8 80.3 99.7 1426 2,842 5.590 12.338 2.1833 70.029 996. u 299.4 79.2 75.0 55,273 26.2 .0397 2,546 5.210 Ti.487 3,9353 70.029 996. 299,2 26.1 78.9 65.7 . .349 2,325 4.579 10.594 3,3982 48,334 70.029 996.v 299.3 79.1 3.945 26.2 56.3 .0301 2.004 8.498 2.8445 40.454 996,4 70.029 32,551 299.6 79.5 3,285 272885 26.4 46.9 .0251 1.670 7.250 70.029 996. 299.4 26.7 80.0 37.3 0201 1.337 2.632 5.803 1.7604 25', 039 70.029 996.0 300,1 27.0 84.5 n155 5.431 4.478 1,3162 18-720 28.7 1.031 70.029 996.0 390.4 27.3 81.1 1.734 1.0941 Ī5.561 24.4 .881 3.824 ...133 70.029 996. u 300.7 27.5 81.6 1.352 11.806 18.9 .0104 .686 2.980 .8300 70.029 996. - 7.963 27.9 82.2 .949 301.0 13.1 .:073 .482 2.193 .5598 70.029 996.0 301.5 28.4 84.1 .960 2.117 12.7 .9074 .488 .5680 B. 079' 70.029 996.6 301.5 28.4 83.1 .708 1,394 12,250 19.7 .0197 3. 674 .8612 70.029 996 . . . 301.5 2A.3 83. 23.5 . 128 847 1.665 3.677 -- î4.931 1.0497 70.029 996.0 301.4 28.3 82.9 28.5 .0155 1.028 5.055 4-464 1.3632 18,536 70.029 996.L 301.2 28.0 82.4 37.4 .0203 1.343 2,645 5.832 1.7685 ~25', <u>1</u>53' 70.029 996.0 30n.9 ÷7.7 81.9 - "Ť- 189" 46.4 .0249 1,651 3.252 2.2590 32,130 70.029 996.0 300.5 27.4 81.2 55.8 .0299 3.907 1.984 8.514 ' 2.8188 40.093 70.029 996.0 300.1 26.9 80.5 . 4344 4.562 9.925 3,3324 ~47.39<del>7</del>.--64.6 2.286 70.029 996.0 299.6 26.5 79.6 74.6 .0396 5.189 ÏΕ446 -3.7309~ 55.210 2.635 70.029 996.0 299.2 78.9 26.0 5.722 82.4 .0436 2,906 12.615 4:4766 63, 663 \*\*\*\* \*\*\* \*\*\* \*\*\* \*\*\* 70.043 996,4 27.2 300.4 80.0

.026

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• 7

DEVIATIONS

#### FLO4 RATE VERSUS DIFFERENTI L PRESSURE

PAGE: 1 DATE: 7/8/76

TEST WUMBER 11J PART J

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 38.9 mg TO TEST DESCRIPTION SYNTHETIC CONTAMINANT ADDED. TEST SEECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

TEST SPECIMEN INLET CONDITIONS FLOWMETER CONDITIONS 

FLOWING IER ONE			***	FLOUMETER TWO					
FLOW RATE (ACFM)	PRESSURE (PSIA)	TFMP (DEG• F)	FLOW RITE (ACFM)	PRESSURE.	TEMP (DEG. F)	TRESSURE (PSIA)	AVG TEMP (OEG. F)	FLOW RĂŢĘ (ĀCĒM)	ij
•88	47.5	<b>55</b> • ≈	.92	47.4	87.0	410.9	86.4	.105a	-
• <b>7</b> 8	5. je	· 95.3	.81	44,5	86.6	419.4	85.9	.0936	
•69	Dt . 4	84 • 1	.7	49.1	86.5	418.7	85.8	.0830	
• 6 ti	7 • לַּא	β <b>π•</b> }	•69	;8.7	₽6.5	418.7	85.7	.0710	
•51	₽2.4	85.2	•51	49.5	36.7	418.7	85.9	.0605	:
•41	9•9	85 <b>:5</b>	.40	79.3	87.6	418.7	86.2	.0461	น
.31	47.7	R5.8	•30	49.3	87.2	418.7	86.5	.0364	
• Se	5,.2	86+3	• = 5	44.9	87.6	419.4	86.9	. 0308	
• <b>5</b> 5	42.7	86.5	.21	. 9.5	87.8	/19.4	87.2	.0250	
• <u>1</u> 5	45.7	86+8	•14	49.5	87.9	420+0	87.4	.0168	
•15	<u> 47.9</u>	ชว์•ูา	.13	49.9	⊁ B •	421.7	87.5	•0167	ų!
ēss	<u>4</u> 7.9	86 <u>.</u> 8	* - 1	49.5	8841	426.7	87.4	.0256	1)
.27	51	86+5	• >5	49.7	97.9	421.7	87.2	.0308	0
•35	44.7	86.	•31	49.1	A7.8	420.7	87.0	.0370	J
.42	47.7	85.9	•41	49•1	£7.6	42n.n	86.7	• 0483	
•52	44.8	85 • 6	•51	49+3	87.4	419.4	86.5	0603.	
• 00	54.4	85 • 4	•61	49.7	87."	418.7	86.5	.0721	.i
.70	4 . 4	85•4	.71	49.1	84.8	418.1	86.1	. 0836	d
• 79	⊃t • 1	P5.5	•8±	48,3	86.8	417+4	86.2	.0940	
.88	47.9	85.8	.91	47.8	A6.8	417.4	86.3	.1045	

PAGE: 2 DATE: 7/8/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION-FLOW RATES VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 38.9 mg OF TEST DESCRIPTION SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

TEST NUMBER 11J

PART J

TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*

,	• • •							
PŖĘŚŚUŖĘ (PŚĮA)	AVG IEMP (DĘG• F)	₄VG FLOŸ A₄TE (·CF∺)	GROSS DIFF• PRESS PRIMERY (PSIO)	GROSS DIFF. PRESS SECOMPARY (PSIn)	AVG GRUSS DIFF• PRESS (PSIU)	TARE DIFF. PRESS (PSIO)	DIFF. PRESS (PSIO)	j
410.7	ø <b>6</b> ,4	.1058	237.179	237,179	237,179	.002	237.177	
419.4	#5 <b>•</b> 9	. 9J6	183,585	183.585	183.585	•001	183.584	
418.	<b>35•</b> 6	.08 0	151,168	143.168	100.165	.001	150.166	
418.1	<b>5.7</b>	.n71e	118,327	118,327	118.327	.001	118.325	
418.	b5.9	.06 5	93,489	94.367	93.9SF	•000	93.926	
418.	5.24	.0481	68.5 <sup>99</sup>	£₹.147	68.923	•000	68.921	1
418.	₹6,5	.0364	48_433	48,97n	48.702	•000	48,700	
419,2	36 <b>.</b> 9	.0318	40.609	44,323	40.46 <u>0</u>	.000	40.464	
419.4	67.2	•4Sb•	31.77	31,482	31.656	• 0 0 0	31.625	
420.0	07.4	.n168	c.119	19.867	19.993	.000	19,992	
420.1	87.5	.0167	20,119	20.038	20.079	•000	20.077	
420.1	۶7 <u>•</u> 4	. 256	32.637	32.514	32,576	•000	32.574	į,
420.!	87 <u>.</u> 2	B0F0.	40,609	40 • i51	40.495	•000	40,493	
420.1	b7 <b>+</b> 0	.0370	49.309	49.916	49.612	•000	49.611	
420 <u>. y</u>	<b>46</b> •7	·-483	68 <b>.94</b> 8	69.462	69.2115	.000	69.203	
419 <u>.4</u>	<b>∞6</b> •5	.0603	<b>97.64</b> 2	93,491	93.032	.000	93,030	
418.	b6.2	.0721	120,534	120.534	120.534	•001	120.532	
418-1	ზი.1	•• 8.3€	152,059	152. 50	152. 59	•001	152.058	1
417.4	06. ·	•0940	184.846	184.846	184.846	.001	184.845	
417.4	5 <b>6</b> €3	• J n 45	229,613	229,613	229,614	.002	229,611	

PAGE:3 DATE:7/8/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

CONTAMINATED CONDITION-FLOW RATE VERSUS TEST DESCRIPTION SYNTHETIC CONTAINANT ADDED. TEST SPECTMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

TEST NUMBER 11J

P'RT J

NET DIFFERENTIAL PRESS. TEST SPECIMEN INLET CONDITIONS

****	***	***	***	****	****	***	****	***	***	***	***
PRESSY		****	[E':PER · TURE   ###########	****	****	****	FLOW RATE	***	****	•	
KG/SQ CM	PSIA	DEG. K	DEG. c	DEG. F	Lit-RS/ Min	. CFM	SCFM	<b>κቮ∖</b> Ημ <sup>ቮ</sup> ι₄S	GN2 LRS/HR	KG/SQ CM Dif <u>f</u> erentiäl	PŞĪD
28,891	413.7	363.4	3, .2	86.4	81	•1 n5rs	2.868	5.649	12.448	16.6752	237.177
29,484	419.4	303.1	30•:	85.9	73.>	•-1936	2.593	5.100	11.258	12.9072	183.584
29,438	418.5	363.0	29.9	85.8	54.7	.0830	2.295	4 <u>.</u> 51g	9.961	10.5577	150.166
29.438	416:1	3ŋ3.	29.9	85.7	55•1	• 71¢	1.964	3.861	8.526	8.3191	118.325
29:438	418.	303.1	ឌស្⊕ម	85.9	n6.8	.06//5	1,673	3.≥-94	7.262	6.6037	93,326
29.438	418 , <u>(</u>	303.3	34.1	66.2	36.9	.0481	1.330	5•01a	5.772	4.8456	68 <sup>•</sup> XŠĪ
29,438	416.5	3,3,5	34.3	86.5	27.8	364	1.006	J *å8Ť	4.366	3.4240	48.700
29 • 484	419•4	303.7	30.5	86.9	.3•2	.0395	.852	1.675	3 <u>*</u> 700	2.8449	40.464
29 • 484	419,4	3,3.8	37.6	87.2	19.1	.,25.	<b>.</b> 692	1•364	3.004	2.2234	31.625
29.530	420 • -	3ŋ3.9	3n.8	87.4	12.6	• 166	.464	• 915	2.013	1.4056	19.792
29.575	420.1	304.3	30.9	87.5	1 > • 5	.0167	.463	*815	2.011	1,411,6	20.077
29,575	420.5	304.n	34.8	67,4	19.5	.0256	.710	1-59	3,080	2.2902	32.574
29.575	4211.	3,3.8	37.7	87.2	23•6	8080.	.854	1:684	3 <b>.7</b> 08	2.8470	40.493
29,575	42001	303.7	35.6	87.0	28.3	•0 <b>37</b> n	1.025	2•)15	4.450	3.4880	49.211
59 •̃230	420.0	303,6	30.4	86.7	37.>	. 1483	1,337	÷•ី្	5.804	4,8655	69,203
29,484	419.4	303.4	30.3	86.5	46.5	.0603	1.669	3.285	7.245	6.5407	93. <u>03</u> 0
29:438	410.	3,3.3	31.1	86.5	55.9	. 721	1.992	3-924	8+647	8.4742	150.435
<sub>2</sub> 9∙393	418.4	303.	30.1	86.1	65.0	.6836	307ءم	4,543	10:016	10.6907	152.058
29.347	417,4	3,8,8	30.1	86.2	73.1	.094g	2,591	2•í0ì	11.246	12,9959	184, 845
29.347 ****	417.4 *****	3·3·3 ****	30•6 ****	66.3	81.4	•1945	2.879	5 <u>.</u> 670	12•499	16•1433	55 <b>3</b> •ē1 i
29 <u>.</u> 445	41ā+a	303,5	30.3	86.6							
<u>•</u> 084	1.4	•3	• 3	•5	DEVIATIONS	5					

FLOW HATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 7/8/76

TEST NUMBER 11K PART K

TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 53.9 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL)

									•
,	FLOMP: 1ER ONE		***	****	FLO:MFTER TWO	****			
	FLOW RATE	(もゔ゙゙゙゙゙゙゙゙゙゙゙゙゙゙゙゙゚゙゚゙ゔ゚゚゚゚゚゚゚゚゚゚゚゚゚゚゚゚	TEMP (DEG: F)	FLOW RITE (	PRESSURE.	TEMP (OEG+ F)	TRESSURE (PSIA)	AVG Temp (Deg. F)	FLOW RATE (ACFM)
	.86	⊅ <sub>V</sub> 4	65 <u>.</u> 7	• 90	48.3	*0 <b>* 7</b>	1.07.9	48.Z	.0431."
	.78	50.4	65.7	.91	48.7	71.6	1.07.9	68.2	, 6392·
	<u>.</u> 69	5 <sub>2.4</sub>	66+2	•71	48.9	7 9	1'07.9	68.5	• 0344·
	.60	۵۵.۵	65•6	•60	49.1	71.	1 07.9	68,9	.0297
	.50	<u>ታ</u> ፶ • 9	67•4	.50	49.1	71.7	1 -07,9	69,5	.0247
	.41	<sup>4</sup> 2∗7	4F . 1	,41	49,7	5.2	1:07,9	70.1	,0201° ~~
	<u>.</u> 31	Py.1	64.9	.3.	49.7	72.7	1 07.9	70.8	.0153
	•26	45.7	69+8	.,5	49.3	73.3	1 07.9	71.5	.0127
	•21	4×.9	7 -+8	440	49.7	72.9	1 07.9	72.4	.0103
	•15	47.5	75.7	•19	49.3	74.5	1 07.9	73.1	.0070
	.15	20.4	73+2	• 1 4	5 • • 2	75.6	1.07.9	74.4	.0071
	•22	Þγ.1	73.0	• 7 1	49.9	75.7	1 4 0 7 . 9	74.5	.0106
	<u>.</u> 27	49.5	73•ĭ	.26	49.1	75.8	1 07.9	74.5	.0159
	۹3۶	47.7	7~+9	•71	49.3	76.	1.07.9	74,5	.0153
	.42	47.9	72.4	.41	49.3	75.9	1.07.9	74.2	.0203.
	•50	55	71 • 7	•5:	49.5	75.7	1 07.9	73.7	
	160	47.9	71+9	• 60	48.7	75	1 07.9	73.2	.0294.
	,69	ລະ *8	69.9	.70	48.9	74.8	1 07.9	72,4	.0342
	• 7b	45.8	60+1	•91	48.3	74•1	1 07.9	71.6	• 6386-
	.87	₽Č*S	68.5	.91	48.1	73.5	1/07.9	71.0	.0435
							•	•	<b>-</b>

PAGE: 2 DATE: 7/8/76

FLOW PATE VERSUS DIFFERENTI L PRESSURE

TEST HUMRER 11K PART &

TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 53.9 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL)

TEST SPECLMEN INLET COMPITIONS

PRESSUME (PSIA)	υνς 1εμρ (υςG• F)	FLOW RATE (CCFM)	·ROSS DIFF• PRESS PRIM.RY (DSIU)	RRESS SECONDARY (PSID)	AVG GKOSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSIO)	NET Diff• Press (PSID)	
1007.9	00.2	.4431	66,657	67.31H	66*98	-0.000	66.987	
1007.9	58.5	. 342	58,767	59.417	59.194	<b>~</b> 0 • 0 0 0	59.092	
1007.7	ঽ৳•ব	. 1344	49.619	5 .251	49,935	-0.000	49.935	
1007.7	<b>ა</b> ৪.9	.u297	42.247	41.924	42.485	-0.000	42.086	
1007.7	<b>&gt;9∙</b> 5	. 247	33.625	33. 786	33.45	<b>~</b> 0 • 0 0 0	33.457	
1007.9	10.1	.02.1	26,234	25,475	26.484	-0.000	26.084	
1007.7	ļ0.8	.0153	19.011	18,772	18*88\$	-0.000	18.892	
1007.5	/1.5	.^127	15.457	15,226	15.342	<b>-0.000</b>	15,342	
1007.∞₹	12.4	.01 3	12.213	11,769	12. 191	-0.000	12.091	
1007.7	77.1	+0070	7.91	7.746	7.624	-0.000	7,825	
1007.7	f4-4	.0071	7,965	7,974	7.970	-0.000	7.970	
1007:2	74.5	.pl 6	,12,40,	12,426	12.413	-0.000	12 <u>.</u> 413.	
1007.7	14,5	.0129	15,457	15. 97	15.42]	-0.000	15.428	
1007.7	14.5	.0153	19.762	18.715	18.735	-0.000	18,739	
1007+2	14.2	£ S0.	26,233	26.164	26.195	<b>⇔0.000</b>	26,199	
1007.9	13.7	. 1245	२३,62४	33.516	33.574	<b>~</b> 0.000	33.572	
1007.2	13.2	.0294	41.318	41.116	41.21]	-0.000	41.218	
1007-9	12.4	. 342	48.992	49.019	49.396	-0.000	49.306	
1007.9	/1.6	*n 386	57.114	57.8·6	57.424	-0.000	57,424	
1607.7	/1.0	.0435	67,157	67 <b>.</b> 950	67.552	<b>~0.000</b>	67.554	

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 7/8/76

TEST NUMBER LIK PART K

TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 53.9 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000(ESIA (NOMINAL)

(S/N 020) INLET PRESSURE 1000(RSIA (NOMINAL)

TEST SPECIMEN INLET CONDITIONS

NET DIFFERENTIAL PRESS

1	***	***	***	. 1631 ********	NEI DIFLEMENTIAL LAKES								
ń	PRESS		TE:4PER:TURE ****************			****	FLOW RATE					÷ š	
	K@/SQ CM	P\$1 <sub>M</sub>	DEG. K	υE6 ດ	OEG. F	LITERS/ MIN	ACFM	SCFM	KA/HK Gus	Γ¤2∕HB GN3	KG/SQ CM DIFFERENTYAL	₽ަD	J
	70.865	1,07,5	293.3	21	68.2	84 • 1	• 431	2,968	5.847	12.886	4.7 <sub>0</sub> 97	66-787	
	70,866	1807.7	2 <sup>9</sup> 3•2	29.1	68.2	76.4	, 139,	2.699	5,314	11.715	4.1546	59.092	
	70 .865	1007,7	293,5	2,	68,5	66.7	344	2,366	4.65%	10.272	3,5108	49. 335	
•	70.865	1007.7	293.7	24.5	6A.9	57.3	• 1297	2.042	4.020	8.863	2.9589	42.086	
	70.865	1007.7	294.0	20.9	69.5	47.3	• 247	1.692	3,331	7.344	2.3523	33 <b>.45</b> 7	1
	70,865	1007,7	294.4	21,2	7),1	38.3	.3201	1,377	2.711	5,977	1.8339	26.084	ţT
	70.865	1007.7	294.7	21.5	5.27	29 • 1	• * 153	1.047	2:064	4.546	1.3282	18.492	-
	70.865	1007.7	29=.1	22.0	71.5	2, • 1	• 1127	.870	1.714	3.779	1.6786	12-345	
	70 <u>.</u> 865	1007.7	295,6	22.4	72.4	19•3	.0103	.703	1,384	3 <u>.</u> ń52	.8501	12.091	
•	70.865	1701.5	296.4	22.8	73.1	12.9	•9070	.475	•93#	2.060	•3501" "" .	7:425	
	70.865	1007:3	2 <sup>96</sup> •7	23.6	74.4	13.1	.1071	.482	• <b>95</b> 0	2 • 095	•5603	7.270	11
	70.865	1007.7	296,7	23,6	74.5	20 • 9	•91.16	.723	1:425	3.138	•8727.	12.113	v
	70.865	1007:2	296.8	23.6	74.5	24.2	• 129	.876	1.722	3.804	1.0847	12.458	
	70,865	1707.7	296.7	23.6	74.5	28.8	153	1.038	2_044	4.505	1.3175	18,]39	
	70 - 865	1007.2	296.6	23.4	74.2	38.5	• )543	1.383	2.724	6.005	1.8420	26.199	
I	70,865	1007.7	296.3	23.2	7a.7	47.7	• >249	1.697	3•34€	7.369	2.360*****	33-97Z-	
	70.865	1003-3	296.0	22.9	73.2	56.4	• o294	2.007	3.954	8.713	2,8979	41.418	ı
	70,865	1401.5	295.6	?2•4	72.4	65.9	• '34 >	2+333	4.594	10.129	3,4666	49.306	ŋ
	70.865	1007,7	295.1	. 22.3	71,6	74.8	. :386	2,636	5.187	11.441	4,0373	57', 124	
	70.865 ****	1507.7	294•8 ****	21.7 *****	71•?	84•4	• -435	2.976	5•ੁਖ਼6 ′	12.918	4.7495	67.554	
	70 <u>.</u> 865	1007+3	295.2	25.1	71,8								
	•000	• •	1.1	1 • 1	1.9	DEVIATION:	3						

TABLE 92 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

DATE: 7/8/76 CONTAMINATED CONDITION-FLOW RATE VERSUS

PAGE: 1

TEST NUMBER 11L PART L

TEST DESCRIPTION DIFFERENTIAL PRESSURE TOTAL OF 53.9 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

TEST SPECIMEN INLET CONDITIONS. FLOWMETER CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* FLOWME LED ONE

1	****	FLOWME IER ONE			FLOWMETER TWO	***			•	
	FLOW RATE (ACFM)	( <u>651</u> √) 64F3504€	TEMP (DEG: F)	FLOW RATE (ACEM)	PRESSURE.	TEMP (DEG + F)	TRESSURE (PSIA)	ÂVG TEMP (DEG. F)	FLOW RATE (ACFM)	'J
	• 88	#4.p	78 <u>:</u>	.91	47.5	79•8	419.4	79.2	1034	
	• ?9	อก์*1	78.7	.81	48.3	79.9	418.7	79,3	.0937	
	<u>•</u> 69	24.5	78•7	•71	48.8	R +1	418.7	79.4	.0828	
;	•60	ສິດ 🕶	78+9	•60	49.	90.1	418.I	79 <u>•</u> 4	.0717	
	•51	44.9	78.8	•50	49.0	80.2	418.1	<b>79.</b> 5	.0597	.1
	<u>.</u> 41	47.9	78:9	• 40	49.5	en.3	418.í	79.6	.0483.	**
	• <b>3</b> 1	₽ñ.5	79.0	.30	49.8	86.5	418.7	79.8	,¢ <b>367</b> ′ '	
	<u>.</u> 27	<del>1</del> 7.5	79:2	• 56	49 • 2	8 6	418.7	79.9	.0313	
	• 22	20.4	73:4	•sj	30.2	80.8	.,18.7	80.1	.0255	
ť	.14	<b>ນ</b> ິນ • 4	79:6	•1³̃	50.2	8n.8	418.7	80.2	- 6810.	•
	<u>.</u> 14	47.9	79.9	•13	49.6	8].]	419.4	80.5	-0164	y
	• 22	⊐မို • ခ	79 • 9	• 2 j	50.0	81.1	419.4	80.5		•
	• <b>2</b> ?	4¥.9	79 <u>•</u> 8	• 76	49•4	81+1	419.4	80.4	·~ : ē3ĭ4·	
	•32	ង់ពី•ី១	79•5	•=1	49.8	81.1	418.7	80.3	.0375	
	• <del>4</del> 2	÷α•1	79•3	•41	49.4	86.8	418.7	80.1	• 0489	
ı	•51	49.9	79 <u>•</u> 2	•50	48.8	9ñ•8	418.i	80+0		•
	<u>.</u> 60	20.4	79•1	•60	49.4	მი∙მ	418 <sub>*</sub> 1	79.9	•0719	
	• 70	⊐v.5	79.2	.71	48.8	81.7	417.4	79.9	.0835	4
	<u>.</u> 78	5 /+ J	79•2	:81	48•3	8r • 6	476.8	79.9"	. 6939	
	. 88	47.7	79•7	•91	47.7	80.6	416.i	80.1	.1044	

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2

DATE: 7/8/76

TEST NUMBER 11L PART ( TEST DESCRIPTION SYNT'E

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE TOTAL OF 53.9 mg OF SYNTIETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

TEST SPECIMEN INLET CONDITIONS

							****	
PRESSUME	AVG TEMP (DEG. F)	FLOW RATE (ACFM)	GROSS DIFF. PRESS PRĪMARY (PSID)	gRass DIFF. PRESS SECONDARY (PSID)	AVG GHOSS DIFF. PRESS (PSID)	TARE OTFF. PRESS (PSID)	DIFF PRESS.	ıı
419.4	19.2	.1034	257 256	257,256	257.256	.005	257,254	_
418.	19• <u>3</u>	.,,937	206,752	206.752	500.125	.001	206•750	
418.1	19-4	•n8 8	165.086	165.086	165.086	.001	165.084	
418.1	19.4	a 0717	130.364	131,364	130.364	.001	130.363	
418.1	19.5	. 4597	99,430	99,430	99.430	.000	99.429	
418.1	(9•6	.0,83	73.063	73.5 7	73.305	•000	73.303	J.
418.	79.8	.0367	51,311	52, 983	51,697	.000	51,695	
418.1	19.9	.0313	43,177	42,918	43.042	•000	43,041	_
418.1	#4. <b>•1</b>	. 1255	33,441	33,244	33.343	•000	33+341	
418:	80.S	.0166	20.444	20.178	20.911	•000	S0 - 309·	_
419.4	- ៦0•5	.1164	800.05	19,949	19.979	-0.000	19 <u>-</u> 977	
419.2	8ე.5	.0260	34.248	34.1 6	34.17!	•000	34.176	4
419.4	80.4	.0314	42.805	42.562	42.683	.000	42.682	
418.	80.3	.,376	52,312	53,29	52.671	•000	52,669	
418.	on <u>.</u> 1	. 6489	73,815	74.494	74.152	•000	74.150	
418-1	~ 0.0	.0598	98,483	93.487	98,483	•000	98.482	
418.4	19.9	. 11719	130.048	130.048	130.048	.001	130.047	•
417,4	19.9	. 1835	166,033	166.033	166.033	.001	166.031	1
416.8	19.9	• 1939	>07.067	o07.067	207.067	.001	207,066	
416.1	۵0 <b>.</b> 1	.1044	271.776	271,776	271.776	.002	271,774	•

LARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM) +2 +

0 (ACFM) \*\*3

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 11L PART L

TEST DESCRIPTION

CONTAMINATED BONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE TOTAL OF 53.9 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

PAGE: 3 DATE: 7/8/76

		NEŢ DIFFEREN	TEST SPECIMEN INLET CONDITIONS											
,			****	****	FLOW RATE	***	*****	***	TEMPER:TURE	***		PRESSU		
S T D	(L PI	KG/SQ CM Differentiāl	GNR LBŠ/HR	KĞ∖HŔ Ğ⋈≶	scĘM	4CFM	LITARS/ MIN	DEG. F	DEG. C	UEG. K	PSIA	KG/SQ CM		
, ਟ54∙	257	18.0868	į2 <u>.</u> 582	5.70!	2,899	•1034	82•0	79.2	26.2	299.4	419.4	29 <u>.</u> 484		
,750	206	14,5360	11:383	5.165	2.622	.0937	74.1	79.3	<b>≈6.3</b>	299.4	418,5	29 <u>•</u> 438		
, <u>0</u> 84	165	11.6066	10.059	4.563	2,317	.v828	65.3	79,4	26.3	299.5	418,1	29 438		
`3ē3 -	130	9.1654	8,699	3 <u>•</u> 949	2.004	•11717	56 • a	79.4	26.4	299.5	418	29.393		
129	997	6,9905	7 <u>•</u> 237	3 <u>•</u> ⊳8⊴	1.667	•0597	46.6	79.5	<b>96∙</b> 4	799 <b>.</b> 5	418.L	29 • 3 § 3		
ğoż	73	5,1537	5,851	2.654	1.348	. 3483	37,3	79.6	26.5	299.6	419.1	29,393		
<u> </u>	51.	3.6345	4 • 457	2•42€	1.027	• 1367	28.3	79.8	<b>≽6</b> •5	299.7	418.	29.438		
041	43	3.0261	3 <u>*</u> 805	1.720	.876	./313	24•Z	79.9	<b>76.</b> 6	299.8	418.5	29 • 438		
341	33.	2,3441	3.088	1 • 4 0 1	.711	.0255	19.6	B∩.1	26.7	299.9	415.5	29.438		
¥08	.20	1.4279	2,020	2912	.465	• 166	12.6	8: •5	26.8	299.9	416,5	29,438		
777	19	1.4045	1.996	<u>.</u> 905	.460	.0164	15.5	80.5	÷6.9	300.1	419.4	29,484		
<u>176</u>	34,	2.4028	3,160	1.434	.728	.026^	20.0	8g.5	26,9	300.1	419.4	29 484		
ĕ85	42.	3.0008	3.811	1:727	.878	• 314	24•2	84.4	26.9	3ây <b>.</b> 1	419.4	29.484		
669	52	3•7030	4.563	2 <u>*</u> 070	1.051	• 0376	29•1	89.3	26.4	300.0	418.	29.438		
, <u>1</u> 50	74,	5,2133	5.930	> <b>∓</b> ēāā	1,366	.0489	°7•9	80.1	s6.7	299.9	418.5	29,438		
¥8Š	~. 98.	6.9240	7.240	3,284	1,668	.0598	46.5	80.0	26.7	299.9	418,1	29.393		
047	130	9.1432	8.708	3.950	2,006	• J <b>7</b> I 9	56 <u>•</u> 2	79.9	, 26.6	299.8	416.1	86•363		
031	166	11.6732	10.098	<b>4</b> •580	2.326	. 1835	65•5	79.9	26.6	299.8	417.4	2 <sup>9</sup> •34?		
åēē	267	14.5582	11.345	5 <u>•</u> 149	2,613	.11939	73.8	79,9	26,6	8,668	416.5	29.302		
374	27)	19+1976	12.585	5 <u>•</u> ?₀¤	2.899	•1044	85-0	ម៉ូ೧•1 *****	26.7	299 <b>.</b> 9	416•1 ****	29 • 256 *###		
								79.9	26.6	299.8	41គ <sup>ី</sup> 4	29.416		
							DEVIATIONS	•3		•2	. 0	<u>•</u> 046		

PAGE: 1 DATE: 7/8/76

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 11M PART M

CONTAMINATED CONDITION-FLOW RATE VERSUS
DIFFERENTIAL PRESSURE, TOTAL OF 67.3 mg OF
SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN
(S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL)

FLOWMETER CONDITIONS	TEST SPECIMEN INLET CONDITIONS
<sup>我我我我我我我我们的我们的我们的我们的我们的我们的我们的我们的我们的我们的我们的</sup>	<b>图像存在现在中央中的工作的工作的工作的工作工作工作工作工作工作工作工作工作工作工作工作工作工作工</b>
, , , , , , , , , , , , , , , , , , , ,	

FLOWMCIER ONF			***	FLOWMETER TWO	<b>****</b>		·	**		
FLOW RATE	PRESSURE (PSIA)	TEMP (DEG <u>*</u> F)	FLOW RITE (ICFM)	PRESSURE* (PSI4)	TEMP (DEG • F)	CRESSURE (PSIA)	AVG TEMP (DEG. F)	AVG FLOW RATE (ACFM)		
•87	44.7	74 ° 6	.91	47.5	92+1	1:07.9	79.3	. ŏ42 <del>7</del>		
<u>.</u> 78	añ.S	76:1	.81	48.5	P1.5	1004.0	78,B	.0391		
<u>.</u> 69	5:4	75•9	+71	48.A	<b>~</b> 1•2	1 04•n	78.5	.0346		
• 60	5ÿ.1	76+1	•60	49.0	91.3	1 04.0	78.7	•0296·		
•50	ង់តី <b>•</b> 1	76.7	.50	49.0	81.5	1004.0	79,1	8450.		
.41	⊃4.4	77.3	.40	49.a	4) <b>.</b> A	1:04.0	79.6	£oŝo,		
•31	44.8	78.3	.30	49.4	82.4	1004.0	80.3	.0152 "		
•se	49.5	7950	• 25	49.0	82.7	1004•n	81.B	.0126		
• 22	47.5	79•5	1	49.2	P3• 1	1.04.0	81.3	.0105		
<u>•</u> 14	47.5	8: •4	.13	49.2	83.5	1007.9	81.9	-, 0 <sup>-</sup> 067		
•14	56.4	8ì•6	•13	50.2	n4.3	1107.9	83.0	.0069		
•53	47.5	81 • 5	• 25	49.0	<sup>14</sup> 4•3	1007.9	82.9	.0109		
• 26	44.5	£•78	• 25	49.	-4-4	1.07.9	82.8	.0125		
*35	⊃ບໍ•ິ່ງ	81+1	1	49 • 8	84.4	1007.9	82 <b>.</b> 7	.0154 °		
<u>.</u> 41	47.7	8n•4	.40	49.0	84.1	1007.9	82.3	.0200		
•50	42.5	79•4	•50	48.5	83.7	1.07.9	81.6	0244		
<u>.</u> 60	50.1	78•=	•60	49.0	8 <sub>2•</sub> 2	1104.0	80.8	.0295		
•69	5 ų . 4	77•4	.71	48.8	82.4	1004.0	79.9	.0346		
<u>•</u> 78	pi.S	76 <u>*</u> 8	•81	48 • 5	81•B	1.04.0	79+3			
.87	±9.,7	76•0	.91	47.5	81.2	1004.0	78,6	~.0431¯		

PAGE: 2 DATE: 7/8/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PART M

TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS
DIFFERENTIAL PRESSURE, TOTAL OF 67.3 mg OF
SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN
(S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL)

TEST SPECIMEN INLET CONDITIONS

TEST NUMBER 11M

PRESSURE	AVG LEMP (DEG. F)	,VG FLOW RATE (:CFM)	çRASS DIFF. PRESS PRIMARY (pSID)	GRASS DIFF. PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRES (PSID)
1007.4	19.3	.0427	71,193	71.774	71,483	-0.000	71,484
1004 <sub>9</sub> v	/8 <u>+</u> 8	•/391	63,(74	63,577	63.325	<b>~</b> 0.000	63,326
1004.9	18.5	• (* 746	53,562	54.119	59.841	-0.000	53.8 <u>4</u> 1
1004.4	78.7	.0296	45_096	44.867	44,981	-0.000	44,982
1004.0	(9+1	. 248	36,172	35.887	36.030	-0.000	36,030
1004 • v	[9 <u>*</u> 6	£050.	28.1.1	27.9 P	28.n3 <u>4</u>	-0.000	28.035
1004.4	80.3	.9152	20.008	19,835	19,921	-0.000	19.922
1004.9	¤0.8	.0126	16,081	15,835	15 <b>.</b> 95ខ្ព	-0.000	15.958
1004.0	Þ1.3	.9105	12.962	12.81%	15.886	-0.000	15.886
1007.7	01.9	•0057	7,965	7.795	7.879	-0.000	7.880
1007.7	0.E¢	.0069	7.993	7.9 7	7.905	<b>~0.00</b>	7.905
1007.7	~2 <u>.</u> 9	•0109	13.395	13,300	13,389	-0.000	13.390
1003.5	82 <u>.</u> 8	.1125	15,717	15.66,	15.685	-0.000	15,685
1007.7	82.7	.0154	19,946	19.892	19.919	<u>~</u> 0.000	19.919
1007.7	82.3	.nzuo	27.166	27, 148	27.107	-0.000	27.107
1007.4	¤1 • 6	• · 244	34.93:	34,853	34,492	-0.000	34,892
1004,4	ងប•្ន	•n295	44.167	43.945	44.050	-0.000	44.056
1004.4	19.9	.0346	53,061	53,8.4	53.433	-0.000	53,433
1004.0	19.3	•485	62.448	62.947	62.697	-0.000	65 • 63B
1004.9	18:6	.64 11	72,065	72,720	72.39Ž	<b>~0.00</b>	72+393

LARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM) ##2 +

0 (ACFM) \*\*3

PAGE: 3 DATE: 7/8/76

FLOW PATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 114 PART W

TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL FRESSURE, TOTAL OF 67.3 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 FSIA (NOMINAL)

\_\_\_ --

NET DIFFERENTIAL PRESS TEST SPECIMEN INLET CONDITIONS PRESSURE TEMPER TURE FLOW RATE \*\*\* \*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* GN2 GN2 KG/SQ CM LITCHS/ KG/HK DIFFERENTIAL KG/SQ CM p51A DEG. K DEG . . DEG. F MI / CFM SCFM LBS/HR PS.D 2.879 70.865 1007.7 299.4 79.3 5.665 51.0258 26.3 81.7 . 427 12.496 71.484 70.586 . 1391 î1,401 1004.0 299.2 26.0 78.8 74.5 2.626 5-171 4.4522 63,326 53,541 70.586 299.0 78.5 4.573 1004.6 25.8 65.5 .0346 2.323 10.0B2 3.7854 . 296 70.586 1004. 299.1 25.9 78.7 55.9 1.987 3.914 44,982 " 8.625 3.1625 70.586 1004.0 299.3 26.2 79.1 46.6 - 394B 1,666 3.280 7.232 2.5332 36,030 70.586 1004,0 299.6 26.4 79.6 37.9 .02.)3 1.363 2.685 5.919 1.9710 28,035 70.586 1004.9 26.8 .0152 1.018 19, 722. 300.0 Bu.3 28.2 2.004 4.419 1.4006 70.586 1004.7 27.1 8,18 15:958 300.3 23.2 · (126 .84( 1.654 3.647 1.1220 .699 70.586 1004.9 300.5 77.4 19.4 1.37/ 12,586 81.3 .0135 3.035 .9060 70.865 1007.7 27.7 .0067 .452 •660 7.580 300.9 81.9 12.3 1.963 .5540 70.865 1.07.7 29.3 • 1069 .900 7.905 311.5 83.4 12.6 .460 1.997 .555B 70.865 1007.7 301.4 .0109 .9414 13,390 2A.3 82.9 .730 1.435 3.171 20.2 70.865 1007.2 28.2 301,4 8.58 23.1 . .. 125 ,837 1 • 945 3.634 1.1028 15,085 70.865 1607.7 3.1.3 28.2 82.7 28.6 . 1154 1.030 2.127 4,473 1.4004 19,919 70.865 1007.3 27.9 301,1 8:.3 37.3 .0200 1.339 2.23( 5.813 1.965B 27,107 70,865 1007.2 300.7 27.5 81.6 45.8 .0244 1.639 3,220 ...34.092 7.116 2.4532 70.586 1004.0 300.3 27.1 ar.a . 1295 1.973 3.485 3.0975 55.5 8.567 44,056 70.586 1904.0 299.8 79.9 .4346 >.319 26.0 65.4 4.56 3.7567 10.069 53.433 70.586 1004.9 299.4 26.3 79.3 .0394 74.1 5.15V 62,098 2,615 11.353 4.4081 70.586 78.6 . 1431 2,896 1004. 299.0 25.9 82.1 5.703 5.0897 72,393 12,573 \*\*\* \*\*\* \*\*\* \*\*\* \*\*\* 70.698 1005,0 300.2 27.0 80,6 .134 DEVIATIONS 1.7 • H • F3 1.4

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 11N PART N

TEST DESCRIPTION

PAGE: 1 DATE: 7-8-76

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE TOTAL OF 67.3 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

FLOWMETER CONDITIONS

TEST SPECIMEN INLET CONDITIONS

****	FLOWMLIER ONE	***	***	FLOWMETER TWO	<b>የ</b> ቀተ የተ ቀ ቀ ቀ ቀ ቀ ቀ ቀ ቀ ቀ ቀ ቀ ቀ ቀ ቀ ቀ ቀ ቀ			*** **
FLOW RATE	PRESSURE (PSTA)	Temp (DEG: F)	FLOW RATE (4CFM)	PRESSURE.	TEMP (DEG• F)	TRESSURE (PSI <sub>4</sub> )	AVG TEMP (DEG F)	FLOW RATE (ACEM)
•83	5ú*5	ន្ទ5 •្ទ5	•86	48.3	84+3	4Î6•8	85.9	• 0997
• 79	50.4	85.6	.81	48.7	R6.5	416.1	86.0	.0952
•70	50.4	85•4	•71	49•	86.5	416.1	86.0	.0840
<u>•</u> 61	47.5	95•4	•6l	,8 <u>.</u> 7	86.7	416.1	86.0	.0717
• <del></del> 51	ລຄ້*ຮ	85.4	•50	49.4	B6.7	416.8	86.1	• 0 <u>6</u> 05'
<u>.</u> 41	5 · 2	<b>6</b> 5•្5	0 ۵ •	49.4	87.3	A16.8	86.2	.0488
<u>.</u> 31	4X+9	85.9	•30	49.4	87.2	415.B	85.6	.0354
•27	4×.9	86 <u>•</u>	• 25	49 • 4	87 • 4	416.8	86.7	.0309
•ss	5, ñ⊊	85•=	•51	æ0.0	B7.6	417.4	86.9	.0254
<u>.</u> 15	⊃v • 4	86.6	•1 <u>4</u>	50.2	87.9	417.4	87.2	.0172
<u>•</u> 15	20.5	87 <u>•</u> .•	•13	50+0	<b>88</b> •2	41B.1	87.6	.0169
· • Sã	47.7	#6•9	•21	49 • 5	P8.1	418.1	87.5	.0560
<u>.</u> 27	42.7	86:7	<del>4</del> ې 5	49•2	88.1	418.í	87•4	<u>.0308</u>
<u>.</u> 32	4X.9	86+5	-31	49.0	H8• 1-	418.1	87.2	10376
<u>•</u> 42	47.9	86.2	.40	49.2	87 <b>.</b> 9	417.4	87 <u>•</u> 0	<sub>2</sub> 0486 <sup>—</sup>
•51	4×.9	85.9	•5¤	48.8	87.7	417.4	86.8 '	, 0598
<u>.61</u>	6×.7	B≈≛B	•61	∠8.7	87.5	¢16.8	86.6	.071s
• 70	47.9	85.7	.71	48,5	87.4	416.1	86.6	.0830
• 78	47.9	as • 9	<u>•</u> 8)	48.3	87•3	415.5	86+6	
*83	42.7	86•3	•86	47 • 7	87.2	415.5	86.7	6993 T

# TABLE 94 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7-8-76

TEST NUMBER 11N PART N TEST DESCRIPTION SYNTH

CONTAMIMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE TOTAL OF 67.3 mg OF SYNTHETIC CONTAMINANT ADDED, TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

1501	SPECTIFIE	INCEL	CONDITIONS
***	***	***	****

PRESSURE (PSIA)	AVG LEMP (DEG. F)	AVG FLON RATE (.cem)	GROSS DIFF. PRESS PRIMARY (PSIO)	GRCSS DIFF• PRESS SECONDARY (PSIA)	AAG GHOSS OILL HHESS (ball)	TARE DIFF. PRESS (PSID)	NET DIFF• PRESS (PSIO)
416.0	b5 <b>,</b> 9	.0947	292,875	292,875	\$92 <b>.</b> 875	.001	292,873
416.1	۰ و ۵۵	• * 952	255,674	≈55 <b>.</b> 674	255.674	•001	255-673
416•Į	¤6≗≬	•0846	195,145	195.1.5	195.145	.001	195:143
416 <u>.</u> 1	90.0	. 2717	147,541	147,541	147,541	.001	147,539
416.5	¤6•1	.06 S	112,547	112.547	112.54/	• 0 0 0	112.546
416.0	06 <u>.</u> 2	.0,88	32,116	82.282	A2.199	.000	82 <b>.</b> 198
416 <u>.</u> p	٥6 <u>•</u> 6	.0364	55,566	55 <sub>.</sub> 8 . <sub>l</sub>	55,683	•000	55,682
416 <sup>8</sup> 8	56.7	.0349	46,024	45,732	45.875	.000	45 <sub>8</sub> 877
417.4	46•9	. 254	35,924	35,657	35.791	•000	35.789
417:4	87.2	.0172	22,686	24,452	22.517	+000	22.517
418.1	<b>07.</b> 6	.0169	22,312	22,237	22.275	•000	22.273
418.1	5 <u>•</u> 5	• 026.	36,793	36,635	36.714	•000	36,712
418.1	67.4	•0 109	45,467	45. 13	45•34 y	.000	45,339
418et	57.2	, 6376	57,319	57,692	57 <b>.</b> 505	•000	57.5 <sub>0</sub> 4
417.4	67 <u>•</u> 0	·n486	80.263	80.716	80.485	.000	80.483
417.4	56 <b>∙</b> 8	•05 <sup>9</sup> 8	109,710	109,710	109.710	.000	109.708
416.5	¤6 <b>,</b> 6	.0715	145,964	145.964	145.964	•001	145.963
416:1	46•€	• 664 •	189.785	169.785	189.785	•091	189.784
415.5	86.€6	.0939	>45.586	>45.5m6	245.589	.001	245+585
412-3	b6.7	.1993	296,342	296,342	296.342	.001	296,341

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER LIN PART N

.047

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TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE TOTAL OF 67.3 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

7-8-76

PAGE: 3

DATE:

TEST SPECIMEN INLET CONDITIONS " 'NET DIFFERENTIAL PRESS \*\*\*\*\* PRESSURE FLOW RATE TEMPER TURE \*\*\*\* \*\*\*\*\*\* \*\*\*\*\* 6N2 GNS KG/SQ CM LITHRS/ SCFM KG/SQ CM PSIA KĞŹĤĶ DIFFERENTIAL' DEG. K DEG. F MIN ACEM LBS/HR PSID DEG C 29.302 415.0 65.9 77.4 . 997 2.745 20.5910 292.473 3 3.1 29.9 5 404 11.914 29.256 416.1 17.9756 255.973 303.0 30.0 36. n 73.8 .0950 2.615 5.150 11:354 29,256 416.1 303.1 30.0 86.0 64.9 .0840 2.309 4.54! 13,7199 195,143 10.024 29.256 416.1 3,3.2 30 ... 86.5 55.2 .:717 1.971 3.881 8.557 10.3730 147.539 29.302 410.0 7.9127 30.0 86.1 46.5 .0605 1.665 3 - 277 7.229 112.546 303.2 29.302 .0488 5,7791 416,9 3-33.3 86.2 37.1 1.342 2.645 82,198 30.1 5.826 29,302 416.0 55',082 3.3.5 3.1.3 27.6 . 9364 1.970 3,9148 86,6 4.344 1.001 29.302 416.5 45.577 303.6 84.7 .0369 .848 1.071 3.683 30.4 3.2254 3.3 29.347 417,4 86,9 .0254 1.375 35, (89 363.7 30.5 19.3 .700 3.038 2,5162 29.347 417.4 3,3.8 3/.7 87.2 12.8 .473 .934 2.055 1.5831 -52.517. . 172 418.1 29.393 304.1 30.9 87.6 1 .. 6 .0169 .466 791! 1.5660 22.273 2:021 29,393 418.1 304.5 30.8 87.5 19.6 . 126, .715 1.40! 3,102 2,5811 36,712 29.393 418.1 3:3.9 87.4 .850 1.675 45.339" 34.0 23.4 .0309 3.689 3.1876 29.393 410.1 3.3.8 87.2 28.7 57.504 30.1 . 4376 1.036 2:040 44498 4.0429 417.4 29.34 20.0 87.0 ,0486 1,338 2.634 5,6585 80.483 303.7 77.1 5.808 29,347 417.4 .0598 1.647 363.6 30.4 86.8 45.9 3.244 7:7133 199; 708: 7.151 29.302 410.0 3:3.5 30.4 86,6 1.965 3.870 145,263 55.1 ...715 8 . 531 10.2622 29.256 416.1 86.5 363.5 64.1 .0830 2.277 9.886 189./84. 36.3 4 • 48 4 13.3431 415.9 2,574 29,210 86,6 303.5 34.3 77.8 .0939 5.065 11.172 17,2663 245, 985. 29.210 415.0 3:3.6 30.4 86.7 75.7 .0993 2.720 5.357 20.8349 296.341 11:807 \*\*\* \*\*\*\* \*\*\* \*\* \*\*\* 29.311 410.4 303.5 30.4 d6.7

DEVIATIONS

.4

TABLE 95 FLOW RATE VERSUS DIFFERENTIAL PRESSURE PAGE: 1 \_\_\_\_\_. DATE: 7-8-76

PART n TEST NUMBER 110

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE versus
DIFFERENTIAL PRESSURE. TOTAL OF 83.5 mg
OF SYNTHETIC CONTAMINANT ADDED. TEST
SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL)
TEST SPECIMEN INLET CONDITIONS
SECRET SPECIMEN INLET CONDITIONS

FLOWMETER CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*

******	FLOWN LER ONE		***	FLO4METER T40	***			The state of the same
FLOW RATE	PHESSURE (PSIA)	TEMP (DEG• F)	FLOW RATE (ACFM)	PRESSURE. (PSIA)	TEMP (DEG. F)	YRESSURE (PSIA)	AVG TEMP (DEG. E)	FLOW RATE (ACFM)
.86	Pu . 1	7' :3	•91	47.9	76.1	1015.9	73,2	7.0427
.7e	⊅v.2	74.0	.81	48.5	75.7	1015.9	72,8	.0386
• 69	àu*S	70:1	•70	48.7	75.5	1 15.9	72.8	, 0338
<u>.</u> 60	5y.1	7 * • 4	.61	29.l	75.5	1715.9	72.9	.0596
<u>.</u> so	4¥.9	70-9	•50	49-1	75.8	1,11.9	73.3	.0246
<u>,41</u>	47.9	71.6	. 40	49.3	76.2	1.11.9	73.9	.0500
•31	47.9	72.6	•3	49.5	76.7	1111.9	74.6	ozro
.z.	50°5	73.1	4;6	50.1	77.1	1 11.9	75.0	.0129
• 22	ခ <b>်</b> ဂီ ၂	73.8	.21	49.9	77.4	1011.9	75.6	.0104
<u>.</u> 15	49.5	74:5	• 54	49.3	77.8	1 15.9	76.1	.0071
•15	#¥ • ?	761 .	•14	₹9•5	78.9	1 15.9	77.6	.0071
•55	₽₩.1	76.2	.21	49.9	79.0	1015.9	77.6	.0108
<u>.</u> 27	17.7	76•	.26	49.3	79.1	1 15.9	77.5	0158.
•35	4½.5	75.7	• 31	49 . 3	79.1	1 15.9	77.4	.0151
•41	4¥.7	75-1	.40	49.1	78.8	1715.9	76.9	.0198.
<u>.</u> 51	5,,.2	74+2	•51	49.5	78.5	1 11.9	76.4 -	
<u>•</u> 60	50.2	73•4	•61	, 9 • 1	77.9	1,11.9	75.6	.0296
<b>.</b> 69	⊅v.2	72.7	.71	48.9	77.2	1"11.9	74.7	.0344
• 78	5 .2	71 • 4	•81	48.5	76.5	1 11.9	73.9	. 0386
.87	<b>⊃</b> ( •1	7 •5	•91	47.9	75.7	1 111.9	73.1	.0430

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 110 PART 5

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 83.5 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL)

PAGE: 2

DATE: 7-8-76

TEST SPECIMEN INLET CONDITIONS

PRESSURE (PŠĨA)	AVG TEMP (DEG. F)	"VG Flow Rate (~CFH)	ARDŞS DIFF: PRESS PRÎMDRY (PSID)	GRNSS DIFF• PRESS SECONDARY (PSID)	AVG GROSS DIFF. PRESS (PSIO)	TARE DIFF. PRESS (PSID)	NET DIFF: PRESS (PSIQ)
1015.7	(3.2	.0427	77.951	78,597	78.274	<b>~</b> 0.000	78,274
101255	(2.8	•n386	67,49	68,496	67.995	<b>-0.000</b>	67,993
1015.7	12.8	.0328	56.607	57.449	57.028	-0.000	57.028
1012.7	12.9	.n296	48 645	48,295	48,47v	-0.000	48,470
1011-5	/3+3	. 1246	38,192	37.89n	38.041	-0.000	38.041
1011,9	(3:9	.0200	29.388	29.1:4	29.211	-0.000	29,211
1011-3	14.6	.0150	20,688	20.490	20.589	-0.000	20,589
1011.7	75.0	.1129	17,327	17,113	17,220	-0.000	17.220
jujjėž	/5 <sub>2</sub> 6	-01-4	13,413	13,226	13.414	-0.000	13,314
1015.7	/6 <u>∗</u> 1	.0071	8,788	8,669	6.723	-0.000	8,723
1015.¥	17.6	.0071	8,725	8.716	8 <b>.</b> 720	-0-000	8,721
1015.7	17:16	.01-8	13,991	13,911	13,906	-0.000	13,906
júj2°ă	/7 <u>.</u> ≈	.0128	17.014	17.056	17.036	<b>~0.00</b> 0	17.036
roie <sup>™</sup> X	(7 <sub>±</sub> 4	.0151	20.875	20.891	50*883	-0.000	20.883
1015.7	<u>(6.</u> 9	·1198	28,891	28.8 4	28,845	<b>₩0</b> •000	28.848
1011 <sup>5</sup> ā	16.4	.0250	48,750	38,639	38,694	-0.000	38.694
1011-7	15.6	.4296	48,089	47,663	47.875	<b>⇔0.000</b>	47.876
1011:9	14.7	• 344	57,484	58,396	57.940	+0.000	57.940
1011.7	13.9	•11-å <b>9</b> -0	67.740	68.496	98° j1≅	-0.000	68.118
1011.7	13.1	.0430	79,066	79,860	79.463	-0.000	79.463

LARE DIFF. PRESS = -1.64000E-04 + -1.26930E-02 (ACFM) + 2.48070E-01 (ACFM) ##2 +

0 (ACFM)##3

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST NUMBER 110 PART O

•139

200

• 13

• 8

1.5

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 83.5 mg. OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA

PAGE: 3

DATE: 7-8-76 -- -----

(NOMINAL) NET DIFFERENTIAL PRESS TEST SPECIMEN INLET CONDITIONS 444444444444444444 PRESSURE LEMPERSTURE FLOW RATE \*\*\*\* \*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\*\*\*\*\*\*\* LITERS/ GNZ GNS KG/SQ CM PSID. KG/SQ CM PSIA MIN **ACFM** SCFM K@\HŬ LBS/HR DIFFERENTIAL DEG. K DEG\_ C DEG. F 5,781 5',5732 78,274 71.423 1,,15,7 296.1 22.9 73.2 83.5 . .427 2.936 12.746 4,7804 1015.7 295.9 22.7 2.655 57.993 71.423 . :386 72.8 75•4 5:22! 11:523 4.0095 71.423 1015.3 295.8 22.7 65.7 .0338 2,326 4.572 10.095 57, 025 72.8 71.423 1,15,7 295.9 7.55 72.9 57.2 . :296 2.033 4.002 8.824 3,4078 48-470---1,682 71,144 1011.7 296.1 27. 47.2 . .246 3.317 7.300 2.6746 38,041 73.3 71.144 1011.7 296.4 23.3 73.9 38.1 .0200 1,366 5,690 5.930 2,0538 29.211 74.6 4.432 .50<u>. 5</u>86. ... 71.144 1011.7 296.8 23.7 28.4 .0150 1.021 2,010 1.4476 1011.7 297.1 71,144 23.9 .882 1.732 1.2107 17:220 75.J 24.5 a: 129 3.827 71.144 1011.7 297.4 1.39 .9361 24.2 75.6 19.6 .0134 .710 3 • 080 13,314 1015.7 71.423 297.7 24.5 . 071 .483 \*32 F 2.097 .0133 8.723 76.1 13.2 71,423 1015.7 298.5 77.6 .0071 .484 956 2,099 8,721 25.7 12.2 .6131 3:192 1015.7 71.423 298.5 25.3 77.6 20.4 .0118 .735 1.445 .9777 134906 71.423 1015.7 298.5 25.3 77.5 24.1 . 128 .871 1:710 3.783 111978 17,036 71.423 1415.7 298.4 25.2 77.4 -28-8 . :151 1.032 2 034 4.481 1.4682 50-783. 71.423 1015.7 298.1 35 · 1 76.9 37.7 • 719B 1.350 2.657 5.862 2,0282 28.048 71.144 1011,7 297.8 24.6 76.4 47<u>.</u>8 .0251 1.702 3,354 7:390 2:7205 36, 594. " 71.144 1/11/2 297.4 3,965 47.476 24.2 75.6 56.8 . 296 2.15 8.747 3.3660 71.144 1011.7 296.9 23.7 74.7 66.3 . 1344 >.345 4.01 10.179 4.0736 57.740 71.144 1011.7 296.5 23.3 73.9 74.7 . .386 2,637 5.195 4.7892 68,116 11.449 71.144 1,11.7 296.0 2,945 5.794 27.8 73.1 83.5 . /-43n 12.784 5.5868 791163 \*\*\* \*\*\* \*\*\* \*\* \*\*\* 71,283 1013.9 297.1 23. . 75.1

DEVIATIONS

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

Page: 1 Date: 7/8/76

TEST NUMBER 11P PART P TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS
DIFFERENTIAL PRESSURE TOTAL OF 83.5 mg OF
SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N
020) INLET PRESSURE 415 PSIA (NOMINAL)

FLOWKETER CONDITIONS ' TEST SPECIMEN INLET CONDITIONS \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* ELOWN LED ONE

***	FLOWNLIER ONE	***	***	FLOWMETER TWO	***			
FLOW RATE	PHESSURE	TFMP (DEG: F)	FLOW RATE	PRESSURE, (PSIA)	TEMP (DEG. F)	TRESSURE (PSIA)	AVG TEMP (DEG. F.)	FLOW RATE (ACFM)
ées	47.A	81.	<b>-</b> 85	47•9	87•8	417.4	82.2	•0976
•,79	2.7.5	81.5	.81	48 ,5	82.5	415,5	82.0	70948
• 70	2: •5	81 • 3	•7 L	48.9	42.5	415.5	81.9	• ō937
<u>•6</u> 0	5v.2	8121	-60	49•3	47.5	435.5	81.8	•0723
• <u>,</u> 51	44.7	81.1	.51	48.9	88 <b>.</b> 5	415.5	81.8	10606
·42	5y.1	81+1	-40	49.5	87.5	415.5	81.8	•0791
<sup>6</sup> 35	47.9	81.1	•31	49.5	87.5	415,5	81.8	0374
šsi	5v.1	81.5	.25	49.7	A2.7	415.5	B1.9	.0311
•ss	20.5	41:3	• 20	49.9	82.7	415.5	82.0	EZS0.
<u>•</u> 15	79.4	81.5	.14	50.2	62,7	415.5	82.1	" ;7173"
,15	Do . 4	81+6	•14	5*•2	£2.9	416.j	82.3	.0173:
· • 55	20.5	81 • 6	.51	49.9	82.9	416.1	82.2	.0262
.27	44.7	8 • 4	• 56	49.3	82.7	416.1	82.0	.0311
•35	49.9	81 <b>•</b> 3	:31	49.5	8~•7	416.1	82.0	.0376
,42	àñ*5	81.0	.41	49.9	P2.6	415.5	81.8	.0501
<u>.</u> 51	44.7	A 48	•50	48,9	AS+2	415.5	8176	
• <u>6</u> 0	43.8	82.7	.60	48.7	82.2	.14.8	81.5	.0715
• 70	₽ų.1	8 .7	.71	48.7	£2.1	414.2	81.4	.0835
• 79	49.9	4. •3	•01	48.3	÷2•2	413.5	81.8	* 0 à £ à
.19	5 <sub>4.4</sub>	47.1	.81	48.7	82,7	412,9	82.4	.0962

PAGE: 2 DATE: 7/8/76

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

TEST RUNGER 11P PART D

TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 83.5 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020)INLET PRESSURE 415 PSIA (NOMINAL)

ŢĿSŢ	PAFCIMEN	INLET	CONDITIONS
			****

PRESSURE (PSIA)	4V6   EMP (UEG = F)	AVG FLOW RATE ( CFM)	GROSS DIFF• PRESS PRIMCRY (PSID)	GR: SS DIFF. PRESS SECONDARY (PSTD)	VA ČKORŽ DIEL PEEŽS (bžīņ)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)
417.4	92.2	.0976	310,180	310,180	310,180	•001	310.179
415.5	₹2•	. 4948	286.825	284,825	280.825	.001	580·853
415 <u>*</u> 5	81 <u>.</u> 9	.3837	209.172	209.172	509•115	•001	209.170
415.5	Þ1,8	.0723	158,983	158,943	158.984	.001	158,982
415.5	*1.8	.06 6	119,211	114,211	119.211	.000	119,210
415.5	51 <u>.</u> 5	491	85.791	87.330	87.061	.000	87,059
415.5	51.8	.03/4	59,697	60.164	59.940	•000	59,939
415 <u>.</u> 5	¢1,9	,~311	47.986	47,558	47.772	.000	47,771
415 5	45.4	. ;253	37,198	36,738	36.914	• 000	36,913
415.5	اوده	.0173	23,445	23.171	p3.31b	• 0 0 0	23.317
416,1	¤2.3	.4173	23,321	23,3 6	23.314	.000	23.312
416:1	×2.2	. 202	38,151	38.053	38.102	.000	38.101
416.1	0 > 0	1150.	47.615	47.284	47.500	•000	47.499
416.1	₽2.0	.9376	59,321	63,164	59.752	•000	59,751
415,5	8***	.95 1	86,913	87.962	87.437	•000	87 436
415.7	81,6	•05 <sup>98</sup>	115.739	115.7-9	115.732	•000	115.738
414.5	°1.5	.4715	154.880	154,85դ	154,88ÿ	.001	154.878
414.6	<b>01.4</b>	.^8. <sup>45</sup>	206.647	246.647	296.647	•001	206.648
413,5	>1.8	. 1949	284.612	284.6) g	284.612	•001	284.611
415.7	٥¿.4	.0962	298.817	298,817	298.817	.001	298,815

LARE DIFF. PRESS = -3.40000E-05 + -4.44000E-04 (ACFM) + 1.50933E-01 (ACFM)\*\*2 +

0 (ACFM)\*\*3

#### FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 7/8/76

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 83,5 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

TEST NUMBER 11P PART P TEST DESCRIPTION SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

TEST SPECIMEN INLET CONDITIONS

NET DIFFERENTIAL PRESS

***	***	****	****	***	***	****	***	****	***	ងន៍ជំនងស័ក្ <b>ងិសត់</b> ន៍ជង	****	
PRE55 <u>y</u>		***	TENPERATURE	***	****	***	FLOW RATE	****	***			
K@∕≌a cM	P\$14	DEG, A	DEG. ¢	DFG F	LIT#RS/ MIN	ACFM	SCFM	KP\H¥ PNS	LBŞ/HR	KG/SQ CM	PŞĂD	ļ
29.347	417.4	3 1.1	27.9	82.2	76.5	. 976	2.710	5•439	11.764	21.8077 **	310:179-	
29:210	415.9	306.9	27.8	85.0	74.1	•4948	2.621	5 <u>•</u> 161	11.377	19.7438	\$80°#53′	•
29,210	415,5	300.9	27.7	81.9	65.2	<b>.</b> ⊴837	2,314	4.550	10.044	14.7061	209.170	
29.210	415,2	308	7 • 72	8 <sub>1.8</sub>	56."	• 723	1.998	3,935	8.674	11.1775	158.782:-	
29.210	415.5	500.2	7.7	81.8	46.7	.0606	1.674	3,495	7.267	6.3813	119.510	,
29.210	415.5	304.8	27.5	8,,8	37.7	. 491	1.357	2.674	5.890	6.1209	87", 959	1
29.210	<u> </u>	3nr.8	27.7	81.8	28+7	• 4374	1.035	2:437	4 • 494	4.2141-	-23533	
29.210	415.5	-00.9	27.7	81.9	2 <sub>7•</sub> 6	•0311	.860	1:693	3.732	3.3586	47.371	
29,210	415,5	300.9	27.8	<b>65</b> *0	19,2	.0253	.700	1,379	3.037	2,595z	36,913	
29.210	415,5	3(1	27.8	82.1	12.9	. 173	.478	1944	2.076	1,6393	23,317	
29,256	410,1	3,1.1	.7.9	82.3	12.9	•0173	.478	±94±	2.075	1,6390	23.312	н
29.256	416.1	301.1	27.9	82.2	19.9	•1,262	.725	1.42	3,146	2,6787	38,101	Ų
29.256	416.1	301."	27.8	82	23.5	• 311	.861	1:595	3.739	3.3395	47.499	
29.256	415.1	360.4€	27.8	82.0	24.8	• )376	1.040	2:04%	4,517	4.2009	59. [5]	
29.210	415.5	360.5	′ 27.7	81.8	58.4	•9501	1.384	21722	6-009	6.1474	87.436	
29.210	415,2	300.7	27.0	81.6	46.3	.0598	1,655	3,252	7.185	§.1372		
29.165	414.9	306.6	27.5	81.5	55,2	. 715	1.975	3-883	8.573	10.8890	154.078	
29,119	414.6	306.6	×7.4	81.4	64•8	• 0835	p.304	4,53	10.001	14.5286	206.045.	.1
29.073	413.5	3,0,8	27.6	81.8	73.8	. ú949	2,612	5,144	11.341	20.0102	594.511	
59.02B	412.7	3 1.1	28.	52.4	74+5	•4962	2.640	2•19×	11.462	21.0088	298.412	
29,203	415,4	300.9	27.7	ul.9								
•04⊴	• ō	•1	•1	• Z	DEVIATIONS	<b>b</b>						

#### FLOW RATE VERSUS DIFFERENTI L PRESSURE

TEST HU-AFR 110 PART Q

TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 100.2 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL).

PAGE: 1

DATE: 7-8-76

 TEST SPECIMEN INLET CONDITIONS

***	766 A31 (14074)		****	FLOWMETER TWO	***			
FLOW RATE	( <u> </u>	TE'AD	FLOW PATE (+ CEM)	PRESSURE, (PSI <sub>a</sub> )	TEMP (DEG. F)	CRESSIJRE	AVG TEMP (DEG. F)	AVG FLOW RATE (ACFM)
-85	<b>*</b> 2•7	77*,	-01	47.4	81+7	1 11.9	79.3	.0425
• 7B	44.3	76.2	.81	48,3	41.2	1 (11,9	78,7	.0387
•69	+y.4	74-1	• 7 ·	44.5	H1+1.	1 11.9	78.6	.0338
.60	+2+1	75*	• 59	48.5	71.1	1 11.9	78.6	.0291
<b>.</b> 50	47.7	74.6	.5v	48.9	81.2	1,11,9	78,9	.0245
•41	<b>4</b> 2.5	77+1	•4•	49.3	11.4	1 11,9	79.2	.0198
•32	20.00	77.9	• 40	49.9	41 <b>4</b> 8	1 11.9	79.9	.0153
•27	#7.b	79.9	•5ē	49.1	b3•2	1 15.9	81.6	.0127
• 22	P1	ધ •્2	• 51	49.9	ч <b>3.</b> 4	1 15.9	81.8	.0104
.15	*À*A	81+8	•1 <i>+</i>	49.9	n 1+7	1 15.9	82.3	.0070
•15	47.9	81.8	.)3	49.7	64.3	1 15,9	83.1	.0069
<u>,</u> 23	44.5	8-1-6	•21	49.3	14.2	1 15,9	82.9	.0107
.27	45.5	81.5	• 23	49.5	44•1	1 15.9	82.7	.0127
.32	44.7	A +8	+31	49.3	.4.	1 15.9	82.4	.0153
•42	+₹.5	8 •1	- 41	48 <b>.</b> 9	B~•7	1 15.9	81.97	.0199
<b>.</b> 51	49.7	79.2	•51	48.9	83.4	1 15,9	81.3	.0246
• <b>6</b> 0	÷ •4	72.2	•61	49.3	F2.7	1 15,9	80.4	.0296
• 69	5 <sub>4</sub> , .	77++	.71	,.9 <sub>€</sub> 1	A1.8	1 15.9	79.4	.0343
.78	<b>ተጟ•</b> ፟፟፟፟	76.4	.81	48,3	81.2	1411.9	78.8	.0385
.87	51	75•7	•61	47.9	96	1 11.9	78.1	.0430

TABLE 97
FLUW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7-8-76

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TFST NUMBER 11Q PART Q TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS
DIFFERENTIAL PRESSURE. TOTAL OF 100.2 mg OF
SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN
(S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL).

TEST SPECIFIEM INLET COMPITIONS

,	• •						
PRESSUKE	nvG LEMP (DEG. F)	.VG FLOW RATE ( CFM)	GROSS DIFF• PRESS PRIMARY (⊝SIO)	gRass DIFF. PRESS SECONDARY (PSIn)	AVG GRUSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	NET DIFF. PRESS (PSID)
1011.7	19.3	, 425	81,911	82,7:1	82,300	-0.000	82.306
1011.7	/8.7	.1387	71.733	72.690	72.165	<b>-0.000</b>	72.167
1011.4	10.6	BLEn.	59,737	60,605	60,171	-0.000	60.171
1011-7	/8•6	. 2 <sup>9</sup> 1	48.973	49.873	49.424	-0.000	49.423
1011.4	18.9	. 12.45	40.141	39.798	39.970	-0.000	39.970
1011.7	19,2	_a198	30,460	30,145	30.304	-0.000	30,303
inll <sub>*</sub> y	/9•9	. ,153	22,180	21.494	22.041	-0.000 _	22 <u>•0</u> 41
1012,4	01.6	. 1127	17.827	17.6 6	17.716	-0.000	17.716
1912°Ā	81.8	.01 '4	14.022	13.780	13,901	~0.0UO	13.901
1012 <b>-</b> 4	52 <u>•</u> 1	.00(0	8.84	8.7/2	8.801	-0.000	8.801_
015.¥	I.Ea	.0009	8.715	d.762	8.738	-0.000	8,739
1015.7	32 <b>.</b> 9	.0177	14,272	14.293	14.284	⇔9.000	14.283
015.7	ø2• <b>7</b>	.1127	17,640	17.669	17.65]	-0.000	17.651
1012.4	52.4	.0153	21,939	21.894	· 21.915	-0.000	21.917
1015.4	·1•9	.0199	30,4/0	30.317	30.389	-0.000	30.389
1015.,4	o1.3	. 1246	40.141	39.971	40.055	-0.000	40.056
1012.7	ø <sub>11 +</sub> 4	•≎296	49.724	50.5 14	50.114	-0.000	50.114
ذة 1015	(9 <u>•</u> 4	<b>₽</b> 9343	60.864	61.552	61.407	-0.000	61.208
rofi'i	8,81	.1)3H5	71,483	72.284	71.884	-0.000	71.884
lo11•X	18.1	+0439	84.007	84.910	84.459	<b>*0.000</b>	84.459

0 (ACFM) \*\*3

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# TABLE 97 FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 7-8-76

TEST NUMBER 110 PART 3 TEST DESCRIPTION

CONTAMINATED CONDITION - FLOW RATE VERSUS DIFFERENTIAL PRESSURE. TOTAL OF 100.2 mg OF CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 1000 PSIA (NOMINAL).
NET DIFFERENTIAL PRESS

TEST SPECIMEN INLET CONDITIONS 

\*\*\*\*\*\*\*\*\*\*\*

PRESSURE		EMPER			FLOW RATE							
	K@/50 CM	PSIA	DEG. K	DEG. C	DEG. F	LIT-RS/ MIN	СFМ	SCEM	ĸä∖Hử ċúS	GN2 LBS/HR	KG/SQ CM Differențiăl	PS¦D.
	71.144	1111.7	299.5	₽6.3	79,3	81.6	. 425	2.874	5,660	12.478	5,7867	85*306 .
	71,144	1011.3	299.1	25.9	78.7	74•4	• 1387	2.619	5 <u>•</u> 15 <i>!</i>	11•369	5.0738	72.167
	71,144	1011,7	299.0	25. <sup>9</sup>	78.6	64.6	<b>.</b> 0338	2,287	4.504	9.929	4.2304	60,171
ij	71.144	1 111-3	299•1	25.9	78.6	55•5	• 2 <sup>9</sup> 1	1.972	3 • គ 8 ភ	8.561	3.4748	49.423
	71.144	1011.7	ے 99م	26.1	78.9	46 • S	•"245	1.658	3.265	7.197	2.8102	39.270
	71,144	1011'5	299.4	26.2	79.2	37.2	.0198	1,338	2.635	5.810	2.1305	30.303
	71+14 <del>4</del>	171197	299.8	26.6	79.9	28.7	. 1153	1.036	2, 35	4,496	1.5496	55.04Î
	71:423	1015.7	300.7	>7.5	81.6	93.7	. 11:27	.859	1*651	3.728	1.2456	17.716
	71.423	1415,7	300.8	27.7	81.8	19•4	.0104	.704	1*38	3.057	.9774	13,501
	71.423	1 /15.7	3 1.1	27.9	82.3	12.8	•#071	•471	• 551	2.043	.6188	- 8°ã0j -
	71,423	1015.7	301.5	8 • 4	83.1	12.6	.4069	•466	∙åĭä	2•024	•6144	8.139
	71.423	1015,7	3n1.5	28.3	82.9	19.9	.0107	.723	1,423	3,136	1.0042	14.283
	71.423	1115.7	3.1.3	28.2	82.7	23.7	. 127	.858	1.690	3.725	1.2410	17.651
	71,423	1915,7	301.2	28.4	82.4	. 28.5	• 7153	1.030	5.052	4+472	1.5409	S1•313
	71,423	1,115.7	300.9	27.7	81.9	3 <b>7 •</b> 5	. 199	1.147	2 <u>•</u> 65≮	5 846	2,1365	30.389
1	71,424	1,15.7	300,6	27.4	81.3	46.8	.J246	1,667	3 • 28 4	7.239	5.87es	40 :056
	71.423	1015.7	300.1	26.9	80+4	56•,3	•11296	2.005	3.941	8.702	3.5234	50.114
	71,423	1015.7	299.5	و. 6٤	79.4	65.8	• 1343	S+358	4 <u>•</u> 583	10.104	4.3033	61.208
	71.144	1911.9	299,2	26.0	78.8	74.1	.0385	2,610	2°13×	11.330	5,0540	71.464
	71:144	1911+2	***** 299.8	25.6 ****	78 • 1 *****	82•8	• 043 <i>1</i> 1	2.918	5.747	ĩ2 <u>•</u> 665	5.9381	84,459
	71.297	1014.4	300.1	26.9	ថ្ន0.5						M .W.	
	•138	۶۰۷	•9	•9	1.5	DEVIATION	s					

# FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 1 DATE: 7/8/76

TEST NUMBER 11R P\_RT Q TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE TOTAL OF 100.2 mg OF. SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL) TEST SPECIMEN INLET CONDITIONS

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# FLOWMETER CONDITIONS

· · · · · · · · · · · · · · · · · · ·	AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA		
FLOWNILIER ONE	FLOWMETER TWO		***** * *
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***	****	***	****	***				
FLOW RATE (ACFM)	(hàin) brespore	TEMP (DEG• F)	FLOW RATE (ACEM)	PRESSURE, (PSIA)	TEMP (DEG. F)	PRESSURE (PSIA)	AVG TEMP (DEG. F)	ÁVĞ FLOW RATE (acem)
-81	#2+7	7 :3	٤8.	47-9	77.5	417.9	76 <b>•</b> 9	.7958
.78	àñ *3	76.1	.81	48,5	77.3	416.6	76.7	.0944
• 70	ხ; •5	75 • B	+71	48.9	77.3	416.	76.5	.0839
•60	26.5	75+6	•61	49•3	77•3	416.0	76+5	.0724
<b>,</b> 51	42.7	7=,6	•50	48.9	77.4	416.n	76.5	• 9 <b>599</b> °
<b>,</b> 42	44.8	7557	.41	49.3	~7.5	416.	<del>76</del> .6	.0₹92.
.32	ឆ្នក់*3	75.7	.30	49.9	77.6	416.0	76.5	, ŏ373' ¨
•27	5 1 a 3	75 <u>•</u> ,	• 26	49.9	77.7	416.	76.7	.0315
• 22	3 يا ت	76.6	1	54.1	77.8	416.9	76.9	•0256
.15	44.8	7n+3	•14	49.9	78.1	416.6	77.2	.0173
•15	±7.	75 <u>4</u> 8	<b>∍</b> 1 4	49.5	78.4	417.3	77.6	.10112
•22	42.9	76+8	• 71	49.5	78.4	417.7	77+5	•0258°
•27	4Å*8	76 <u>*</u> 7	+26	49.5	78.4	417.3	77.5	
•32	47.9	76•6	• 7,1	49.5	78 • <i>4</i>	416.6	77.5	.0373
•42	49.9	76+4	•41	49.3	78.7	416.6	77.3	•0489
<b>.</b> 51	49.5	76 <u>*</u> 3	•5i	49.3	77.9	412.1	77-1	*0ē15
•60	ခန့္နဲ႔	76+3	•60	49.1	78.1	16.5	77.2	.0719
.70	50.1	76+3	.71	48.7	77.9	415.3	. 77.1	.0838
.78	44,9	76 <u>•</u> 8	•81	48.3	78•1	414.7	77.5	
• 79	?v.1	77•4	.81	48.3	78.3	414.0	77.B	.0950

TABLE 98
FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 2 DATE: 7/8/76

TEST WUMBER 11P PART P

TEST DESCRIPTION

CONTANINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE, TOTAL OF 100,2 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

TEST SPECTIVEN INTEL CONVILIONS

PRESSURE .	, 6VG  E P (OrG. F)	aVG FLOM RATE (/CFM)	≒ROSS DIFF• PRESS PRIMARY (PSIO)	GRASS DIFF. PRESS SECOKDARY (PSIA)	AVG GHUSS DIFF. PRESS (PSID)	TARE DIFF. PRESS (PSID)	DIFF. PRESS NET.
417.2	(6.9	.0958	36,9.725	309,725	309,725	.001	309.724
416.0	16,7	944	297.783	297,(83	297.184	.001	297.082
415.0	/6.¤	_68 9	218.388	214,348	218.385	.001	218.387
416.	16,5	.4724	164.970	164.976	164.97 <u>6</u>	.001	164.975
416.0	16.5	599	124,414	12.,414	120.414	.000	120.412
416.0	16.6	.r 92	89,252	89.707	89.505	.000	89.503
416. ي	10.6	_e373	60,641	61,513	60.977	.000	60.976
415.0	16.7	.0315	48,471	48,987	48.729	.000	48.728
416.	76.9	<b>.</b> 256	38,156	37.745	37.951	.000	37.950
416.0	17.2	.0173	24,056	23.7 9	<b>53</b> *885	.000	23.881
417. ي	17.6	.0172	23.495	23,536	23.516	• U O O	23,515
41/•==	17,6	. 258	37,599	37.637	37.615	.000	37.613
417.3	17,5	<u>.</u> 0117	48,471	48,987	48.729	.000	48.728
416.9	17.5	.0373	59,763	60.081	60 <b>.</b> 225	•000	60.221
416.0	17.3	. 489	86,554	87.545	87.050	.000	87.048
417.1	17:1	.0615	118.517	118,517	118,517	.001	118.516
416.4	17,2	.0719	161.816	161,816	161,816	.001	161.814
415•3	17.1	958	217.124	217.124	217.124	•001	217.122
414.1	17.5	-0941	293.031	298,431	588 • 03 j	.001	298.030
414.9	17,8	. 7950	310,673	310,673	310.674	.001	310,672

FLOW RATE VERSUS DIFFERENTIAL PRESSURE

PAGE: 3 DATE: 7/8/76

TEST NUMBER 11R PART R TEST DESCRIPTION

CONTAMINATED CONDITION-FLOW RATE VERSUS DIFFERENTIAL PRESSURE TOTAL OF 100.2 mg OF SYNTHETIC CONTAMINANT ADDED. TEST SPECIMEN (S/N 020) INLET PRESSURE 415 PSIA (NOMINAL)

<b>#</b> # #	****	*****	****	TEST :	SPECIMEN INL	EL CONDITION	S 	****	****	***	NET DIFFERENT	IALI PRESS
}. *****	PRESSURE		aaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaa			FI.OW RATE						
K <u>G</u> /	'SQ CM	bālr	oeg, K	ñEG. C	ΰEĞ. F	LITERS/ MIN	∆ <b>C</b> FM	SCFM	KÖ\HÄ äüS	GN2 LRS/HR	KG/SQ CM DIFFERENTIÄL	PSAD
2	9.384	417.2	298.1	24.9	76.9	75.8	. 958	2,688	5,29,5	11.670	21.7758 ~	399, [54
S	9 • 293	410,9	298.0	24.8	76.7	74.6	•11944	2.643	5.204	11.472	20.8869	297.082
2	9.247	416.7	297,9	24.7	76.5	65.9	.0839	2,345	4,615	10.182	15.3541	218,357
5	9.247	416.	297.9	24.7	76.5	56.8	.0724	2.025	3*,81	8.790	11,5989	164,275
2	9.247	416 • 4	297.9	24.7	76.5	46.8	. 599	1.674	3,295	7.267	8,4658	120.512.
5	9.247	416, 9	297,9	24.8	76.6	38.2	•⊎492	1.376	2.707	5.972	6.2927	89.503
2	9.247	416 <sub>5</sub> .	298.v	24.8	76,6	28.9	.4373	1.044	2:055	4.531	4.2870	60.276
2	9.247	410٠٠	298.0	<b>24</b> •8	76.7	>4.3	./315	.882	1.732	3.827	3.4259	48.728 **
2	9.247	416.5	298.1	24.9	76.9	19+7	1256	.715	1,40/	3:102	2.6682	37'- 250 "
2	9.293	416.0	298.3	25.1	77.2	13.1	. 173	.485	<u>.</u> 954	2.103	1.6790	53-581
5	9 , 338	د. 417	o98.5	o5.3	77.6	13:0	. 117	.481	.945	2.090	1.6532	53.515:
s	9,338	411.3	298.5	25.3	77.6	19.7	• J258	.721	1.420	3.130	2,6445 -	37.513.
S	9.338	417.9	298.5	25.3	77.5	24.4	• 317	.888	1 = 745	3,853	3.4259	48, 728
5	9•59 <i>9</i>	416.9	298.4	25.3	77.5	28•4	• 1373	1.043	2: 654	4.526	4.2339	.60• <b>45</b> 1
S	9.293	41 <u>0, p</u>	298.3	25.7	77.3	38•0	.0489	1.368	2,694	5.940	5.1201	87°, 948
2	8,973	412,1	298.2	25.0	77.1	48.2	.0615	1.702	3 • 350	7,386	8:3325	
S,	9.247	410.	298.3	25.1	77.2	56.4	• 1719	2.009	3,955	8.720	11.3767	161;814
2'	9.201	+15.9	298.2	25•l	77.1	65.8	• v838	335 وڊ	4 <u>•</u> 59 <u>9</u>	14.138	15.2652	217.122
5,	9,155	414.5	298.4	25,3	77,5	74.0	.0941	2,618	ระเระ	11.366	20.9536	588 <u>.</u> 630
	9.110 #####	414. ******	998.6 ****	25.5 ****	77.8	74+3	•095n	2.636	5,190	ĭ1 <u>•</u> 441	21.8424	310.645
S	9.249	410.0	2,8,2	25.0	77.1							
	•058	•0	•2	• 4	• 4	DEVIATIONS	3			•		